PRELIMINARY DRAINAGE REPORT FOR

Oak Grove Subdivision Salem, Oregon

Prepared For: R & S Kamineni 2500 Gleneagles Road Lake Oswego, Oregon 97034

December 3, 2021





1155 13th Street SE Salem OR 97302

 PHONE:
 (503) 363-9227

 FAX:
 (503) 364-1260

 EMAIL:
 mhendrick@mtengineering.net

Contents

ntroduction	. 1
Existing Conditions	.1
Soils	. 2
Infiltration	. 2
Water Quality Methodology	. 2
Nater Quality Analysis	. 2
Nater Quality Design	. 2
Stormwater Quantity Analysis	.2
Stormwater Quality Analysis	.4
Conclusion	.4

Appendix A	Maps
Appendix B	Soils Report
Appendix C	Time of Concentration
Appendix D	Stormwater Quantity & Quality Analysis

INTRODUCTION

The Oak Grove Subdivision is a proposed 57-lot subdivision located east of Lone Oak Road SE and south of La Cresta Drive SE. The parcel of land to be developed is Tax Lots 1900 through 2200 of Marion County Assessor's Map 08 3W 15CB. A vicinity map and supporting maps are in Appendix A of this report. An aerial image is below.



Project Site

Green Stormwater Infrastructure (GSI) to the Maximum Extent Feasible (MEF) is being used for the new developed areas per City of Salem Administrative Rules, Chapter 109, Division 004, Stormwater System, Appendix 4E and Ordinance No. 8-20 (Standards). All facilities will be constructed to meet the City of Salem Standards.

EXISTING CONDITIONS

The 12.2-acre site is irregular in the shape. Surface conditions consist of grassy meadow and Wooded areas. There are no identified wetlands or sensitive areas located on the property. A topographical high point ridge is located on the southerly property line near the terminus of the existing Sarah Renee Avenue SE. Drainage from this high point flows north, east, and west. The maximum relief is approximately 65.5-feet with a high point elevation of 561.5-feet. The abutting properties are zoned

single family residential with public improvements that include storm water conveyance systems. Appendix A contains multiple maps of the site.

Soils

The Natural Resources Conservation Service (NRCS) Soil Resource Report for Marion County was used to determine the Hydrological Soil Group classifications for runoff calculations. The report identifies the site soils to be Jory and Nekia soils. All the soils are in the hydrologic soil group C. The report is in Appendix B.

Infiltration

Infiltration testing will be performed at the site to determine percolation rates of the soils. It is anticipated that test results will indicate rates below 0.5 inches.

WATER QUALITY METHODOLOGY

Because of anticipated poor percolation rates of the soils and natural steep slopes that dominate the site, green stormwater facilities are designed as combination facilities.

WATER QUALITY ANALYSIS

Water quality flow rates will be calculated with HydroCAD 10.00. The SCS TR-20 Unit Hydrograph method will be used to generate the hydrographs. A Type 1A storm and a 24-hour rainfall depth of 1.38 inches per hour will be used to determine the water quality flow rate.

WATER QUALITY DESIGN

The multiple combination facilities will provide water quality treatment by allowing for the removal of pollutants through sedimentation, adsorption onto surrounding vegetation, filtration, and biological uptake. The facilities will be designed per the City of Salem designed standards.

STORMWATER QUANTITY ANALYSIS

Stormwater quantity (Flow Control) is proposed to be handled by on-site detention. Runoff from the developed site will be routed to the facilities that ultimately controls runoff to pre-developed flow rates. Approximately 12.6-acres of land are being disturbed and developed.

Per Subsection 4.2(p)(3)(A) of the standards, one-half of the post development peak runoff rate of the two-year storm must be equal to or less than one-half of the peak runoff rate of the pre-developed two-year, 24-hour storm. This also applies to the 10, 25 and 100-year, 24-hour storm events.

The pre-developed flow rates were calculated using HydroCAD 10.00. Table 1 below lists the 24-hour rainfall depths used for the analysis of each storm event. Please note that the 2-year event was halved and then analyzed.

Table 1	1
---------	---

Storm Event	24-hour Rainfall Depth (in)
2	2.2
10	3.2
25	3.6
100	4.4

For the pre-developed conditions, a time of concentration of 62 minutes was calculated for the Basin. The time of concentration data is in Appendix C. The calculations are incorporated in the HydroCAD output located in Appendix D. The entire area was classified as "City of Salem Pre-Development, HSG C" with a Curve Number (CN) of 72. A pre-developed basin map is in Appendix A.

The SCS TR-20 Unit Hydrograph method was used to generate the hydrographs. A Type 1A rainfall distribution was used with the above rainfall depths. Table 2 below identifies the allowable predeveloped release rate for each storm event.

Half of 2-year0.0410-year1.2625-year1.79100-year3.01	Storm Event	Basin Allowable Release Rate (cfs)
25-year 1.79	Half of 2-year	0.04
	10-year	1.26
100-year 3.01	25-year	1.79
,	100-year	3.01

Table 2

The post-developed flow rates were calculated using HydroCAD 10.00. A time of concentration of 10 minutes was assumed for the developed site. The calculations are incorporated in the HydroCAD output located in Appendix D. Because of existing surrounding streets and large lot areas, the site was classified as 40 percent "Impervious, HSG C" with a CN of 98 and 60 percent "> 75% Grass cover, HSG C" with a CN of 98 and 60 percent "> 75% Grass cover, HSG C" with a CN of 74. Table 3 below lists the CN values for the developed areas that will contribute storm water runoff to the detention systems. A developed basin map is in Appendix A.

Table	3
-------	---

Basin	Impervious Area (Ac) CN = 98	Landscape Area (Ac) CN = 74	TOTAL Area (Ac)	Composite CN
Site	5.04	7.56	12.60	84

Table 4 below identifies the calculated detention volume requirements for each storm event. The required detention was determined by using HydroCAD and taking the differential runoff volume between predeveloped and developed conditions.

