

## **STRUCTURAL CALCULATION**

Project: **Market St Store**

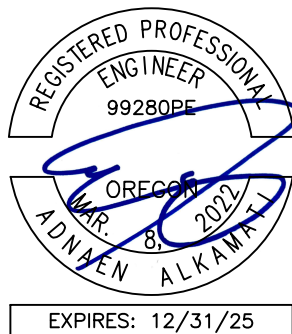
Re: **Design for Walls Openings**

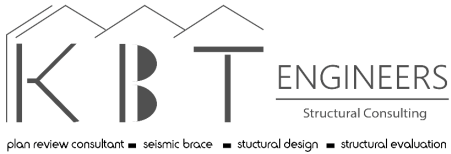
Client: **3170 Market St NE,  
Salem, OR**

Job No.: **24-1052**

Date: **Aug 25th , 2024**

Pages 1 thru 8 contain the calculations for the above-mentioned project located at Salem, OR. This set of calculations is based on the loads and assumptions stated within the set. If these loads and assumptions are different, this set should be revised. The adequacy of the existing structure is the responsibility of others.





JOB:	<u>3170 MARKET ST, SALEM</u>		
SHEET NO.:	_____	OF	_____
CALCULATED BY:	<u>AK2</u>	DATE	<u>7/2/24</u>
CHECKED BY:	_____	DATE	_____
PROJECT NO.:	<u>24-1052</u>		

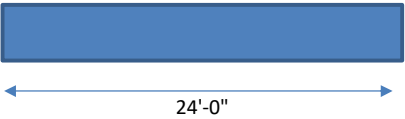
**Gravity Design :**

**BEAM 1 : (TRIB.= 10 ft)**

DL = 15 psf  
 SL = 25 psf

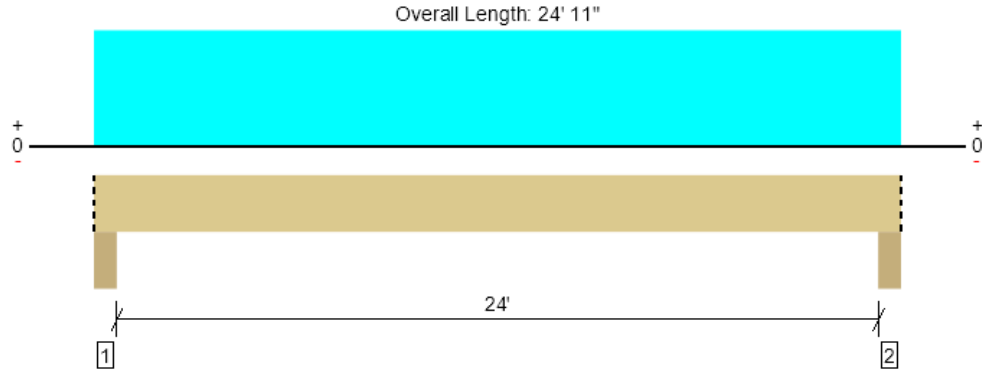
Use : 5 1/2" x 18" 24F-V4 DF Glulam

(SEE FORTE REPOT)



Level, Roof: Drop Beam

1 piece(s) 5 1/2" x 18" 24F-V4 DF Glulam



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal (typ.).

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	6280 @ 4"	19663 (5.50")	Passed (32%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	5293 @ 1' 11 1/2"	20114	Passed (26%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	37053 @ 12' 5 1/2"	64204	Passed (58%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.485 @ 12' 5 1/2"	1.212	Passed (L/600)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.815 @ 12' 5 1/2"	1.617	Passed (L/357)	--	1.0 D + 1.0 S (All Spans)

Member Length : 24' 11"  
System : Roof  
Member Type : Drop Beam  
Building Use : Residential  
Building Code : IBC 2021  
Design Methodology : ASD  
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume/size factor of 0.94 that was calculated using length L = 24' 3".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Column - DF	5.50"	5.50"	1.76"	2542	3738	6280	Blocking
2 - Column - DF	5.50"	5.50"	1.76"	2542	3738	6280	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	24' 11" o/c	
Bottom Edge (Lu)	24' 11" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 24' 11"	N/A	24.1	--	
1 - Uniform (PSF)	0 to 24' 11" (Front)	12'	15.0	25.0	Default Load

- Side loads are assumed to not induce cross-grain tension.

