

PRELIMINARY STORMWATER MANAGEMENT REPORT

FOR

MULTIFAMILY DEVELOPMENT

At

3021 & 3027 D STREET NE

SALEM, OR. 97301

August 21st, 2024



PREPARED BY:

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I. PURPOSE OF REPORT

This report describes the proposed improvements compliance with the City of Salem Stormwater Design Handbook for Developers and Large Projects.

II. PROJECT DESCRIPTION

The site is located at 3021 & 3027 D Street NE in the City of Salem. The property is bordered by D Street NE to the south with private property to the west and north.

A. EXISTING CONDITION

The existing site is currently vacant with a portion of grass and an existing driveway made of concrete. Gravel can also be found on a portion of the site just east of the existing properties. The northeast portion of the site was found to have higher elevations which then slopes toward the northwest portion of the site. South of this portion of the site, is generally flat but slopes slightly towards the south.

The existing site is not located within a FEMA flood zone overlay per FIRM Map 41047C0375G, effective 1/19/2000.

B. PROPOSED CONDITION

The proposed development will be a new 3-story 12-unit multifamily building, with a proposed parking lot and proposed stormwater infrastructure. Where the parking lot is located, the draining pattern will generally remain the same, draining from the northeast portion of the lot to the west where the proposed rain garden will be located.

In the northeastern section of the site, there will be a parking lot that slopes downward toward the north, directing runoff into the bioswale. Simultaneously, the northwestern portion of the site will slope into the rain garden. The proposed rain garden and bioswale serve to address the site's zero-infiltration rate, as indicated in the Geotechnical Report (Branch Engineering Project No. 24-1447). Any excess water from the rain garden and bioswale will flow to the curb along D Street NE. Importantly, the total post-development flow rate will not exceed the predevelopment flow rate.

There is existing runoff from the adjacent development, and although the proposed combination swale is not sized for the existing development, the overflow conveyance system has been sized to anticipate the small amount of runoff.

Geotechnical Report:

Branch Engineering, dated May 22, 2024
Project No. 24-1447

Infiltration Rates:

Table 1: Infiltration Test Results

<i>Test ID</i>	<i>Soil Description</i>	<i>Test Depth (inches)</i>	<i>Infiltration Rate (in/hr)</i>
IT-1	Light Brown - Clayey Silt (ML/CL)	56	0
IT-2	Light Brown - Clayey Silt (ML/CL)	58	0

Groundwater:

Groundwater was not encountered at the explored depth of 7-feet. One well log Mari 66067 showed no groundwater to a depth of 22-feet.

III. METHODOLOGY

The City of Salem's stormwater design handbook for developers and large projects, and Chapter 71 of the Salem Revised Code (SRC) require the following;

Flow Control Requirements

- Stormwater detention facilities must be designed such that the post-development peak runoff rate is equal to or less than the pre-development peak runoff rate for half of the 2-year, 24-hour storm and the 10-year, 24-hour storm, 25-year and 100-year 24-hour storm event.
- The detention volume for a volume-based stormwater flow control facility (such as dry detention basin) shall be sufficient to detain a 100-year design storm event without overflow.

Water Quality Treatment Requirements

- Stormwater treatment facilities must be designed to treat 80% of the average annual rainfall using the water quality design storm event of 1.38 inches in 24 hours.

GSI Requirements

The City of Salem requires large projects to apply GIS to the maximum extent feasible (MEF). The MEF requirements are;

- The total area of the site covered by GSI facilities is at least 10 percent of the combined amount of new plus replaced impervious surfaces on the entire site or;
- GSI is used to fully mitigate the impacts of stormwater runoff from at least 80 percent of the total new plus replaced impervious surfaces.

The proposed development will utilize an infiltration rain garden to mitigate 80 percent of the total new impervious surface area.

IV. CALCULATIONS

The development will be designed in accordance with the Design Standards in Division 004, Appendix D. The Santa Barbara Urban Hydrograph (SBUH) method will be the selected methodology used in the computer program HydroCAD Version 10.20. The following parameters were inputted;

Storm Type: Type 1A Rainfall Distribution

Soil Group: Group C

Curve Number:

Land Cover Category	Curve Numbers for Hydrologic Soil Group			
	A	B	C	D
Impervious Surface	98	98	98	98
Pervious Land Cover				
Pre-developed	35	58	72	79
Unamended Soils	72	82	87	89
Amended Soils	39	61	74	80

Rainfall Depth:

24-hour Rainfall Depths for Salem	
Design Storm Event	Precipitation (inches/24 hours)
WQ Event	1.38
2-year	2.20
10-year	3.20
100-year	4.40

The 25-year 24-hour storm event precipitation is 3.6 in/24 hr per PWDS Table 4D-3

V. SUMMARY

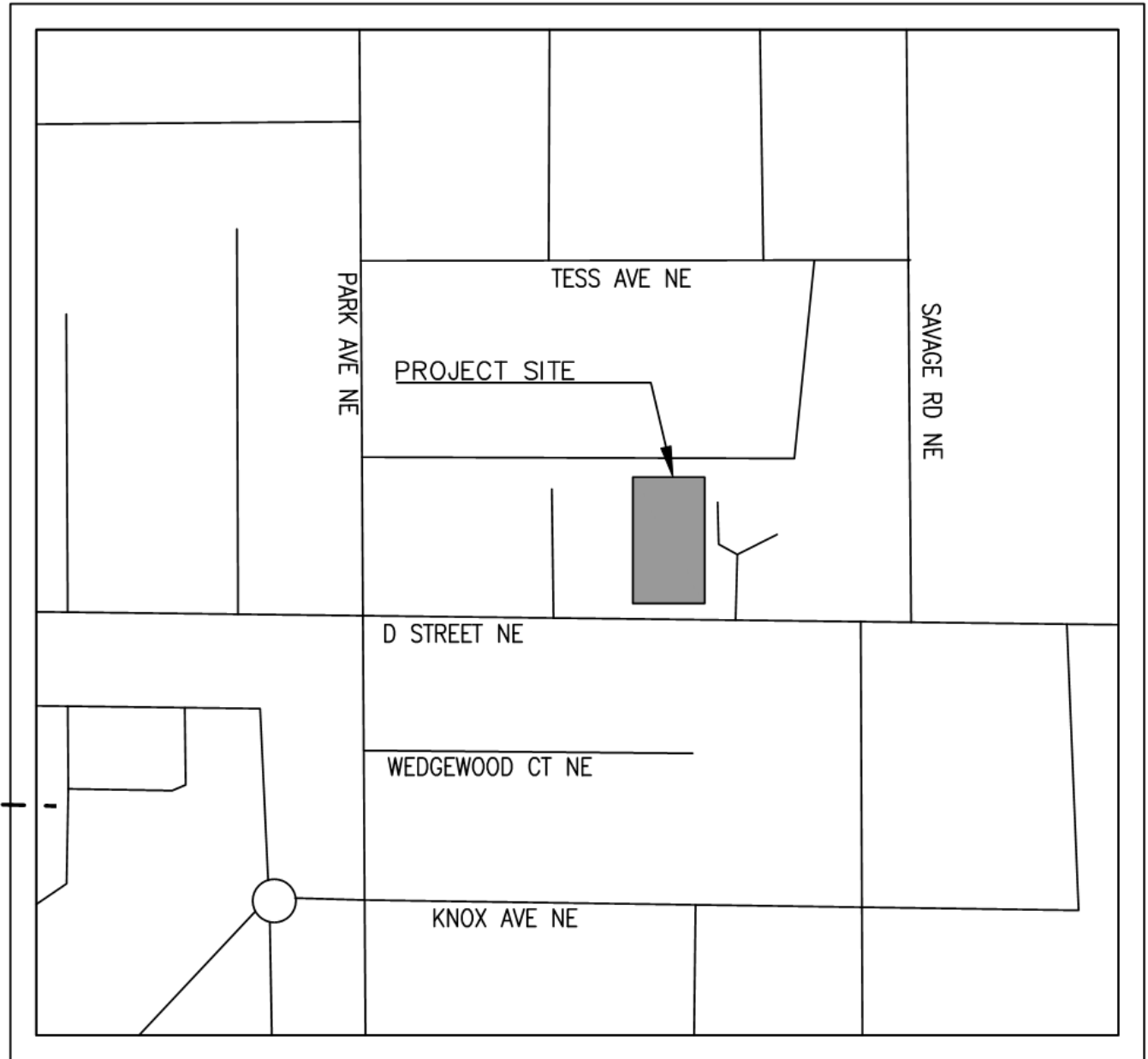
The proposed development will implement a combination swale per City Std. No. 219 at the northwest corner of the site. A low flow pipe has been designed, with an orifice control, to reduce the post development flow rate to not exceed the pre development flow rate, as demonstrated below. The combination swale has been sized with a bottom surface area of 700 square feet.

Lastly, the GSI combination swale has been sized to properly treat the Water Quality Storm Event of 1.38 in/hr. The tables below provide the summary of calculations derived using HydroCAD. Please refer to the Appendix for the complete calculations.