Storm Event	Basin Detention Volume (cf)
1/2 of 2-year	7,900
10-year	34,425
25-year	38,200
100-year	44,825

Table 4	
---------	--

The proposed four detention systems will be located near the lowest corners to maximize the capture of runoff. A basin map has been provided in Appendix A showing the location of the detention ponds/combination facilities. Allowable flow rates for the entire site are identified in Table 2 above.

STORMWATER QUALITY ANALYSIS

Water quality flow rates were calculated using HydroCAD 10.00. The SCS TR-20 Unit Hydrograph method was used to generate the hydrographs. A Type 1A rainfall distribution was used with a 1.38 rainfall depth. Appendix D contains the analysis.

The detention facilities will incorporate combination facility sections and will be constructed per City of Salem standards.

CONCLUSION

Based on the presented information, the proposed design will meet the water quality and quantity standards. If there are any questions regarding this analysis or the design, please contact Matthew

Hendrick at Multi/Tech Engineering by phone at (503) 363-9227 or via e-mail at mhendrick@mtengineering.net.

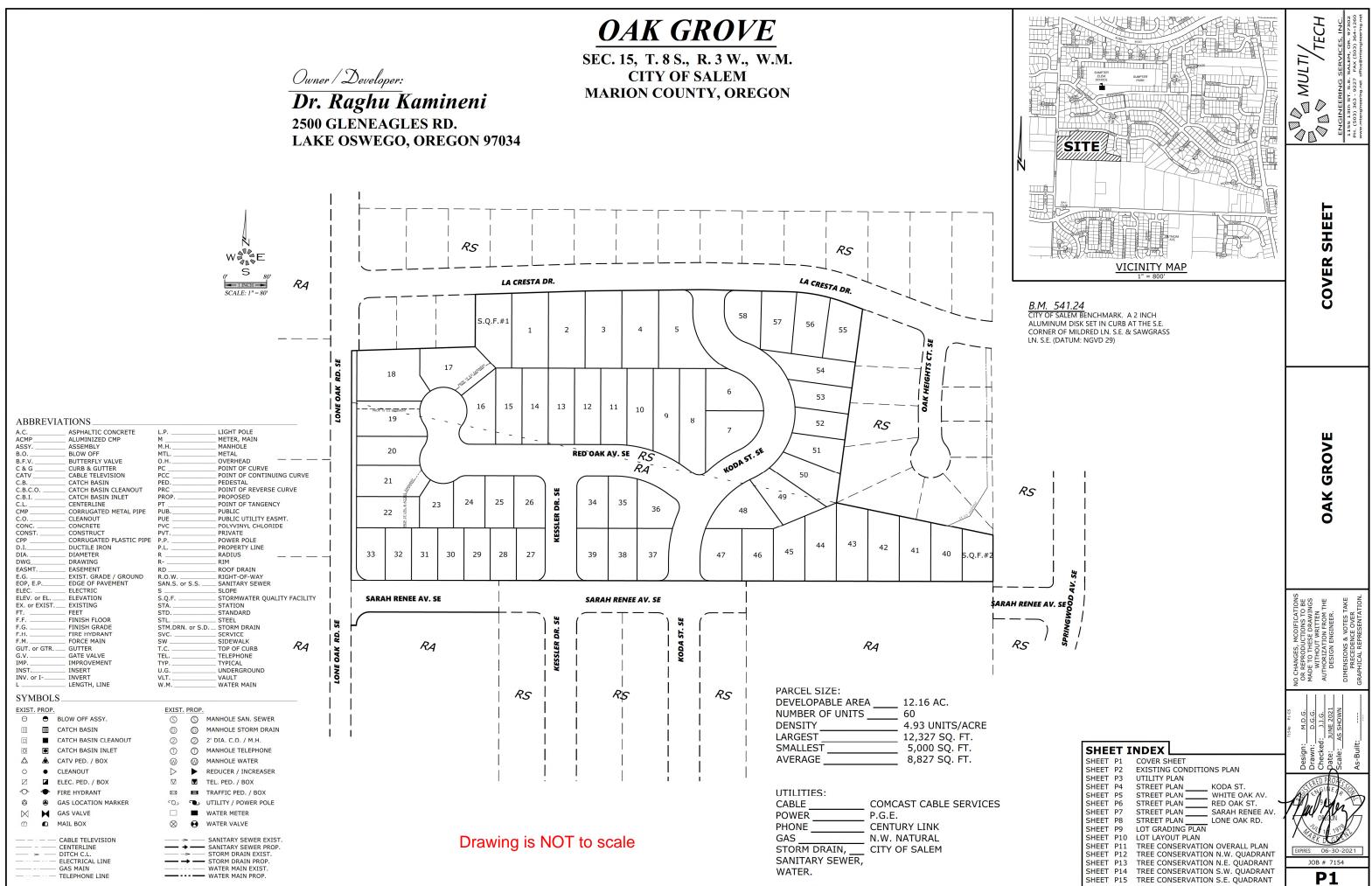
Appendix A

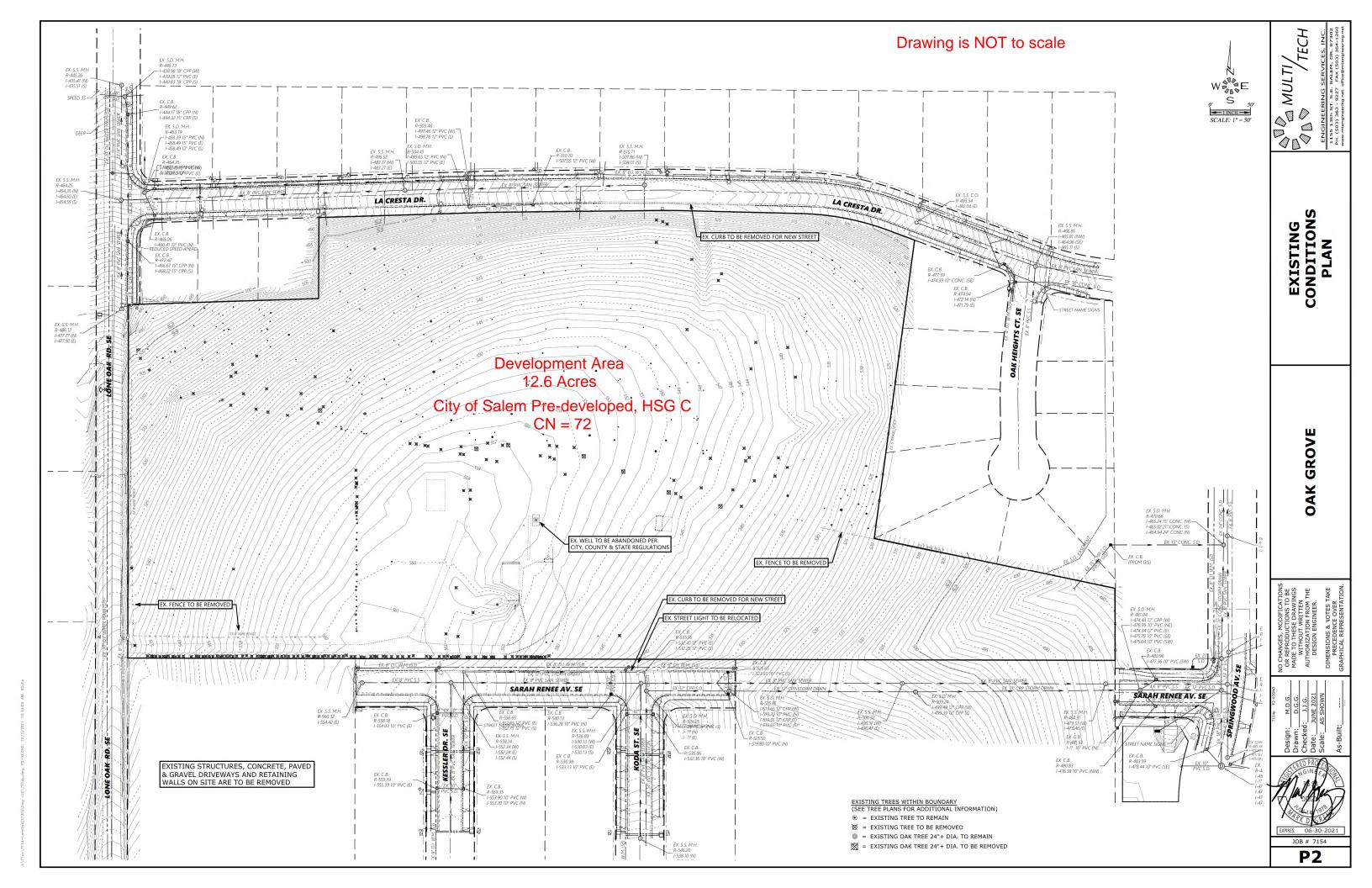


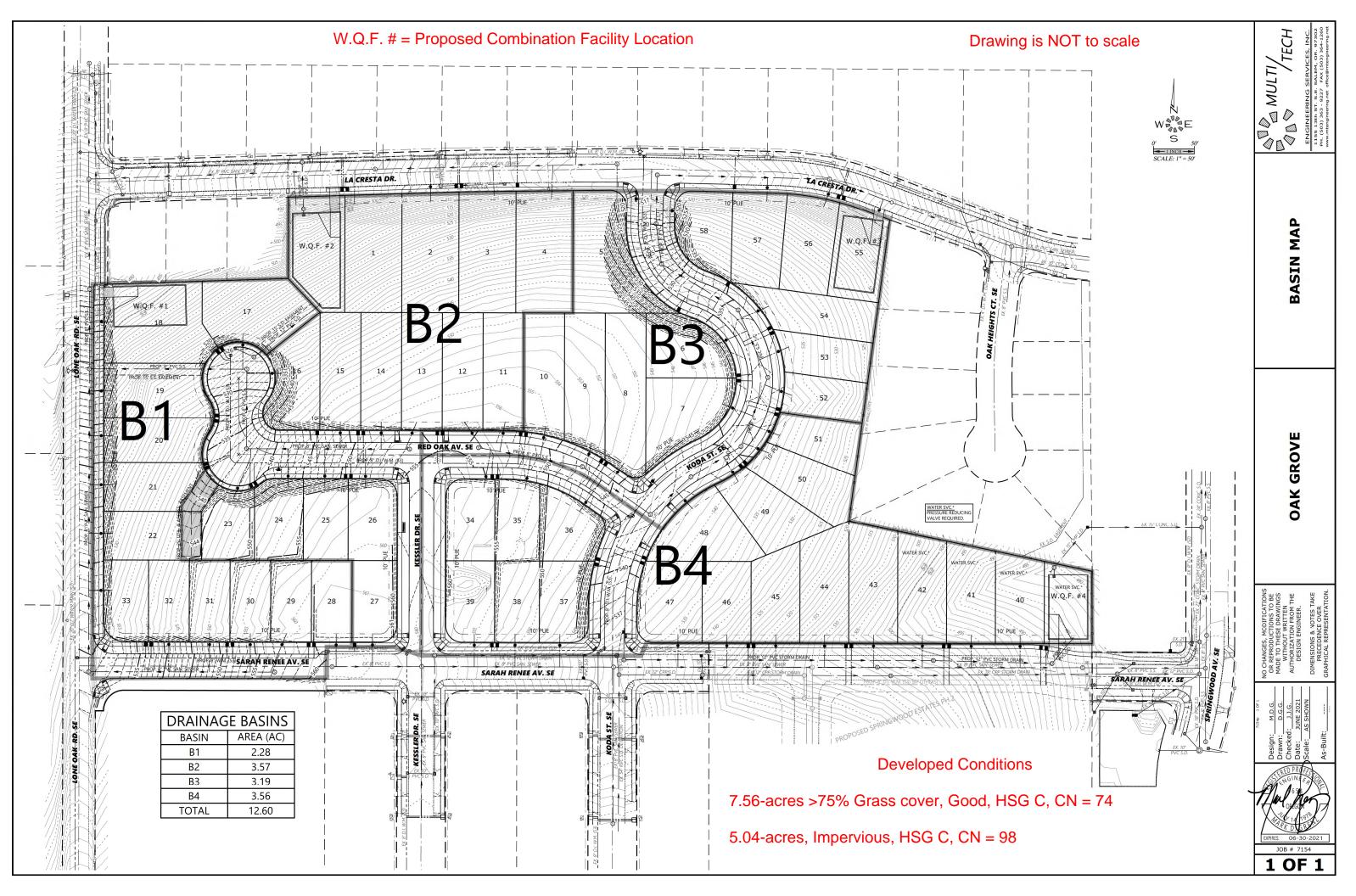
CITY OF SALEM MARION COUNTY, OREGON



2500 GLENEAGLES RD.







Appendix B