#### Weyerhaeuser Notes

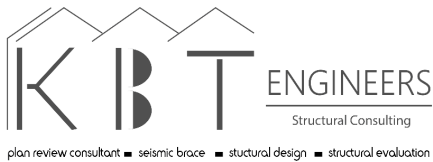
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
ADEL AL-KOMATI KBT ENGINEERS (845) 300-4738 Adel@kbtengineers.com	



7/3/2024 12:03:07 AM UTC  
ForteWEB v3.8, Engine: V8.4.1.22, Data: V8.1.6.2  
File Name: 24-1052

JOB: 3170 MARKET ST, SALEM

SHEET NO.: \_\_\_\_\_ OF \_\_\_\_\_

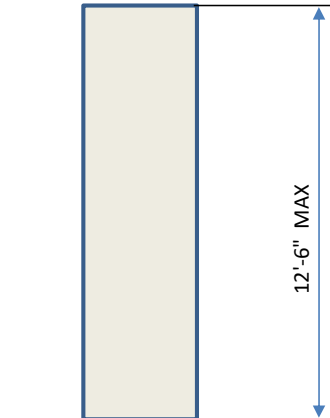
CALCULATE AK2 DATE 7/2/24

CHECKED BY: \_\_\_\_\_ DATE \_\_\_\_\_

PROJECT NO. 24-1052**Gravity Design :****POST :**Loads From Deck Beam :      Post Height = 12.5 ft

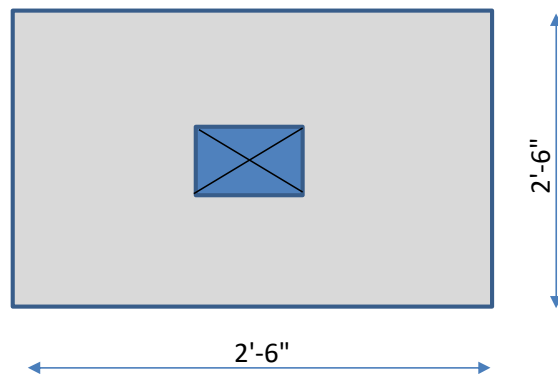
DL = 2542 lbs

SL = 3738 lbs

use: 6x6 DF#2 post  
(SEE ENERCALC REPOT)use: Simpson Moment Post Base Connection ABW66Z**OK****PAD FOOTING :**

DL = 2626 lbs

SL = 3738 lbs

use: 2'-6" X 2'-6" X 12" W/ (4) #4 Rebars Each Way .  
(SEE ENERCALC REPOT)

## Wood Column

Project File: foundation and post.ec6

LIC# : KW-06013368, Build:20.22.7.25

KBT ENGINEERS

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**DESCRIPTION: 6x6 POST**

### Code References

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16  
 Load Combinations Used : ASCE 7-16

### General Information

Analysis Method	Allowable Stress Design			Wood Section Name	6x6	
End Fixities	Top & Bottom Pinned			Wood Grading/Manuf.	Graded Lumber	
Overall Column Height	13 ft			Wood Member Type	Sawn	
( Used for non-slender calculations )						
Wood Species	Douglas Fir-Larch (North)			Exact Width	5.50 in	Allow Stress Modification Factors
Wood Grade	No. 1/No. 2			Exact Depth	5.50 in	Cf or Cv for Bending 1.0
Fb +	850 psi	Fv	180 psi	Area	30.250 in^2	Cf or Cv for Compression 1.0
Fb -	850 psi	Ft	500 psi	Ix	76.255 in^4	Cf or Cv for Tension 1.0
Fc - Prll	1400 psi	Density	30.59 pcf	Iy	76.255 in^4	Cm : Wet Use Factor 1.0
Fc - Perp	625 psi					Ct : Temperature Fact 1.0
E : Modulus of Elasticity . . .	x-x Bending	y-y Bending	Axial			Cfu : Flat Use Factor 1.0
	Basic	1600	1600	1600 ksi		Kf : Built-up columns 1.0 NDS 15.3.2
	Minimum	580	580			Use Cr : Repetitive ? No
Brace condition for deflection (buckling) along columns :						
				X-X (width) axis :	Unbraced Length for buckling ABOUT Y-Y Axis = 13 ft, k	
				Y-Y (depth) axis :	Unbraced Length for buckling ABOUT X-X Axis = 13 ft, k	

### Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Column self weight included : 83.538 lbs \* Dead Load Factor

AXIAL LOADS . . .

Roof drop beam: Axial Load at 13.0 ft, D = 2.542, S = 3.738 k

BENDING LOADS . . .

Lat. Point Load at 8.50 ft creating My-y, E = 0.1060 k

### DESIGN SUMMARY

Bending & Shear Check Results

<b>PASS</b> Max. Axial+Bending Stress Ratio =	<b>0.5435 : 1</b>	<b>Maximum SERVICE Lateral Load Reactions . .</b>	
Load Combination	+D+S	Top along Y-Y	0.0 k
Governing NDS Formula	Comp Only, fc/Fc'	Bottom along Y-Y	0.0 k
Location of max.above base	0.0 ft	Top along X-X	0.06931 k
At maximum location values are .		Bottom along X-X	0.03669 k
Applied Axial	6.364 k	<b>Maximum SERVICE Load Lateral Deflections . . .</b>	
Applied Mx	0.0 k-ft	Along Y-Y	0.0 in at 0.0 ft above base
Applied My	0.0 k-ft	for load combination : n/a	
Fc : Allowable	387.043 psi	Along X-X	0.06104 in at 7.067 ft above base
		for load combination : E Only	
<b>PASS</b> Maximum Shear Stress Ratio =	<b>0.008353 : 1</b>	<b>Other Factors used to calculate allowable stresses . . .</b>	
Load Combination	+D+0.70E	Bending	Compression
Location of max.above base	13.0 ft	Tension	
Applied Design Shear	2.406 psi		
Allowable Shear	288.0 psi		

### Load Combination Results

Load Combination	C <sub>D</sub>	C <sub>P</sub>	Maximum Axial + Bending Stress Ratios			Maximum Shear Ratios		
			Stress Ratio	Status	Location	Stress Ratio	Status	Location
D Only	0.900	0.301	0.2290	PASS	0.0 ft	0.0	PASS	13.0 ft
+D+S	1.150	0.240	0.5435	PASS	0.0 ft	0.0	PASS	13.0 ft
+D+0.750S	1.150	0.240	0.4637	PASS	0.0 ft	0.0	PASS	13.0 ft
+0.60D	1.600	0.176	0.1320	PASS	0.0 ft	0.0	PASS	13.0 ft
+D+0.70E	1.600	0.176	0.2199	PASS	0.0 ft	0.008353	PASS	13.0 ft
+D+0.750S+0.5250E	1.600	0.176	0.4548	PASS	0.0 ft	0.006265	PASS	13.0 ft
+0.60D+0.70E	1.600	0.176	0.1320	PASS	0.0 ft	0.008353	PASS	13.0 ft