ENGINEERED METHOD SUMMARY										
PRE VS. POST CONSTRUCTION FLOW RATES										
FACILITY ID	PEAK FLOW RATE (CFS)									
	HALF OF THE 2 YEAR STORM		5 YEAR STORM		10 YEAR STORM		25 YEAR STORM		100 YEAR STORM	
PROJECT SITE	PRE	POST	PRE	POST	PRE	POST	PRE	POST	PRE	POST
A	0.1	0.08	0.16	0.09	0.2	0.09	0.25	0.1	0.34	0.27

CATCHMENT AND FACILITY TABLE			
AREA	TOTAL AREA (SF)/(AC.)	IMPERVIOUS AREA (SF)	PERVIOUS AREA (SF)
A	19,553	13,687	5,866

APPENDIX A – MAPS

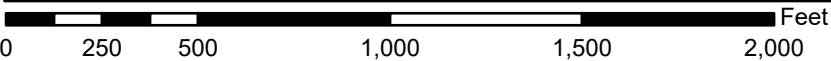
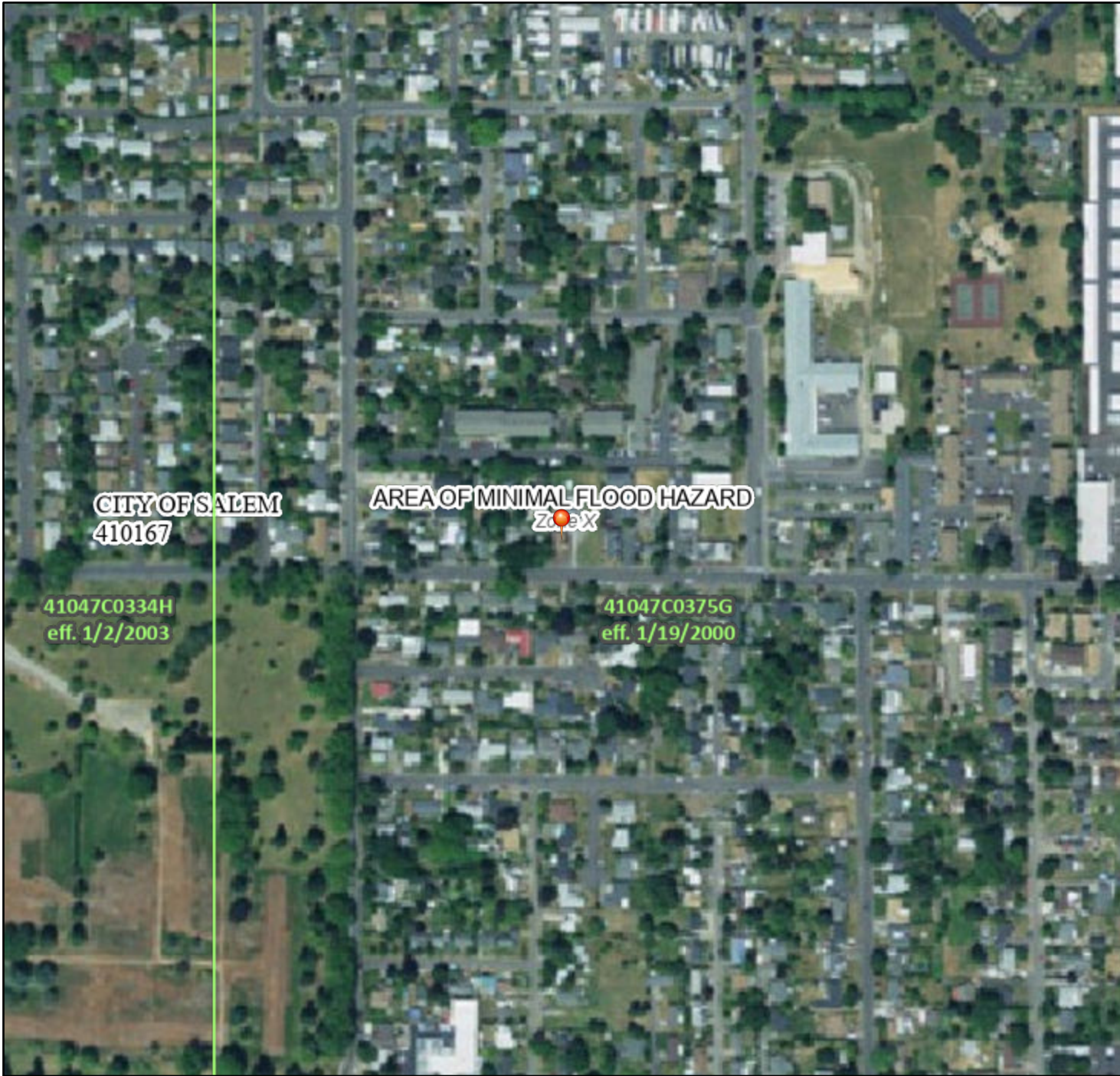


VICINITY MAP
NOT TO SCALE

National Flood Hazard Layer FIRMMette



123°0'11"W 44°56'50"N



1:6,000

122°59'34"W 44°56'25"N

Basemap Imagery Source: USGS National Map 2023

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
		Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
		Area of Undetermined Flood Hazard Zone D
GENERAL STRUCTURES		Channel, Culvert, or Storm Sewer
		Levee, Dike, or Floodwall
OTHER FEATURES		20.2 Cross Sections with 1% Annual Chance Water Surface Elevation
		17.5 Cross Sections with 1% Annual Chance Water Surface Elevation
		Coastal Transect
		Base Flood Elevation Line (BFE)
		Limit of Study
		Jurisdiction Boundary
		Coastal Transect Baseline
MAP PANELS		Digital Data Available
		No Digital Data Available
		Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

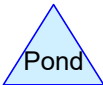
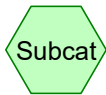
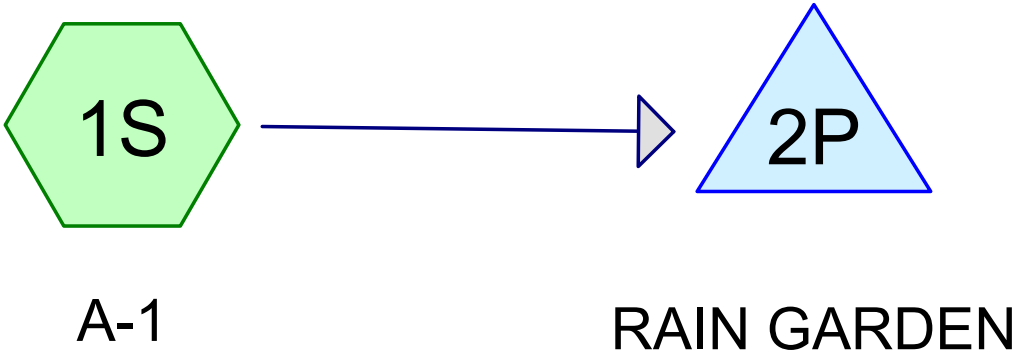
The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 7/23/2024 at 6:30 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

APPENDIX B – CALCULATIONS

POST DEVELOPMENT HYDROCAD

THE ELEVATIONS SHOWN HEREIN ARE ARBITRARY AND USED FOR CALCULATION PURPOSES ONLY



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Rainfall Events Listing

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-Yr	Type IA 24-hr		Default	24.00	1	2.20	2
2	5-Yr	Type IA 24-hr		Default	24.00	1	2.80	2
3	10-Yr	Type IA 24-hr		Default	24.00	1	3.20	2
4	25-Yr	Type IA 24-hr		Default	24.00	1	3.60	2
5	100-Yr	Type IA 24-hr		Default	24.00	1	4.40	2
6	WQV	Type IA 24-hr		Default	24.00	1	1.38	2

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.135	86	<50% Grass cover, Poor, HSG C (1S)
0.314	98	Paved parking, HSG C (1S)
0.449	94	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
0.449	HSG C	1S
0.000	HSG D	
0.000	Other	
0.449		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	0.135	0.000	0.000	0.135	<50% Grass cover, Poor	1S
0.000	0.000	0.314	0.000	0.000	0.314	Paved parking	1S
0.000	0.000	0.449	0.000	0.000	0.449	TOTAL AREA	

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Pipe Listing (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)	Node Name
1	2P	203.18	203.17	2.0	0.0050	0.013	0.0	4.0	0.0	
2	2P	203.18	203.17	2.0	0.0050	0.013	0.0	1.5	0.0	

Post_Development_00330*Type IA 24-hr 2-Yr Rainfall=2.20"*

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Time span=0.01-40.00 hrs, dt=0.05 hrs, 801 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: A-1Runoff Area=19,553 sf 70.00% Impervious Runoff Depth=1.58"
Flow Length=175' Tc=5.0 min CN=94 Runoff=0.19 cfs 0.059 af**Pond 2P: RAIN GARDEN**Peak Elev=205.04' Storage=339 cf Inflow=0.19 cfs 0.059 af
Outflow=0.08 cfs 0.059 af**Total Runoff Area = 0.449 ac Runoff Volume = 0.059 af Average Runoff Depth = 1.58"**
30.00% Pervious = 0.135 ac 70.00% Impervious = 0.314 ac

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Type IA 24-hr 2-Yr Rainfall=2.20"

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Summary for Subcatchment 1S: A-1

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.19 cfs @ 7.90 hrs, Volume= 0.059 af, Depth= 1.58"
Routed to Pond 2P : RAIN GARDEN

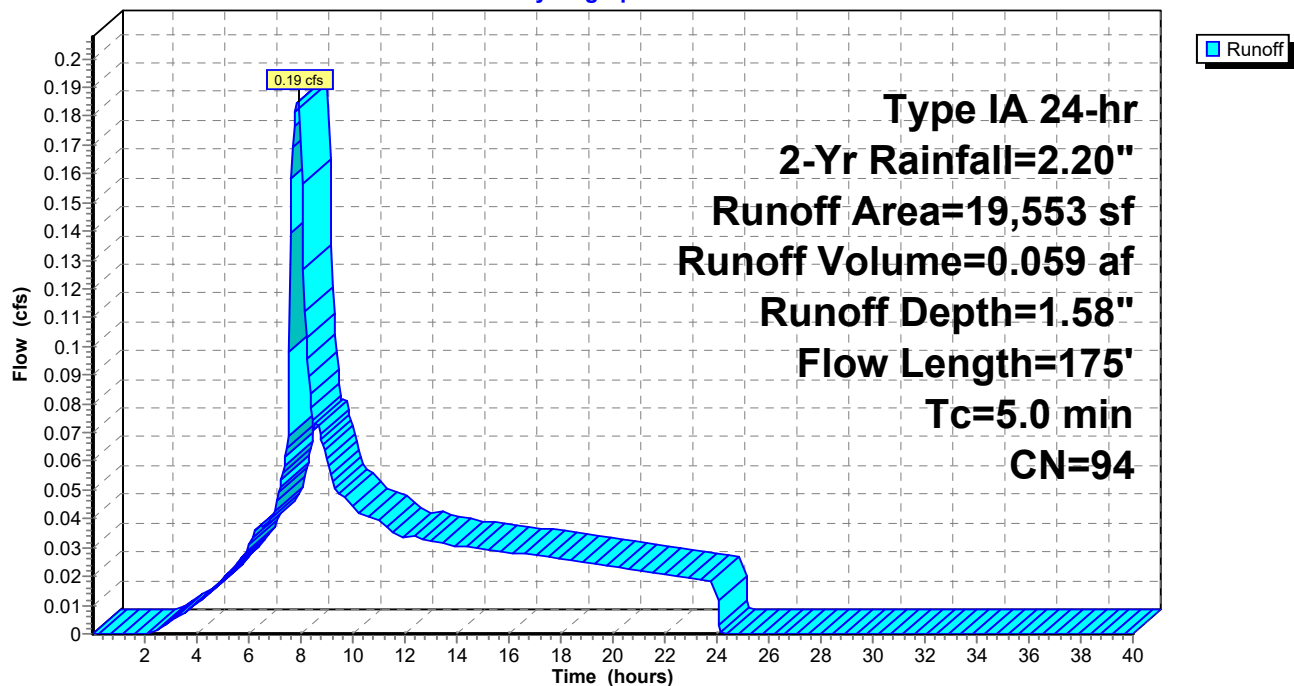
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-40.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 2-Yr Rainfall=2.20"