United States Department of Agriculture

Natural Resources Conservation

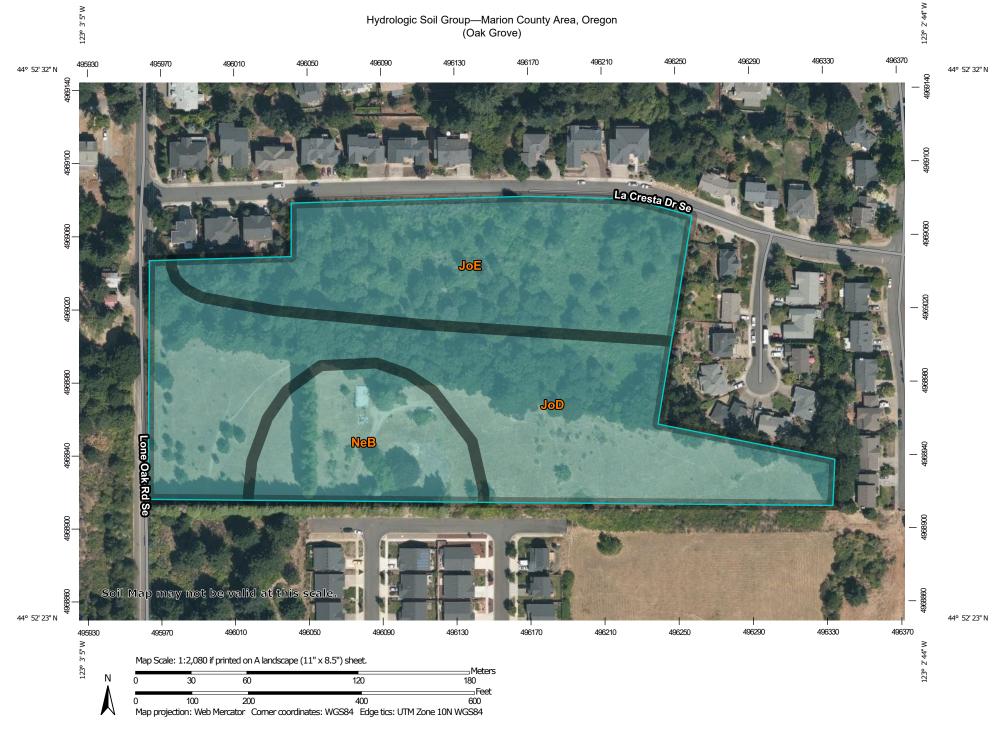
Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

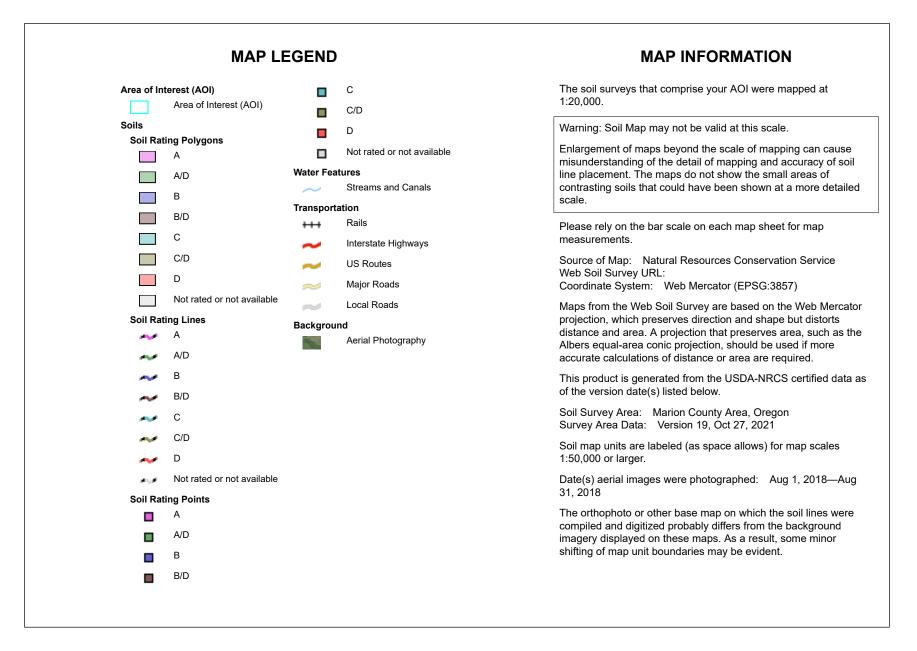
Custom Soil Resource Report for Marion County Area, Oregon

Oak Grove





USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey 12/2/2021 Page 2 of 4



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
JoD	Jory silty clay loam, 12 to 20 percent slopes	С	6.0	49.6%
JoE	Jory silty clay loam, 20 to 30 percent slopes	С	4.2	34.4%
NeB	Nekia silty clay loam, 2 to 7 percent slopes	С	1.9	16.0%
Totals for Area of Intere	est		12.1	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