# Wood Column

Project File: foundation and post.ec6

LIC# : KW-06013368, Build:20.22.7.25

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DESCRIPTION: 6x6 POST

## Maximum Reactions

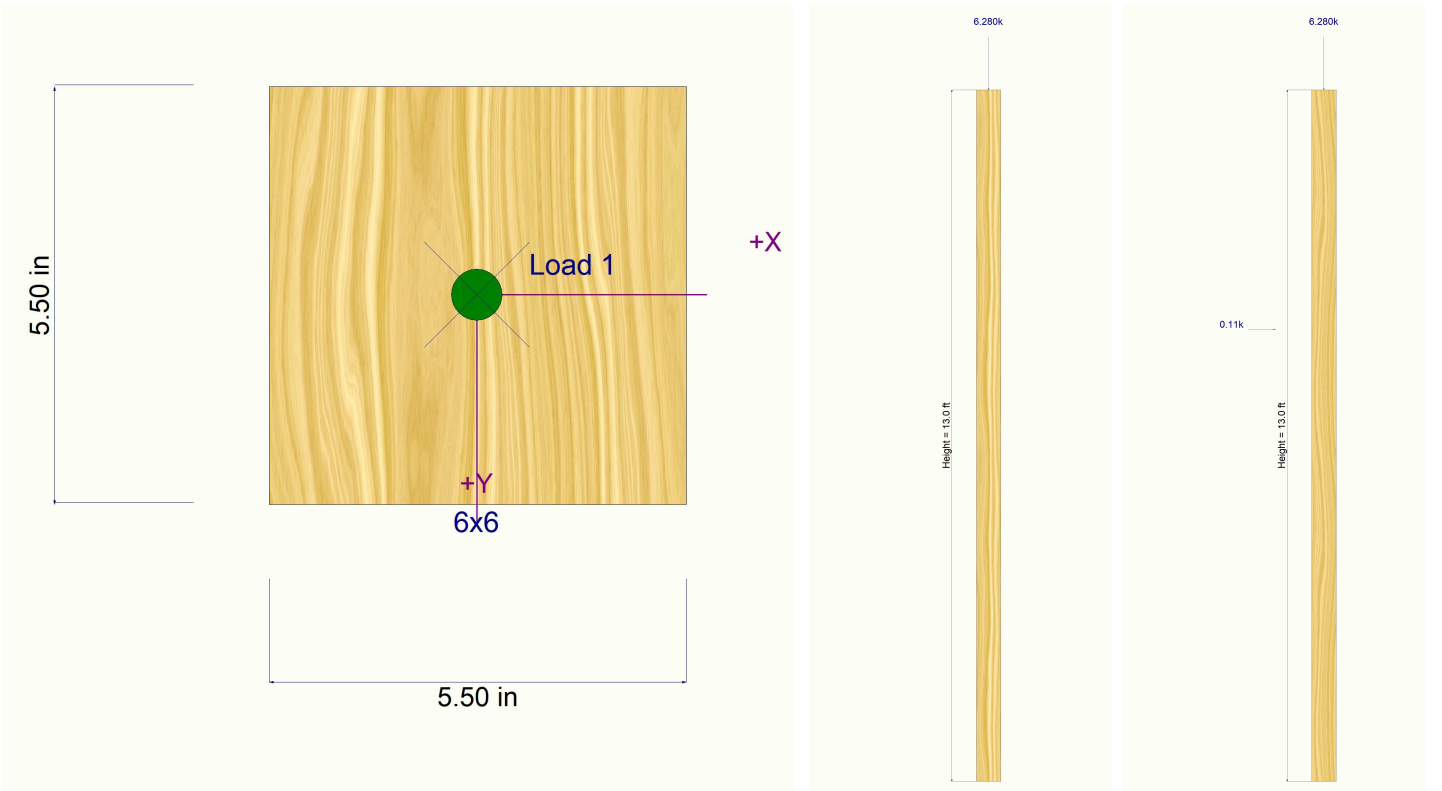
Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		k	Y-Y Axis Reaction		Axial Reaction	My - End Moments		k-ft	Mx - End Moments	
	@ Base	@ Top		@ Base	@ Top	@ Base	@ Base	@ Top		@ Base	@ Top
D Only						2.626					
+D+S						6.364					
+D+0.750S						5.429					
+0.60D						1.575					
+D+0.70E	0.026	0.049				2.626					
+D+0.750S+0.5250E	0.019	0.036				5.429					
+0.60D+0.70E	0.026	0.049				1.575					
S Only						3.738					
E Only	0.037	0.069									

## Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance
D Only	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+S	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+0.750S	0.0000 in	0.000ft	0.000 in	0.000 ft
+0.60D	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+0.70E	0.0427 in	7.067ft	0.000 in	0.000 ft
+D+0.750S+0.5250E	0.0320 in	7.067ft	0.000 in	0.000 ft
+0.60D+0.70E	0.0427 in	7.067ft	0.000 in	0.000 ft
S Only	0.0000 in	0.000ft	0.000 in	0.000 ft
E Only	0.0610 in	7.067ft	0.000 in	0.000 ft

## Sketches



## General Footing

Project File: foundation and post.ec6

LIC# : KW-06013368, Build:20.22.7.25

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### DESCRIPTION: PAD FOOTING

### Code References

Calculations per ACI 318-14, IBC 2018, CBC 2019, ASCE 7-16

Load Combinations Used : ASCE 7-16

### General Information

#### Material Properties

f'c : Concrete 28 day strength	=	3.0 ksi
fy : Rebar Yield	=	60.0 ksi
Ec : Concrete Elastic Modulus	=	3,122.0 ksi
Concrete Density	=	145.0 pcf
φ Values Flexure	=	0.90
Shear	=	0.750

#### Analysis Settings

Min Steel % Bending Reinf.	=	
Min Allow % Temp Reinf.	=	0.00180
Min. Overturning Safety Factor	=	1.0 : 1
Min. Sliding Safety Factor	=	1.0 : 1
Add Ftg Wt for Soil Pressure	:	Yes
Use ftg wt for stability, moments & shears	:	Yes
Add Pedestal Wt for Soil Pressure	:	No
Use Pedestal wt for stability, mom & shear	:	No

#### Soil Design Values

Allowable Soil Bearing	=	1.50 ksf
Soil Density	=	110.0 pcf
Increase Bearing By Footing Weight	=	No
Soil Passive Resistance (for Sliding)	=	250.0 pcf
Soil/Concrete Friction Coeff.	=	0.30

#### Increases based on footing Depth

Footing base depth below soil surface	=	ft
Allow press. increase per foot of depth	=	ksf
when footing base is below	=	ft

#### Increases based on footing plan dimension

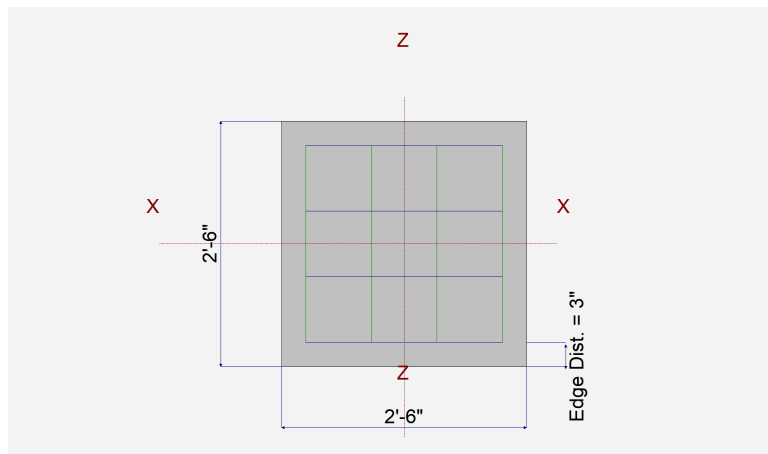
Allowable pressure increase per foot of depth	=	ksf
when max. length or width is greater than	=	ft

### Dimensions

Width parallel to X-X Axis	=	2.50 ft
Length parallel to Z-Z Axis	=	2.50 ft
Footing Thickness	=	12.0 in

#### Pedestal dimensions...

px : parallel to X-X Axis	=	in
pz : parallel to Z-Z Axis	=	in
Height	=	in
Rebar Centerline to Edge of Concrete...	=	3.0 in
at Bottom of footing	=	