Area (sf)	CN	Description
13,687	98	Paved parking, HSG C
5,866	86	<50% Grass cover, Poor, HSG C
19,553	94	Weighted Average
5,866	86	30.00% Pervious Area
13,687	98	70.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	175		0.58		Direct Entry,

Subcatchment 1S: A-1

Hydrograph



Post_Development_00330

Type IA 24-hr 2-Yr Rainfall=2.20"

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Summary for Pond 2P: RAIN GARDEN

Inflow Area = 0.449 ac, 70.00% Impervious, Inflow Depth = 1.58" for 2-Yr event
 Inflow = 0.19 cfs @ 7.90 hrs, Volume= 0.059 af
 Outflow = 0.08 cfs @ 8.40 hrs, Volume= 0.059 af, Atten= 57%, Lag= 30.2 min
 Primary = 0.08 cfs @ 8.40 hrs, Volume= 0.059 af

Routing by Stor-Ind method, Time Span= 0.01-40.01 hrs, dt= 0.05 hrs / 2

Peak Elev= 205.04' @ 8.40 hrs Surf.Area= 700 sf Storage= 339 cf

Flood Elev= 206.34' Surf.Area= 700 sf Storage= 1,057 cf

Plug-Flow detention time= 47.4 min calculated for 0.059 af (100% of inflow)

Center-of-Mass det. time= 48.0 min (781.8 - 733.7)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.18'	1,057 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.18	700	157.0	0.0	0	0	700
203.68	700	157.0	30.0	105	105	779
203.93	700	157.0	0.0	0	105	818
205.43	700	157.0	30.0	315	420	1,053
206.18	700	157.0	100.0	525	945	1,171
206.34	700	157.0	100.0	112	1,057	1,196

Device	Routing	Invert	Outlet Devices	
#1	Device 2	206.18'	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads	
#2	Primary	203.18'	4.0" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 ' /' Cc= 0.900 n= 0.013, Flow Area= 0.09 sf	
#3	Device 2	203.18'	1.5" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 ' /' Cc= 0.900 n= 0.013, Flow Area= 0.01 sf	

Primary OutFlow Max=0.08 cfs @ 8.40 hrs HW=205.04' (Free Discharge)

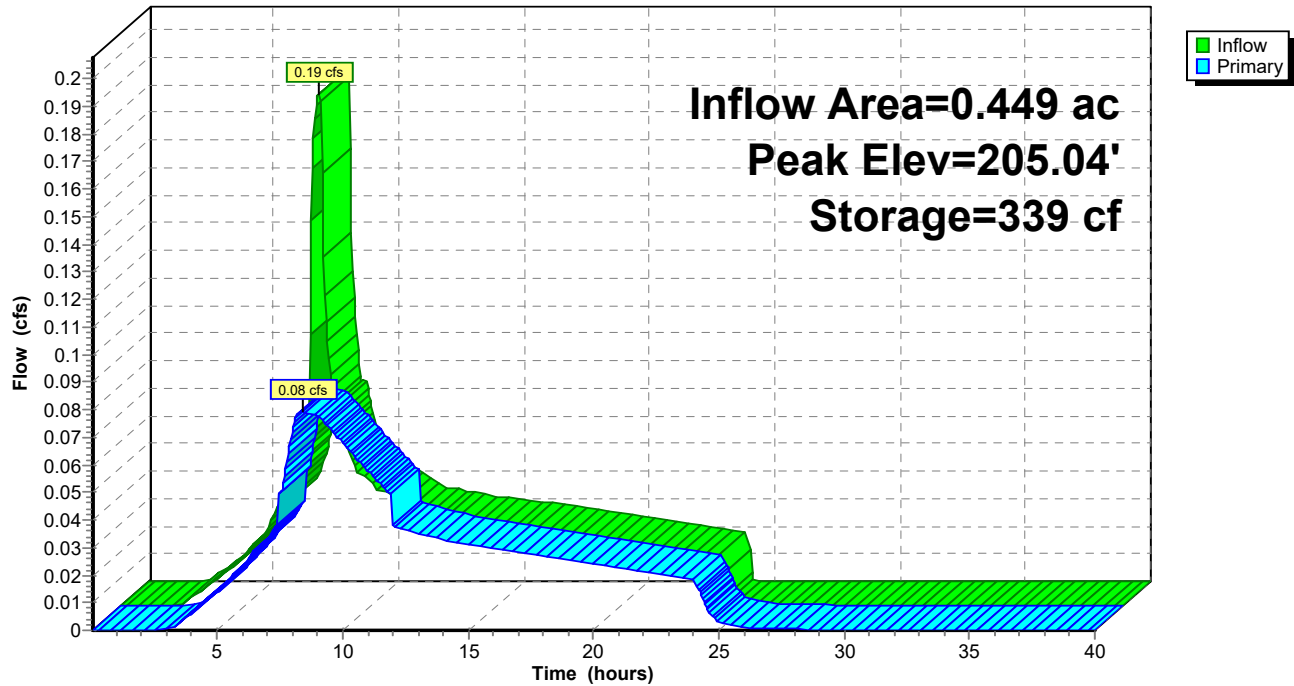
2=Culvert (Passes 0.08 cfs of 0.55 cfs potential flow)

1=Orifice/Grate (Controls 0.00 cfs)

3=Culvert (Inlet Controls 0.08 cfs @ 6.46 fps)

Pond 2P: RAIN GARDEN

Hydrograph



Post_Development_00330*Type IA 24-hr 5-Yr Rainfall=2.80"*

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Time span=0.01-40.00 hrs, dt=0.05 hrs, 801 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: A-1

Runoff Area=19,553 sf 70.00% Impervious Runoff Depth=2.16"

Flow Length=175' Tc=5.0 min CN=94 Runoff=0.25 cfs 0.081 af

Pond 2P: RAIN GARDEN

Peak Elev=205.58' Storage=528 cf Inflow=0.25 cfs 0.081 af

Outflow=0.09 cfs 0.081 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.081 af Average Runoff Depth = 2.16"
30.00% Pervious = 0.135 ac 70.00% Impervious = 0.314 ac

Post_Development_00330

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Type IA 24-hr 5-Yr Rainfall=2.80"

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Summary for Subcatchment 1S: A-1

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.25 cfs @ 7.89 hrs, Volume= 0.081 af, Depth= 2.16"
Routed to Pond 2P : RAIN GARDEN

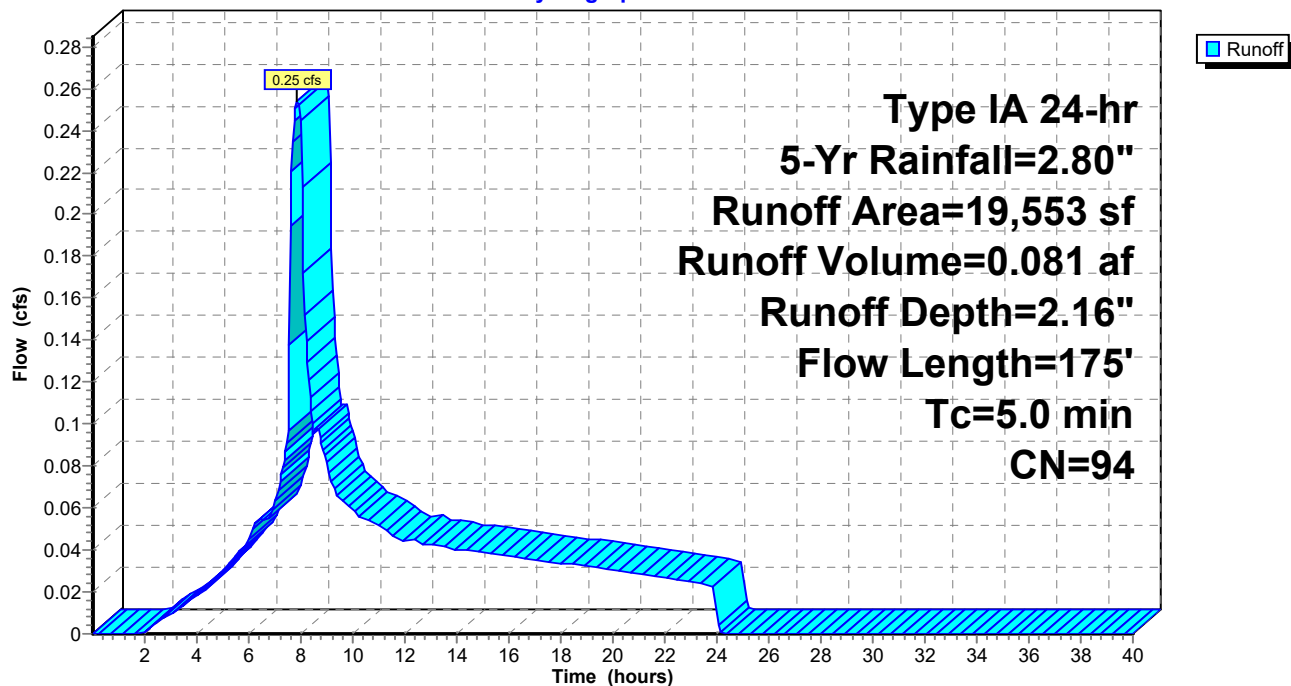
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-40.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 5-Yr Rainfall=2.80"

Area (sf)	CN	Description
13,687	98	Paved parking, HSG C
5,866	86	<50% Grass cover, Poor, HSG C
19,553	94	Weighted Average
5,866	86	30.00% Pervious Area
13,687	98	70.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	175		0.58		Direct Entry,

Subcatchment 1S: A-1

Hydrograph



Post_Development_00330

Type IA 24-hr 5-Yr Rainfall=2.80"

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Summary for Pond 2P: RAIN GARDEN

Inflow Area = 0.449 ac, 70.00% Impervious, Inflow Depth = 2.16" for 5-Yr event
 Inflow = 0.25 cfs @ 7.89 hrs, Volume= 0.081 af
 Outflow = 0.09 cfs @ 8.81 hrs, Volume= 0.081 af, Atten= 64%, Lag= 55.5 min
 Primary = 0.09 cfs @ 8.81 hrs, Volume= 0.081 af