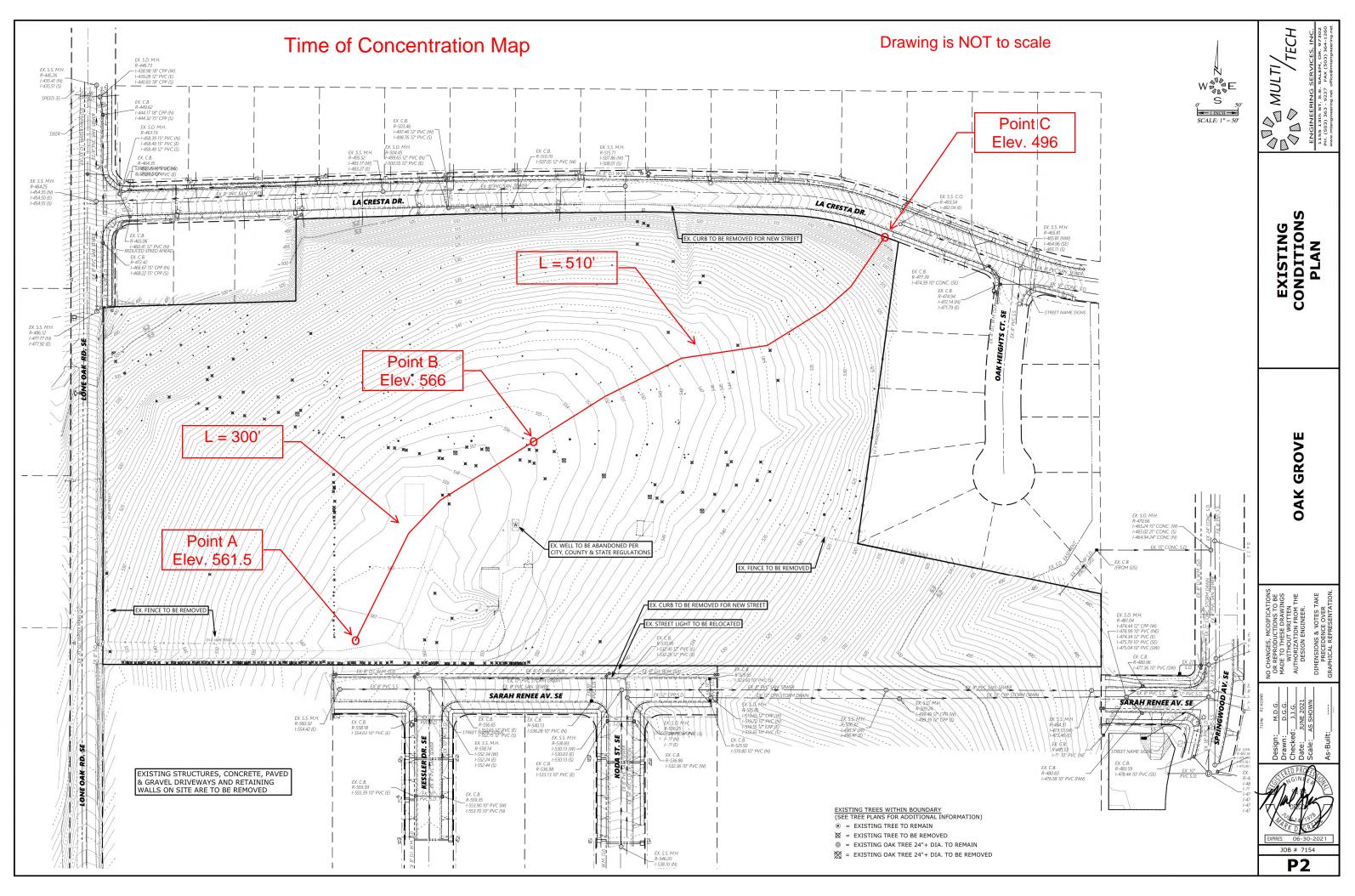
Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

USDA

Appendix C



\71xx\7154-LoneOak(5730)\Dwg v20\7154p.dwg. P2-XCOND. 12/1/2021 1

Worksheet 3: Time of Concentration (T_c) or travel time (T_t)

Project Oak Grove	^{By} M. Hendrick	Date 12/2021			
Location Salem, Oregon	Checked	Date			
	Check one: Crc CTt through subarea				
Sheet flow (Applicable to Tc only)	-				
Segment ID1. Surface description (Table 4D-4)2. Manning's roughness coefficient, n (Table 4D-4)3. Flow length, L (total L † 300 ft)4. Two-year 24-hour rainfall, P25. Land slope, s5. Land slope, s6. $T_t = \frac{0.007 (nL)}{P_2^{0.5} s^{0.4}}$ Compute Tt	. Mixed	= 0.861			
Shallow concentrated flow					
$\begin{array}{c} \text{Segment ID} \\ \text{7. Surface description (paved or unpaved)} & \dots \\ \text{8. Flow length, L} & \dots \\ \text{9. Watercourse slope, s} & \dots \\ \text{10. Average velocity, V (figure 3-1)} & \dots \\ \text{11. } T_t = \underbrace{L}_{3600 \text{ V}} & \text{Compute T}_t & \dots \\ \text{hr} \end{array}$	B-C Forest 510 0.118 0.8 0.177 +	= 0.177			
Channel flow					
Segment ID12. Cross sectional flow area, a		= Hr 1.04			

Manning's Roughness Coefficients for Overlar	nd Sheet Flow
Surface Types:	n
Impervious Areas	0.014
Gravel Pavement	0.02
Developed: Landscape Areas (Except Lawns)	0.08
Undeveloped: Meadow, Pasture, or Farm	0.15
Developed: Lawns	0.24
Pre-developed: Mixed	0.30
Pre-developed: Woodland and Forest	0.40
Development Types:	n
Commercial Development	0.015
Industrial Development, Heavy	0.04
Industrial Development, Light	0.05
Dense Residential (over 6 units/acre)	0.08
Normal Residential (3 to 6 units/acre)	0.20
Light Residential (1 to 3 units/acre)	0.30
Parks	0.40