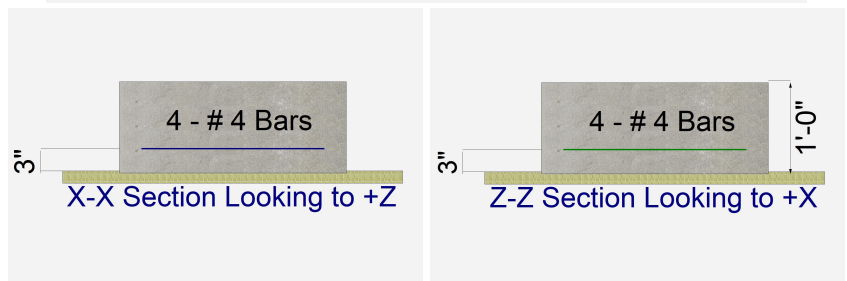
### Reinforcing

Bars parallel to X-X Axis	=	
Number of Bars	=	4
Reinforcing Bar Size	=	# 4

Bars parallel to Z-Z Axis	=	
Number of Bars	=	4.0
Reinforcing Bar Size	=	# 4

#### Bandwidth Distribution Check (ACI 15.4.4.2)

Direction Requiring Closer Separation	=	n/a
# Bars required within zone	=	n/a
# Bars required on each side of zone	=	n/a



### Applied Loads

	D	Lr	L	S	W	E	H
P : Column Load	=	2.626		3.738			k
OB : Overburden	=						ksf
M-xx	=						k-ft
M-zz	=					0.0	k-ft
V-x	=						k
V-z	=					0.0	k

## General Footing

Project File: foundation and post.ec6

LIC#: KW-06013368, Build:20.22.7.25

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### DESCRIPTION: PAD FOOTING

### DESIGN SUMMARY

Design OK

	Min. Ratio	Item	Applied	Capacity	Governing Load Combination
PASS	0.7753	Soil Bearing	1.163 ksf	1.50 ksf	+D+S about Z-Z axis
PASS	n/a	Overturning - X-X	0.0 k-ft	0.0 k-ft	No Overturning
PASS	n/a	Overturning - Z-Z	0.0 k-ft	0.0 k-ft	No Overturning
PASS	n/a	Sliding - X-X	0.0 k	0.0 k	No Sliding
PASS	n/a	Sliding - Z-Z	0.0 k	0.0 k	No Sliding
PASS	n/a	Uplift	0.0 k	0.0 k	No Uplift
PASS	0.09126	Z Flexure (+X)	1.142 k-ft/ft	12.508 k-ft/ft	+1.20D+1.60S
PASS	0.09126	Z Flexure (-X)	1.142 k-ft/ft	12.508 k-ft/ft	+1.20D+1.60S
PASS	0.09126	X Flexure (+Z)	1.142 k-ft/ft	12.508 k-ft/ft	+1.20D+1.60S
PASS	0.09126	X Flexure (-Z)	1.142 k-ft/ft	12.508 k-ft/ft	+1.20D+1.60S
PASS	0.08233	1-way Shear (+X)	6.764 psi	82.158 psi	+1.20D+1.60S
PASS	0.08233	1-way Shear (-X)	6.764 psi	82.158 psi	+1.20D+1.60S
PASS	0.08233	1-way Shear (+Z)	6.764 psi	82.158 psi	+1.20D+1.60S
PASS	0.08233	1-way Shear (-Z)	6.764 psi	82.158 psi	+1.20D+1.60S
PASS	0.1561	2-way Punching	25.649 psi	164.317 psi	+1.20D+1.60S

### Detailed Results

#### Soil Bearing

Rotation Axis & Load Combination...	Gross Allowable	Xecc		Zecc		Actual Soil Bearing Stress @ Location				Actual / Allow Ratio
				(in)		Bottom, -Z	Top, +Z	Left, -X	Right, +X	
X-X, D Only	1.50	n/a	0.0			0.5652	0.5652	n/a	n/a	0.377
X-X, +D+S	1.50	n/a	0.0			1.163	1.163	n/a	n/a	0.775
X-X, +D+0.750S	1.50	n/a	0.0			1.014	1.014	n/a	n/a	0.676
X-X, +0.60D	1.50	n/a	0.0			0.3391	0.3391	n/a	n/a	0.226
Z-Z, D Only	1.50	0.0	n/a			n/a	n/a	0.5652	0.5652	0.377
Z-Z, +D+S	1.50	0.0	n/a			n/a	n/a	1.163	1.163	0.775
Z-Z, +D+0.750S	1.50	0.0	n/a			n/a	n/a	1.014	1.014	0.676
Z-Z, +0.60D	1.50	0.0	n/a			n/a	n/a	0.3391	0.3391	0.226