Routing by Stor-Ind method, Time Span= 0.01-40.01 hrs, dt= 0.05 hrs / 2

Peak Elev= 205.58' @ 8.81 hrs Surf.Area= 700 sf Storage= 528 cf

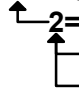
Flood Elev= 206.34' Surf.Area= 700 sf Storage= 1,057 cf

Plug-Flow detention time= 57.7 min calculated for 0.081 af (100% of inflow)

Center-of-Mass det. time= 57.9 min (776.3 - 718.4)

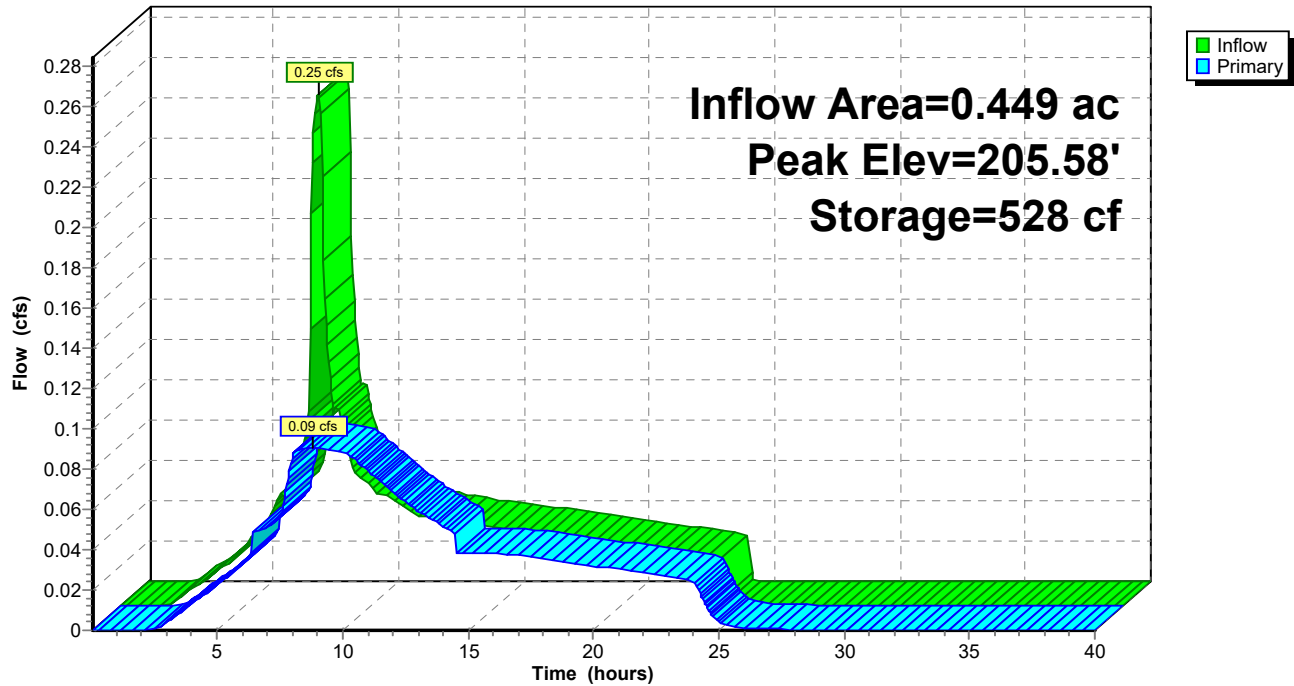
Volume	Invert	Avail.Storage	Storage Description			
#1	203.18'	1,057 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.18	700	157.0	0.0	0	0	700
203.68	700	157.0	30.0	105	105	779
203.93	700	157.0	0.0	0	105	818
205.43	700	157.0	30.0	315	420	1,053
206.18	700	157.0	100.0	525	945	1,171
206.34	700	157.0	100.0	112	1,057	1,196

Device	Routing	Invert	Outlet Devices	
#1	Device 2	206.18'	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads	
#2	Primary	203.18'	4.0" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.09 sf	
#3	Device 2	203.18'	1.5" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.01 sf	

Primary OutFlow Max=0.09 cfs @ 8.81 hrs HW=205.58' (Free Discharge)

2=Culvert (Passes 0.09 cfs of 0.63 cfs potential flow)
1=Orifice/Grate (Controls 0.00 cfs)**3=Culvert** (Inlet Controls 0.09 cfs @ 7.37 fps)

Pond 2P: RAIN GARDEN

Hydrograph



Post_Development_00330*Type IA 24-hr 10-Yr Rainfall=3.20"*

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Time span=0.01-40.00 hrs, dt=0.05 hrs, 801 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: A-1

Runoff Area=19,553 sf 70.00% Impervious Runoff Depth=2.54"

Flow Length=175' Tc=5.0 min CN=94 Runoff=0.30 cfs 0.095 af

Pond 2P: RAIN GARDEN

Peak Elev=205.82' Storage=694 cf Inflow=0.30 cfs 0.095 af

Outflow=0.09 cfs 0.095 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.095 af Average Runoff Depth = 2.54"
30.00% Pervious = 0.135 ac 70.00% Impervious = 0.314 ac

Post_Development_00330

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Type IA 24-hr 10-Yr Rainfall=3.20"

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Summary for Subcatchment 1S: A-1

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.30 cfs @ 7.88 hrs, Volume= 0.095 af, Depth= 2.54"
Routed to Pond 2P : RAIN GARDEN

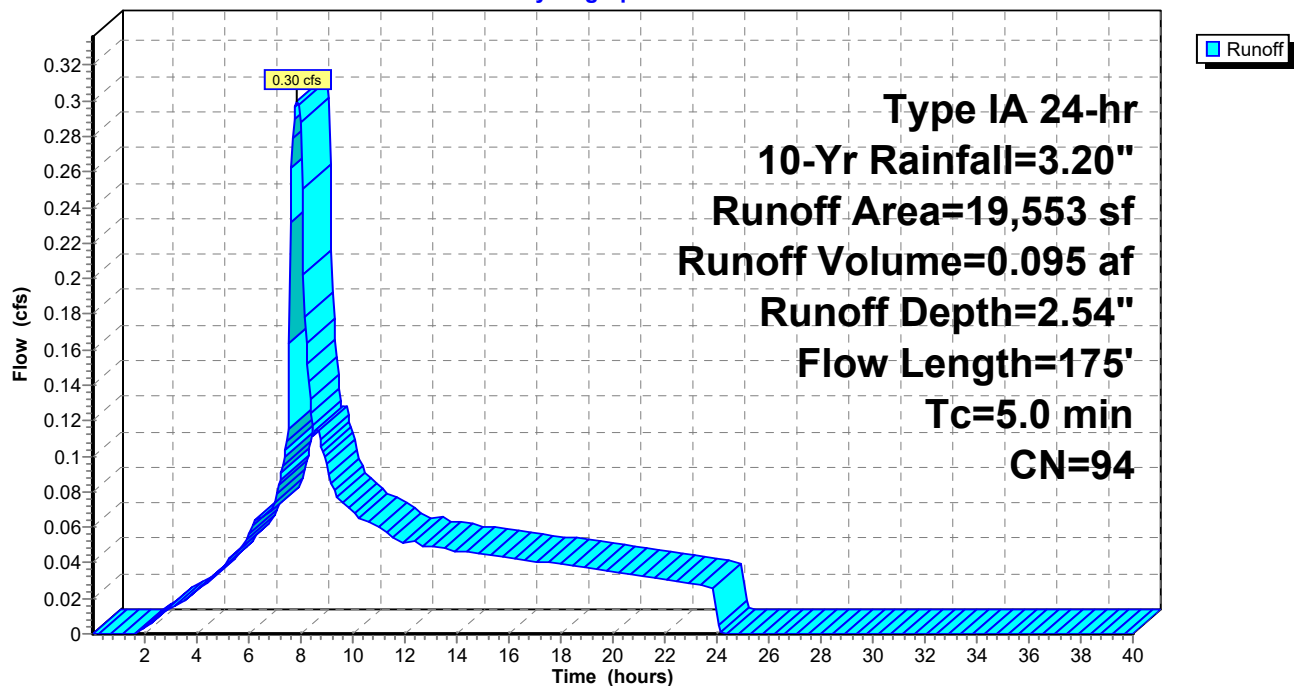
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-40.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 10-Yr Rainfall=3.20"

Area (sf)	CN	Description
13,687	98	Paved parking, HSG C
5,866	86	<50% Grass cover, Poor, HSG C
19,553	94	Weighted Average
5,866	86	30.00% Pervious Area
13,687	98	70.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	175		0.58		Direct Entry,

Subcatchment 1S: A-1

Hydrograph



Post_Development_00330

Type IA 24-hr 10-Yr Rainfall=3.20"

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Summary for Pond 2P: RAIN GARDEN

Inflow Area = 0.449 ac, 70.00% Impervious, Inflow Depth = 2.54" for 10-Yr event
 Inflow = 0.30 cfs @ 7.88 hrs, Volume= 0.095 af
 Outflow = 0.09 cfs @ 8.99 hrs, Volume= 0.095 af, Atten= 68%, Lag= 66.7 min
 Primary = 0.09 cfs @ 8.99 hrs, Volume= 0.095 af

Routing by Stor-Ind method, Time Span= 0.01-40.01 hrs, dt= 0.05 hrs / 2

Peak Elev= 205.82' @ 8.99 hrs Surf.Area= 700 sf Storage= 694 cf

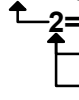
Flood Elev= 206.34' Surf.Area= 700 sf Storage= 1,057 cf

Plug-Flow detention time= 69.1 min calculated for 0.095 af (100% of inflow)

Center-of-Mass det. time= 68.1 min (778.8 - 710.7)