Table 4D-4. Manning's Roughness Coefficients for Overland Sheet Flow

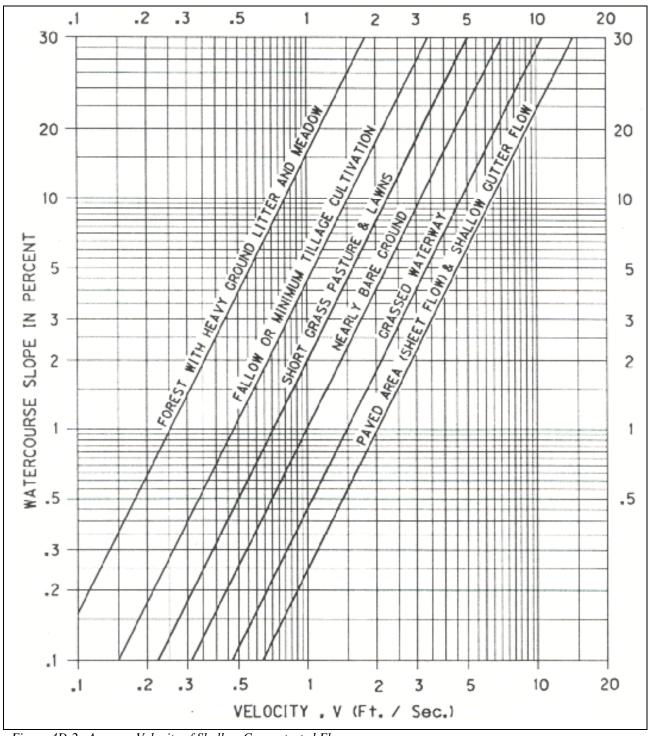
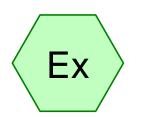


Figure 4D-2. Average Velocity of Shallow Concentrated Flow

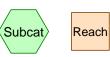
Appendix D



Existing Conditions



Developed Conditions





Link

Routing Diagram for 20211203 Hydrology Master Prepared by Multitech Engineering Services, Inc., Printed 12/3/2021 HydroCAD® 10.10-6a s/n 09412 © 2020 HydroCAD Software Solutions LLC

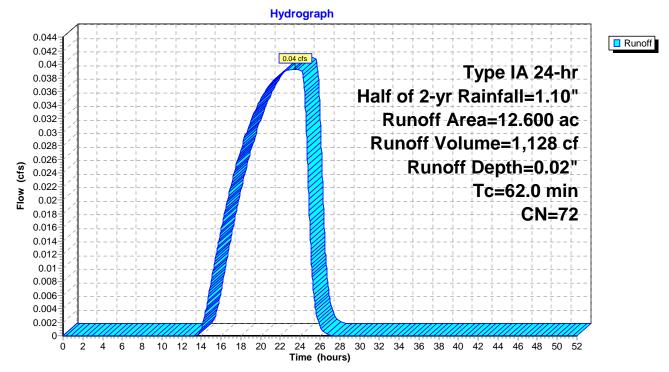
Summary for Subcatchment Ex: Existing Conditions

0.04 cfs @ 23.49 hrs, Volume= 1,128 cf, Depth= 0.02" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-52.00 hrs, dt= 0.02 hrs Type IA 24-hr Half of 2-yr Rainfall=1.10"

_	Area	ea (ac) CN Description					
*	12.	12.600 72		2 City of Salem Pre-deve			bed, HSG C
	12.600		12.600 100.00% Per		00% Pervi	ous Area	
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	62.0	·					Direct Entry, TR-55 Worksheet

Subcatchment Ex: Existing Conditions



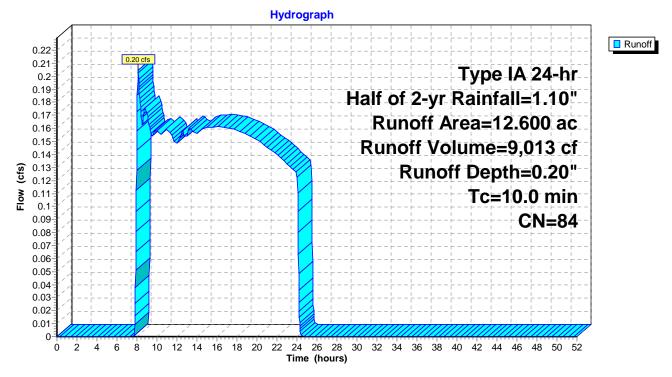
Summary for Subcatchment D: Developed Conditions

Runoff = 0.20 cfs @ 8.10 hrs, Volume= Routed to nonexistent node CMH 9,013 cf, Depth= 0.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-52.00 hrs, dt= 0.02 hrs Type IA 24-hr Half of 2-yr Rainfall=1.10"

Paved parking, HSG C			
>75% Grass cover, Good, HSG C			
Weighted Average			
60.00% Pervious Area			
40.00% Impervious Area			
Slope Velocity Capacity Descriptio (ft/ft) (ft/sec) (cfs)			
Direct Er	v, Assumed		
 >75% Grass cover, Good, HSG C Weighted Average 60.00% Pervious Area 40.00% Impervious Area Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs) 	v, Assumed		