#### Overturning Stability

Rotation Axis & Load Combination...	Overturning Moment	Resisting Moment	Stability Ratio	Status
Footing Has NO Overturning				

All units k

#### Sliding Stability

Force Application Axis Load Combination...	Sliding Force	Resisting Force	Stability Ratio	Status
Footing Has NO Sliding				

#### Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
X-X, +1.40D	0.4596	+Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +1.40D	0.4596	-Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +1.20D	0.3939	+Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +1.20D	0.3939	-Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +1.20D+0.50S	0.6275	+Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +1.20D+0.50S	0.6275	-Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +1.20D+1.60S	1.142	+Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +1.20D+1.60S	1.142	-Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +0.90D	0.2954	+Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +0.90D	0.2954	-Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +1.20D+0.20S	0.4874	+Z	Bottom	0.2592	AsMin	0.320	12.508	OK
X-X, +1.20D+0.20S	0.4874	-Z	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +1.40D	0.4596	-X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +1.40D	0.4596	+X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +1.20D	0.3939	-X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +1.20D	0.3939	+X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +1.20D+0.50S	0.6275	-X	Bottom	0.2592	AsMin	0.320	12.508	OK



## General Footing

Project File: foundation and post.ec6

LIC# : KW-06013368, Build:20.22.7.25

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### DESCRIPTION: PAD FOOTING

#### Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
Z-Z, +1.20D+0.50S	0.6275	+X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +1.20D+1.60S	1.142	-X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +1.20D+1.60S	1.142	+X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +0.90D	0.2954	-X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +0.90D	0.2954	+X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +1.20D+0.20S	0.4874	-X	Bottom	0.2592	AsMin	0.320	12.508	OK
Z-Z, +1.20D+0.20S	0.4874	+X	Bottom	0.2592	AsMin	0.320	12.508	OK

#### One Way Shear

Load Combination...	Vu @ -X	Vu @ +X	Vu @ -Z	Vu @ +Z	Vu:Max	Phi Vn	Vu / Phi*Vn	Status
+1.40D	2.72 psi	2.72 psi	2.72 psi	2.72 psi	2.72 psi	82.16 psi	0.03	OK
+1.20D	2.33 psi	2.33 psi	2.33 psi	2.33 psi	2.33 psi	82.16 psi	0.03	OK
+1.20D+0.50S	3.72 psi	3.72 psi	3.72 psi	3.72 psi	3.72 psi	82.16 psi	0.05	OK
+1.20D+1.60S	6.76 psi	6.76 psi	6.76 psi	6.76 psi	6.76 psi	82.16 psi	0.08	OK
+0.90D	1.75 psi	1.75 psi	1.75 psi	1.75 psi	1.75 psi	82.16 psi	0.02	OK
+1.20D+0.20S	2.89 psi	2.89 psi	2.89 psi	2.89 psi	2.89 psi	82.16 psi	0.04	OK

#### Two-Way "Punching" Shear

Load Combination...	Vu	Phi*Vn	Vu / Phi*Vn	Status
+1.40D	10.33 psi	164.32psi	0.06284	OK
+1.20D	8.85 psi	164.32psi	0.05386	OK
+1.20D+0.50S	14.10 psi	164.32psi	0.08581	OK
+1.20D+1.60S	25.65 psi	164.32psi	0.1561	OK
+0.90D	6.64 psi	164.32psi	0.0404	OK
+1.20D+0.20S	10.95 psi	164.32psi	0.06664	OK

All units k