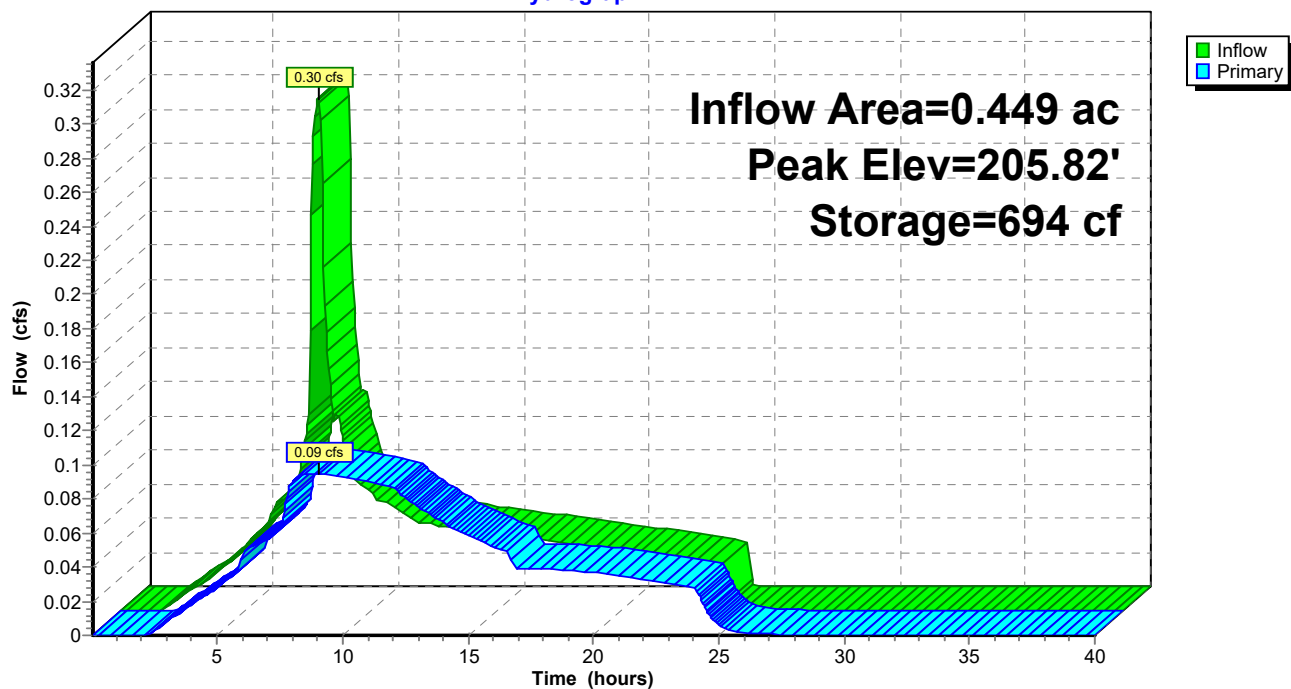
Volume	Invert	Avail.Storage	Storage Description			
#1	203.18'	1,057 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.18	700	157.0	0.0	0	0	700
203.68	700	157.0	30.0	105	105	779
203.93	700	157.0	0.0	0	105	818
205.43	700	157.0	30.0	315	420	1,053
206.18	700	157.0	100.0	525	945	1,171
206.34	700	157.0	100.0	112	1,057	1,196

Device	Routing	Invert	Outlet Devices	
#1	Device 2	206.18'	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads	
#2	Primary	203.18'	4.0" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.09 sf	
#3	Device 2	203.18'	1.5" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.01 sf	

Primary OutFlow Max=0.09 cfs @ 8.99 hrs HW=205.82' (Free Discharge)

2=Culvert (Passes 0.09 cfs of 0.66 cfs potential flow)
1=Orifice/Grate (Controls 0.00 cfs)**3=Culvert** (Inlet Controls 0.09 cfs @ 7.73 fps)

Pond 2P: RAIN GARDEN

Hydrograph



Post_Development_00330*Type IA 24-hr 25-Yr Rainfall=3.60"*

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Time span=0.01-40.00 hrs, dt=0.05 hrs, 801 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: A-1

Runoff Area=19,553 sf 70.00% Impervious Runoff Depth=2.93"

Flow Length=175' Tc=5.0 min CN=94 Runoff=0.35 cfs 0.110 af

Pond 2P: RAIN GARDEN

Peak Elev=206.08' Storage=874 cf Inflow=0.35 cfs 0.110 af

Outflow=0.10 cfs 0.110 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.110 af Average Runoff Depth = 2.93"
30.00% Pervious = 0.135 ac 70.00% Impervious = 0.314 ac

Post_Development_00330

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Type IA 24-hr 25-Yr Rainfall=3.60"

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Summary for Subcatchment 1S: A-1

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.35 cfs @ 7.88 hrs, Volume= 0.110 af, Depth= 2.93"
Routed to Pond 2P : RAIN GARDEN

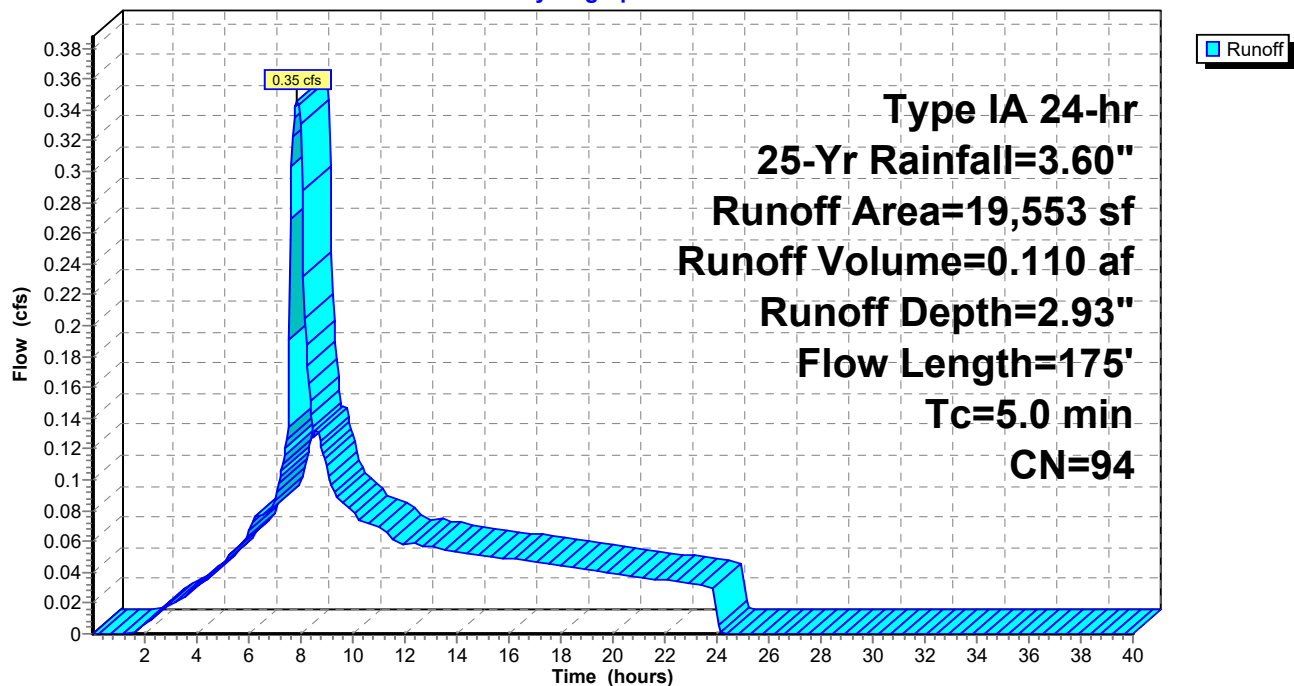
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-40.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 25-Yr Rainfall=3.60"

Area (sf)	CN	Description
13,687	98	Paved parking, HSG C
5,866	86	<50% Grass cover, Poor, HSG C
19,553	94	Weighted Average
5,866	86	30.00% Pervious Area
13,687	98	70.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	175		0.58		Direct Entry,

Subcatchment 1S: A-1

Hydrograph



Post_Development_00330

Type IA 24-hr 25-Yr Rainfall=3.60"

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Summary for Pond 2P: RAIN GARDEN

Inflow Area = 0.449 ac, 70.00% Impervious, Inflow Depth = 2.93" for 25-Yr event
 Inflow = 0.35 cfs @ 7.88 hrs, Volume= 0.110 af
 Outflow = 0.10 cfs @ 9.13 hrs, Volume= 0.110 af, Atten= 71%, Lag= 75.2 min
 Primary = 0.10 cfs @ 9.13 hrs, Volume= 0.110 af

Routing by Stor-Ind method, Time Span= 0.01-40.01 hrs, dt= 0.05 hrs / 2

Peak Elev= 206.08' @ 9.13 hrs Surf.Area= 700 sf Storage= 874 cf

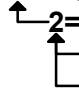
Flood Elev= 206.34' Surf.Area= 700 sf Storage= 1,057 cf

Plug-Flow detention time= 80.7 min calculated for 0.110 af (100% of inflow)

Center-of-Mass det. time= 82.6 min (786.9 - 704.4)

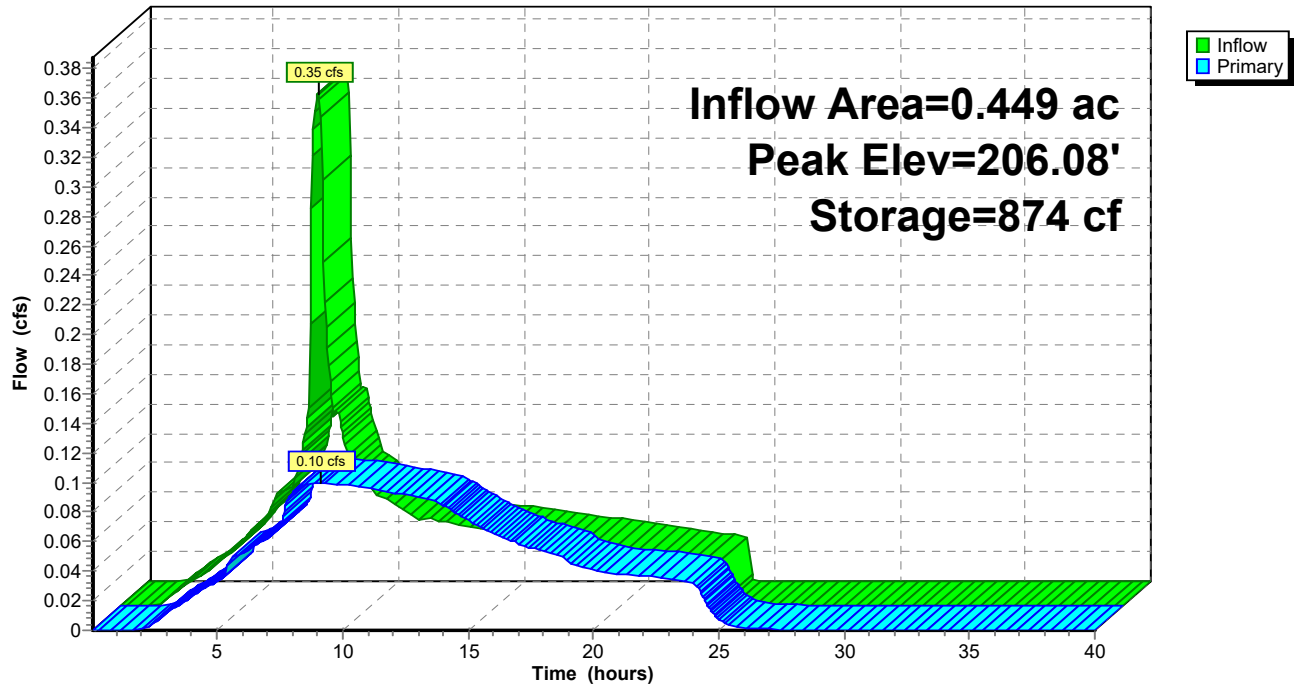
Volume	Invert	Avail.Storage	Storage Description			
#1	203.18'	1,057 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.18	700	157.0	0.0	0	0	700
203.68	700	157.0	30.0	105	105	779
203.93	700	157.0	0.0	0	105	818
205.43	700	157.0	30.0	315	420	1,053
206.18	700	157.0	100.0	525	945	1,171
206.34	700	157.0	100.0	112	1,057	1,196