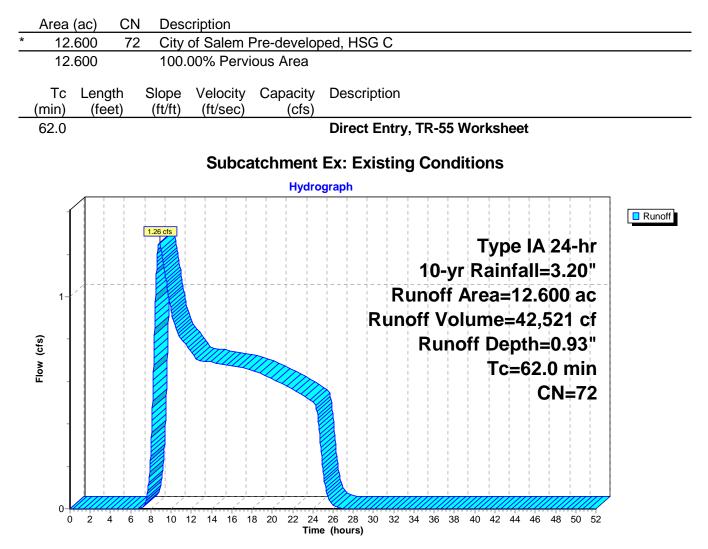
Subcatchment D: Developed Conditions



Summary for Subcatchment Ex: Existing Conditions

Runoff 1.26 cfs @ 8.85 hrs, Volume= 42,521 cf, Depth= 0.93" _

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-52.00 hrs, dt= 0.02 hrs Type IA 24-hr 10-yr Rainfall=3.20"



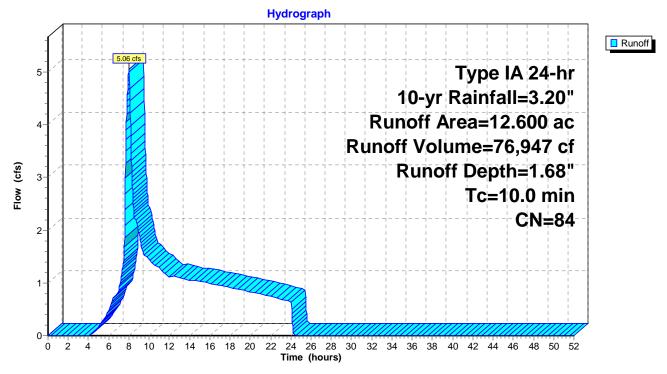
Summary for Subcatchment D: Developed Conditions

Runoff = 5.06 cfs @ 8.02 hrs, Volume= Routed to nonexistent node CMH 76,947 cf, Depth= 1.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-52.00 hrs, dt= 0.02 hrs Type IA 24-hr 10-yr Rainfall=3.20"

Ar	ea (ac)	CN	Desc	Description						
	5.040	98	Pave	ed parking	, HSG C					
	7.560	74	>75%	6 Grass co	over, Good,	, HSG C				
	12.600	84	Weig	ghted Aver	age					
	7.560		60.0	0% Pervio	us Area					
	5.040 40.00% Impervious Area									
-	To Longth (Volocity	Consoitu	Description				
	0		Slope	Velocity	Capacity	Description				
(mi	n) (ree	et)	(ft/ft)	(ft/sec)	(cfs)					
10	.0					Direct Entry, Assumed				

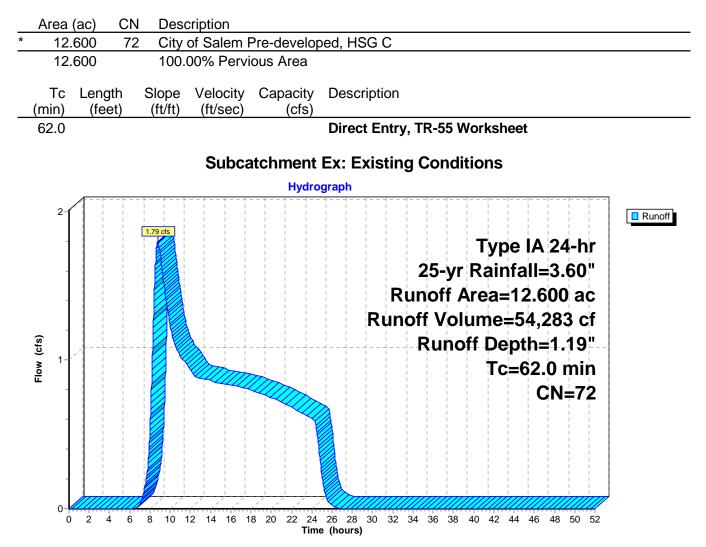
Subcatchment D: Developed Conditions



Summary for Subcatchment Ex: Existing Conditions

Runoff 1.79 cfs @ 8.76 hrs, Volume= 54,283 cf, Depth= 1.19" _

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-52.00 hrs, dt= 0.02 hrs Type IA 24-hr 25-yr Rainfall=3.60"



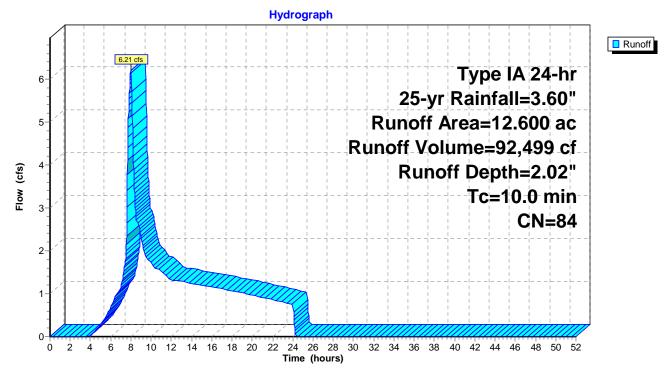
Summary for Subcatchment D: Developed Conditions