Device	Routing	Invert	Outlet Devices	
#1	Device 2	206.18'	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads	
#2	Primary	203.18'	4.0" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.09 sf	
#3	Device 2	203.18'	1.5" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.01 sf	

Primary OutFlow Max=0.10 cfs @ 9.13 hrs HW=206.08' (Free Discharge)

2=Culvert (Passes 0.10 cfs of 0.69 cfs potential flow)
1=Orifice/Grate (Controls 0.00 cfs)**3=Culvert** (Inlet Controls 0.10 cfs @ 8.11 fps)

Pond 2P: RAIN GARDEN

Hydrograph



Post_Development_00330*Type IA 24-hr 100-Yr Rainfall=4.40"*

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Time span=0.01-40.00 hrs, dt=0.05 hrs, 801 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: A-1Runoff Area=19,553 sf 70.00% Impervious Runoff Depth=3.72"
Flow Length=175' Tc=5.0 min CN=94 Runoff=0.44 cfs 0.139 af**Pond 2P: RAIN GARDEN**Peak Elev=206.24' Storage=990 cf Inflow=0.44 cfs 0.139 af
Outflow=0.27 cfs 0.139 af**Total Runoff Area = 0.449 ac Runoff Volume = 0.139 af Average Runoff Depth = 3.72"**
30.00% Pervious = 0.135 ac 70.00% Impervious = 0.314 ac

Post_Development_00330

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Type IA 24-hr 100-Yr Rainfall=4.40"

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Summary for Subcatchment 1S: A-1

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.44 cfs @ 7.87 hrs, Volume= 0.139 af, Depth= 3.72"
Routed to Pond 2P : RAIN GARDEN

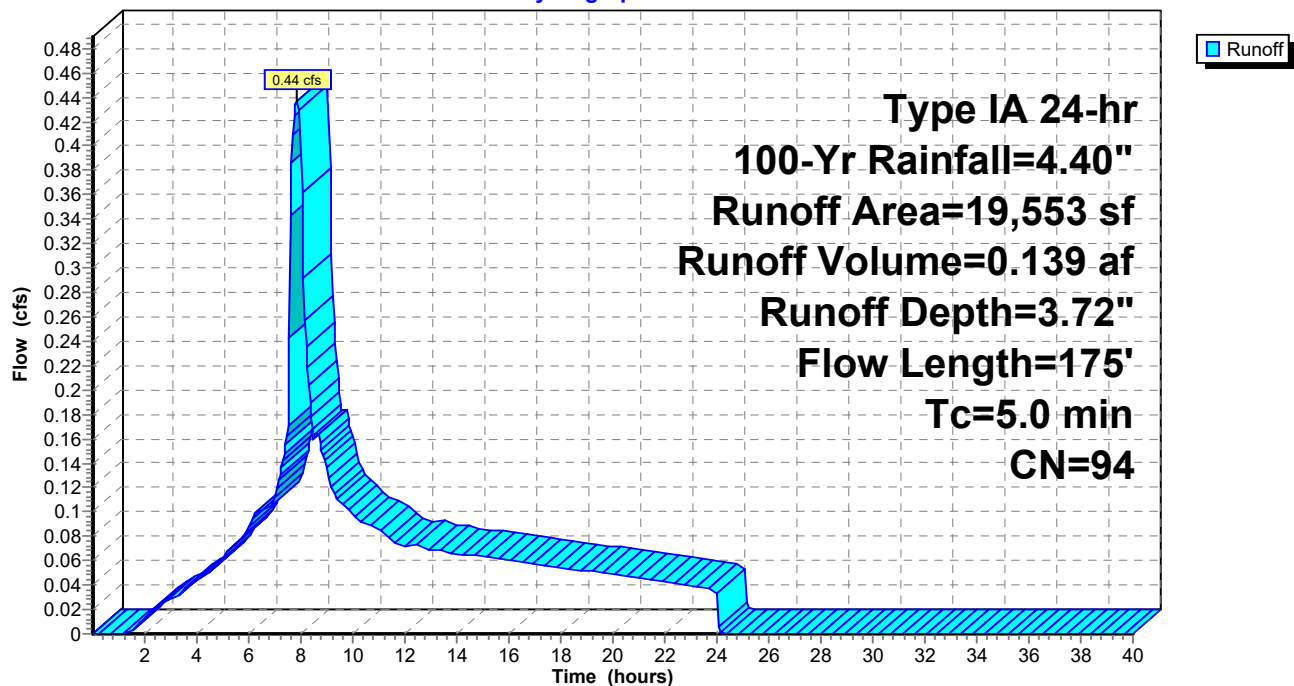
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-40.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 100-Yr Rainfall=4.40"

Area (sf)	CN	Description
13,687	98	Paved parking, HSG C
5,866	86	<50% Grass cover, Poor, HSG C
19,553	94	Weighted Average
5,866	86	30.00% Pervious Area
13,687	98	70.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	175		0.58		Direct Entry,

Subcatchment 1S: A-1

Hydrograph



Post_Development_00330

Type IA 24-hr 100-Yr Rainfall=4.40"

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Summary for Pond 2P: RAIN GARDEN

Inflow Area = 0.449 ac, 70.00% Impervious, Inflow Depth = 3.72" for 100-Yr event
 Inflow = 0.44 cfs @ 7.87 hrs, Volume= 0.139 af
 Outflow = 0.27 cfs @ 8.14 hrs, Volume= 0.139 af, Atten= 38%, Lag= 16.2 min
 Primary = 0.27 cfs @ 8.14 hrs, Volume= 0.139 af

Routing by Stor-Ind method, Time Span= 0.01-40.01 hrs, dt= 0.05 hrs / 2

Peak Elev= 206.24' @ 8.14 hrs Surf.Area= 700 sf Storage= 990 cf

Flood Elev= 206.34' Surf.Area= 700 sf Storage= 1,057 cf

Plug-Flow detention time= 89.7 min calculated for 0.139 af (100% of inflow)

Center-of-Mass det. time= 90.5 min (785.0 - 694.5)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.18'	1,057 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.18	700	157.0	0.0	0	0	700
203.68	700	157.0	30.0	105	105	779
203.93	700	157.0	0.0	0	105	818
205.43	700	157.0	30.0	315	420	1,053
206.18	700	157.0	100.0	525	945	1,171
206.34	700	157.0	100.0	112	1,057	1,196

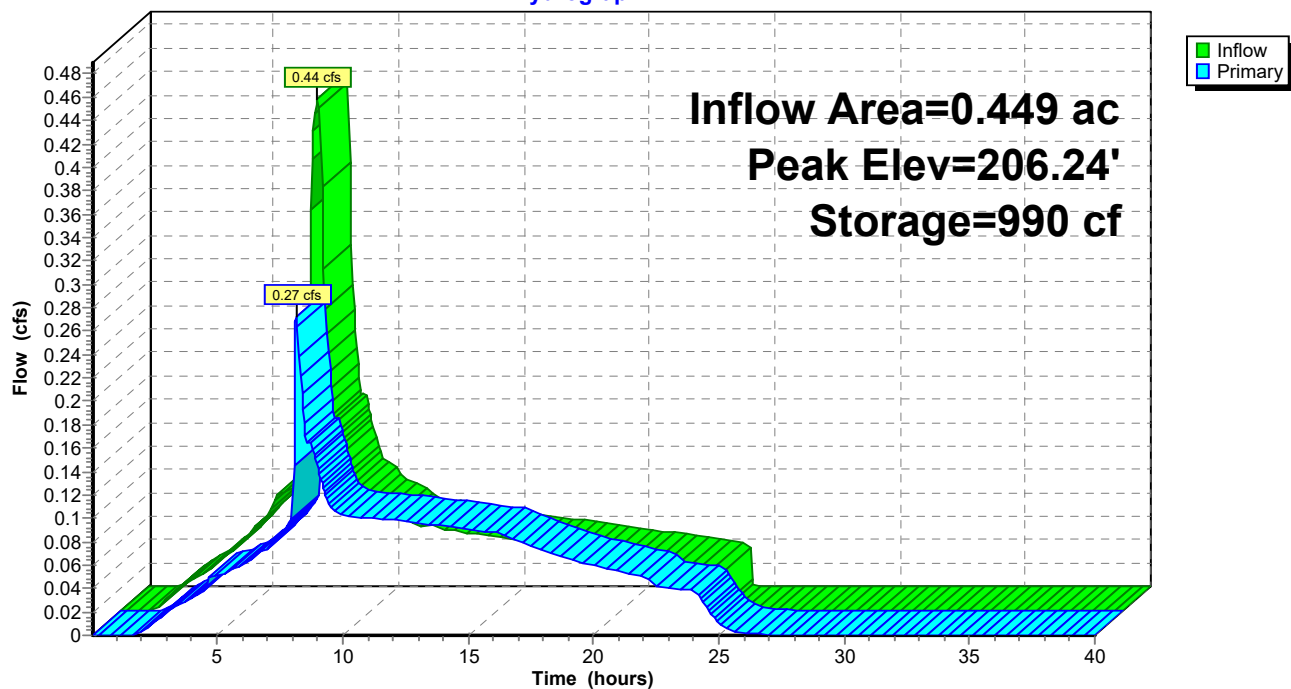
Device	Routing	Invert	Outlet Devices	
#1	Device 2	206.18'	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads	
#2	Primary	203.18'	4.0" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.09 sf	
#3	Device 2	203.18'	1.5" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.01 sf	