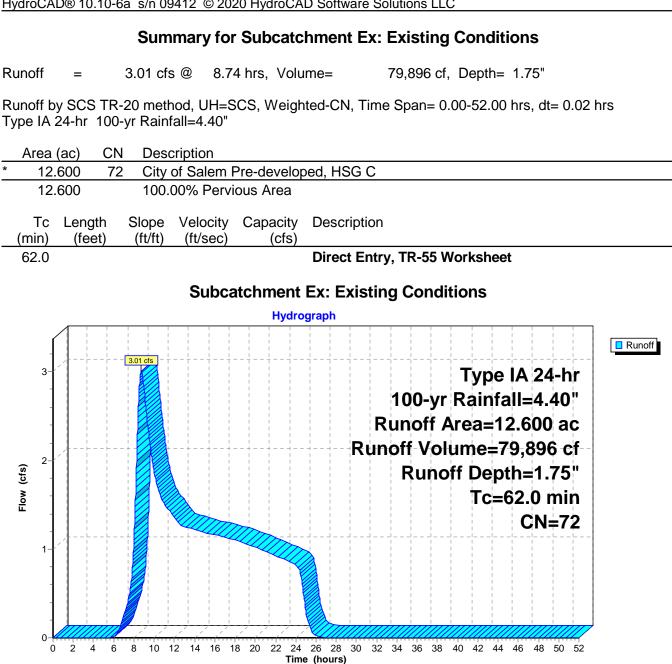
Runoff = 6.21 cfs @ 8.01 hrs, Volume= 92,499 cf, Depth= 2.02" Routed to nonexistent node CMH

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-52.00 hrs, dt= 0.02 hrs Type IA 24-hr 25-yr Rainfall=3.60"

	Area ((ac)	CN	Desc	cription			
	5.0	040	98	Pave	ed parking	HSG C		
	7.	560	74	>75%	% Grass co	over, Good,	, HSG C	
	12.6	600	84	Weig	ghted Aver	age		
	7.5	560		60.0	0% Pervio	us Area		
	5.040				40.00% Impervious Area			
(Tc Length S (min) (feet)		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
	10.0						Direct Entry, Assumed	

Subcatchment D: Developed Conditions





Runoff

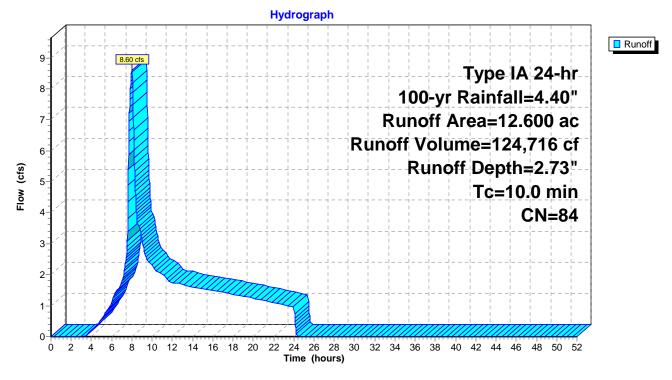
Summary for Subcatchment D: Developed Conditions

Runoff = 8.60 cfs @ 8.00 hrs, Volume= 124,716 cf, Depth= 2.73" Routed to nonexistent node CMH

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-52.00 hrs, dt= 0.02 hrs Type IA 24-hr 100-yr Rainfall=4.40"

Area	(ac)	CN	Desc	escription						
5	.040	98	Pave	ed parking,	HSG C					
7	.560	74	>75%	6 Grass co	over, Good,	, HSG C				
12	.600	84	Weig	ghted Aver	age					
7	.560		60.0	0% Pervio	us Area					
5	.040		40.0	40.00% Impervious Area						
Tc (min)	5		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
10.0						Direct Entry, Assumed				
Tc (min)	(min) (feet)		Slope	Velocity	Capacity					

Subcatchment D: Developed Conditions



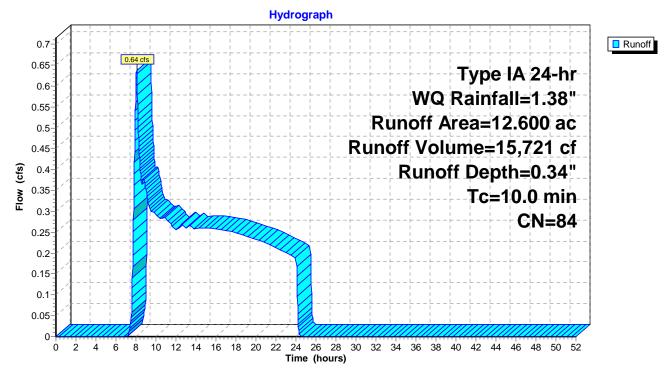
Summary for Subcatchment D: Developed Conditions

Runoff = 0.64 cfs @ 8.06 hrs, Volume= Routed to nonexistent node CMH 15,721 cf, Depth= 0.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-52.00 hrs, dt= 0.02 hrs Type IA 24-hr WQ Rainfall=1.38"

_	Area	(ac)	CN	Desc	cription		
	5.	040	98	Pave	ed parking,	HSG C	
_	7.	560	74	>75%	6 Grass co	over, Good,	, HSG C
	12.	600	84	Weig	ghted Aver	age	
	7.	560		60.00	0% Pervio	us Area	
	5.040 40.00% Impervious Area					vious Area	
_	Tc Length S (min) (feet)			Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0						Direct Entry, Assumed
_	7. 5. Tc (min)	560 040 Leng	th S	60.00 40.00	0% Pervio 0% Imperv Velocity	us Area vious Area Capacity	

Subcatchment D: Developed Conditions



Summary for Subcatchment Ex: Existing Conditions

Runoff = 0.09 cfs @ 20.87 hrs, Volume= 3,693 cf, Depth= 0.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-52.00 hrs, dt= 0.02 hrs Type IA 24-hr WQ Rainfall=1.38"

	Area	(ac)	CN	Desc	cription		
*	12.	2.600 72 City of Salem Pre-develop					ed, HSG C
	12.600		600 100.00% Pervious		ous Area		
	Tc (min)	Lengt (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	62.0	(100)	<u>.</u>	(1011)	(14000)	(010)	Direct Entry, TR-55 Worksheet

Subcatchment Ex: Existing Conditions