Primary OutFlow Max=0.27 cfs @ 8.14 hrs HW=206.24' (Free Discharge)

↑ **2=Culvert** (Passes 0.27 cfs of 0.72 cfs potential flow)
 ↑ **1=Orifice/Grate** (Weir Controls 0.17 cfs @ 0.83 fps)
 ↑ **3=Culvert** (Inlet Controls 0.10 cfs @ 8.34 fps)

Pond 2P: RAIN GARDEN

Hydrograph



Post_Development_00330*Type IA 24-hr WQV Rainfall=1.38"*

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Time span=0.01-40.00 hrs, dt=0.05 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: A-1

Runoff Area=19,553 sf 70.00% Impervious Runoff Depth=0.83"
Flow Length=175' Tc=5.0 min CN=94 Runoff=0.09 cfs 0.031 af

Pond 2P: RAIN GARDEN

Peak Elev=204.09' Storage=138 cf Inflow=0.09 cfs 0.031 af
Outflow=0.05 cfs 0.031 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.031 af Average Runoff Depth = 0.83"
30.00% Pervious = 0.135 ac 70.00% Impervious = 0.314 ac

Post_Development_00330

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Type IA 24-hr WQV Rainfall=1.38"

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Summary for Subcatchment 1S: A-1

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.09 cfs @ 7.93 hrs, Volume= 0.031 af, Depth= 0.83"
Routed to Pond 2P : RAIN GARDEN

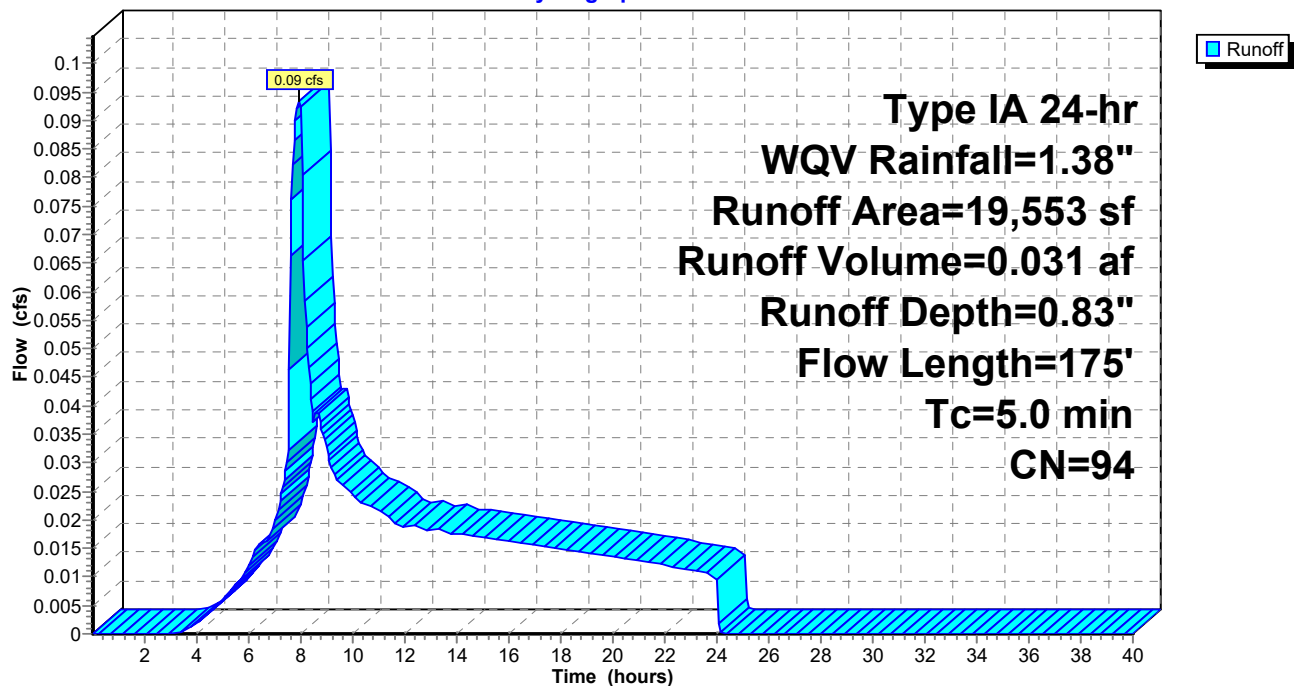
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-40.01 hrs, $dt=0.05$ hrs
Type IA 24-hr WQV Rainfall=1.38"

Area (sf)	CN	Description
13,687	98	Paved parking, HSG C
5,866	86	<50% Grass cover, Poor, HSG C
19,553	94	Weighted Average
5,866	86	30.00% Pervious Area
13,687	98	70.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	175		0.58		Direct Entry,

Subcatchment 1S: A-1

Hydrograph



Post_Development_00330

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Type IA 24-hr WQV Rainfall=1.38"

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Summary for Pond 2P: RAIN GARDEN

Inflow Area = 0.449 ac, 70.00% Impervious, Inflow Depth = 0.83" for WQV event
 Inflow = 0.09 cfs @ 7.93 hrs, Volume= 0.031 af
 Outflow = 0.05 cfs @ 8.21 hrs, Volume= 0.031 af, Atten= 42%, Lag= 16.4 min
 Primary = 0.05 cfs @ 8.21 hrs, Volume= 0.031 af

Routing by Stor-Ind method, Time Span= 0.01-40.01 hrs, dt= 0.05 hrs / 2

Peak Elev= 204.09' @ 8.21 hrs Surf.Area= 700 sf Storage= 138 cf

Flood Elev= 206.34' Surf.Area= 700 sf Storage= 1,057 cf

Plug-Flow detention time= 40.5 min calculated for 0.031 af (100% of inflow)

Center-of-Mass det. time= 40.9 min (810.1 - 769.1)

Volume	Invert	Avail.Storage	Storage Description			
#1	203.18'	1,057 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
203.18	700	157.0	0.0	0	0	700
203.68	700	157.0	30.0	105	105	779
203.93	700	157.0	0.0	0	105	818
205.43	700	157.0	30.0	315	420	1,053
206.18	700	157.0	100.0	525	945	1,171
206.34	700	157.0	100.0	112	1,057	1,196

Device	Routing	Invert	Outlet Devices	
#1	Device 2	206.18'	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads	
#2	Primary	203.18'	4.0" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.09 sf	
#3	Device 2	203.18'	1.5" Round Culvert L= 2.0' Ke= 0.500 Inlet / Outlet Invert= 203.18' / 203.17' S= 0.0050 '/' Cc= 0.900 n= 0.013, Flow Area= 0.01 sf	

Primary OutFlow Max=0.05 cfs @ 8.21 hrs HW=204.09' (Free Discharge)

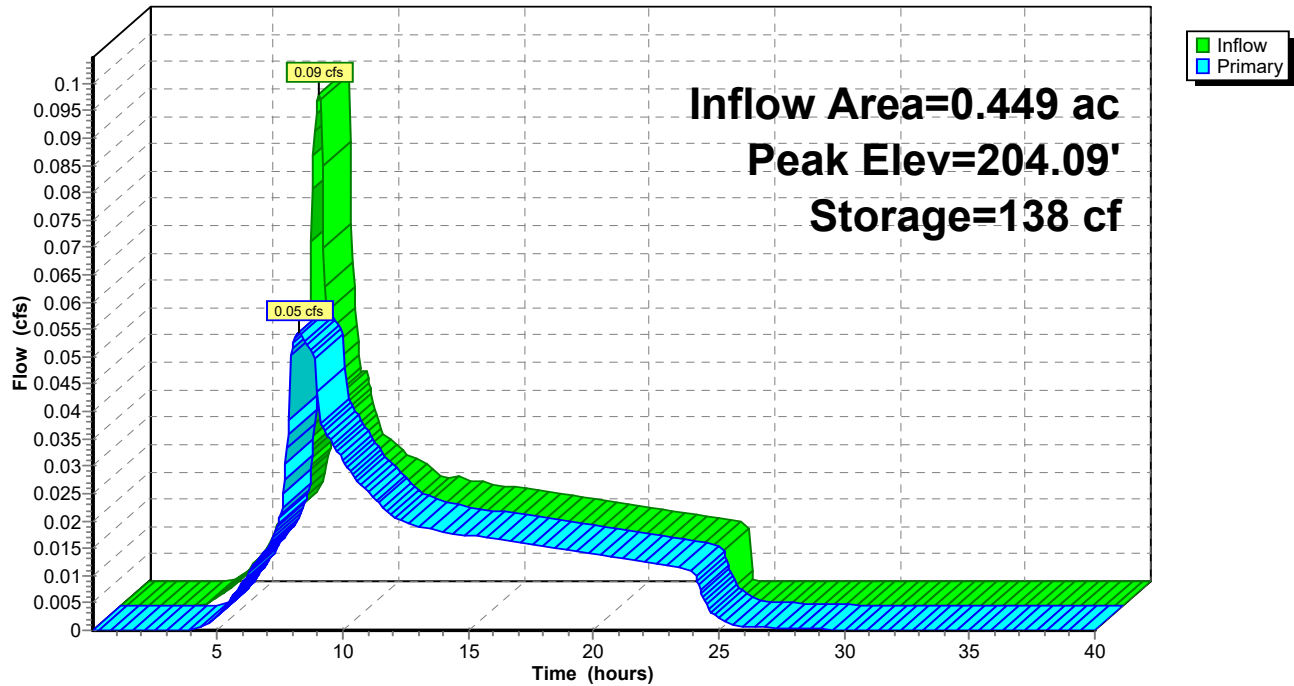
2=Culvert (Passes 0.05 cfs of 0.36 cfs potential flow)

1=Orifice/Grate (Controls 0.00 cfs)

3=Culvert (Inlet Controls 0.05 cfs @ 4.42 fps)

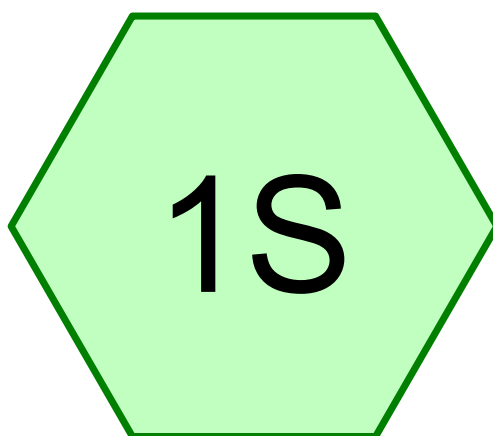
Pond 2P: RAIN GARDEN

Hydrograph

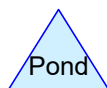
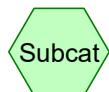


PRE DEVELOPMENT HYDROCAD

THE ELEVATIONS SHOWN HEREIN ARE ARBITRARY AND USED FOR CALCULATION PURPOSES ONLY



EX



Routing Diagram for Pre-Development - 00330
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Pre-Development - 00330

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Rainfall Events Listing

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-Yr	Type IA 24-hr		Default	24.00	1	2.20	2
2	5-Yr	Type IA 24-hr		Default	24.00	1	2.80	2
3	10-Yr	Type IA 24-hr		Default	24.00	1	3.20	2
4	25-Yr	Type IA 24-hr		Default	24.00	1	3.60	2
5	100-Yr	Type IA 24-hr		Default	24.00	1	4.40	2
6	WQV	Type IA 24-hr		Default	24.00	1	1.38	2

Pre-Development - 00330

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.449	86	<50% Grass cover, Poor, HSG C (1S)
0.449	86	TOTAL AREA

Pre-Development - 00330

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
0.449	HSG C	1S
0.000	HSG D	
0.000	Other	
0.449		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	0.449	0.000	0.000	0.449	<50% Grass cover, Poor	1S
0.000	0.000	0.449	0.000	0.000	0.449	TOTAL AREA	

Pre-Development - 00330*Type IA 24-hr 2-Yr Rainfall=2.20"*

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Time span=0.01-60.00 hrs, dt=0.05 hrs, 1201 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: EX

Runoff Area=19,553 sf 0.00% Impervious Runoff Depth=1.00"

Flow Length=275' Slope=0.0200 '/' Tc=5.0 min CN=86 Runoff=0.10 cfs 0.038 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.038 af Average Runoff Depth = 1.00"**100.00% Pervious = 0.449 ac 0.00% Impervious = 0.000 ac**

Pre-Development - 00330

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Type IA 24-hr 2-Yr Rainfall=2.20"

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Summary for Subcatchment 1S: EX[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.10 cfs @ 7.97 hrs, Volume= 0.038 af, Depth= 1.00"

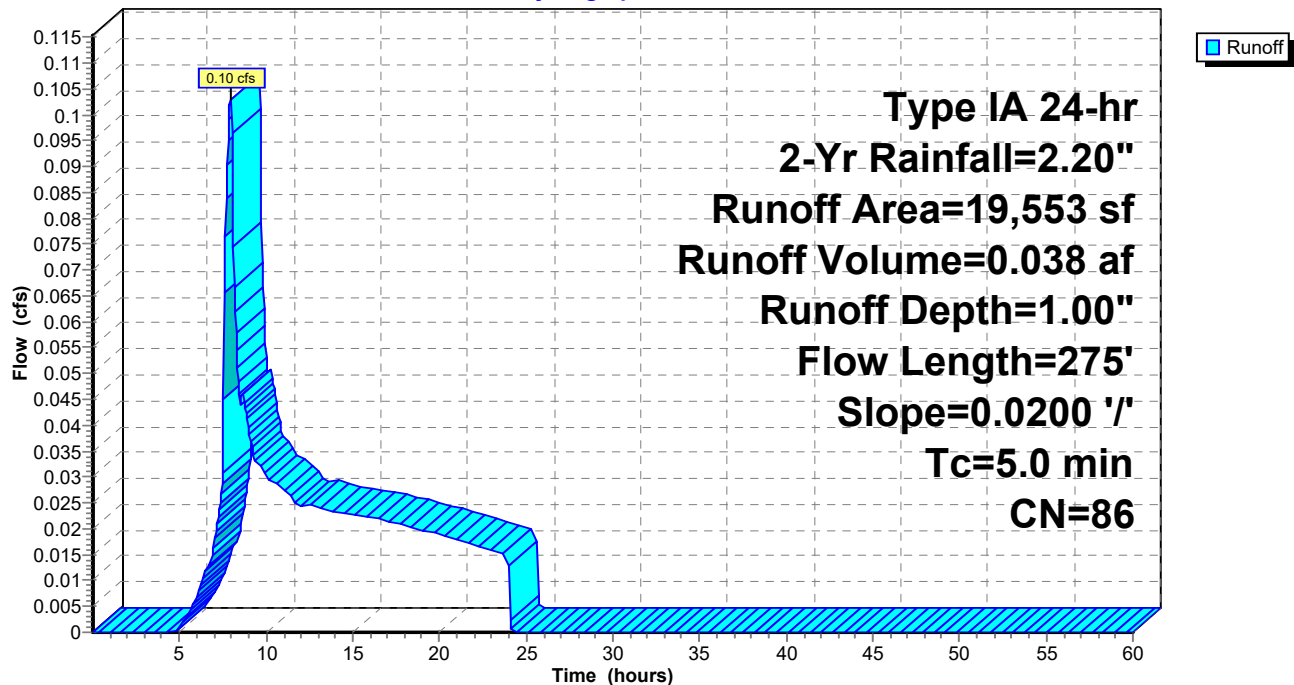
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-60.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 2-Yr Rainfall=2.20"

Area (sf)	CN	Description
19,553	86	<50% Grass cover, Poor, HSG C
19,553	86	100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	275	0.0200	1.40		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.20"
3.3	275	Total, Increased to minimum Tc = 5.0 min			

Subcatchment 1S: EX

Hydrograph



Pre-Development - 00330*Type IA 24-hr 5-Yr Rainfall=2.80"*

Prepared by 7 Oaks Engineering, Inc

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Page 8

Time span=0.01-60.00 hrs, dt=0.05 hrs, 1201 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: EX

Runoff Area=19,553 sf 0.00% Impervious Runoff Depth=1.49"

Flow Length=275' Slope=0.0200 '/' Tc=5.0 min CN=86 Runoff=0.16 cfs 0.056 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.056 af Average Runoff Depth = 1.49"**100.00% Pervious = 0.449 ac 0.00% Impervious = 0.000 ac**

Pre-Development - 00330

Prepared by 7 Oaks Engineering, Inc

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Type IA 24-hr 5-Yr Rainfall=2.80"

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Page 9

Summary for Subcatchment 1S: EX[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.16 cfs @ 7.95 hrs, Volume= 0.056 af, Depth= 1.49"

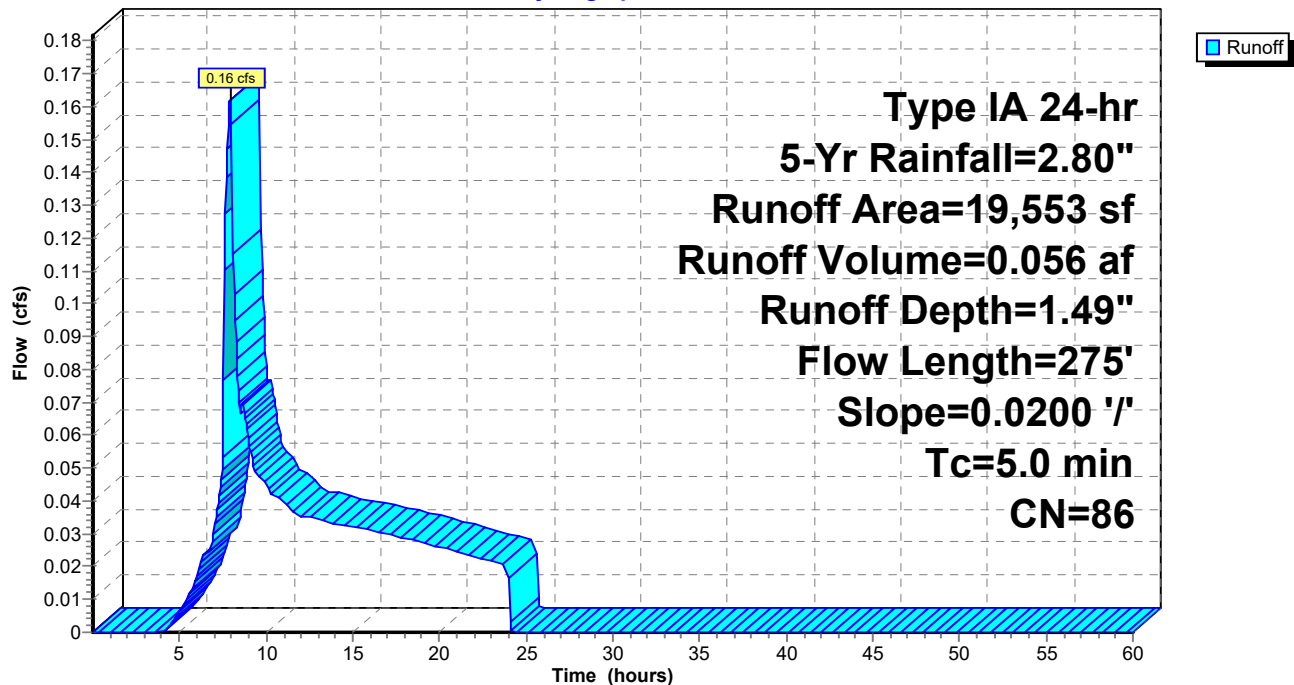
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-60.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 5-Yr Rainfall=2.80"

Area (sf)	CN	Description
19,553	86	<50% Grass cover, Poor, HSG C
19,553	86	100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	275	0.0200	1.40		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.20"
3.3	275	Total, Increased to minimum Tc = 5.0 min			

Subcatchment 1S: EX

Hydrograph



Pre-Development - 00330*Type IA 24-hr 10-Yr Rainfall=3.20"*

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Time span=0.01-60.00 hrs, dt=0.05 hrs, 1201 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: EX

Runoff Area=19,553 sf 0.00% Impervious Runoff Depth=1.84"

Flow Length=275' Slope=0.0200 '/' Tc=5.0 min CN=86 Runoff=0.20 cfs 0.069 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.069 af Average Runoff Depth = 1.84"**100.00% Pervious = 0.449 ac 0.00% Impervious = 0.000 ac**

Pre-Development - 00330

Prepared by 7 Oaks Engineering, Inc

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Type IA 24-hr 10-Yr Rainfall=3.20"

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Page 11

Summary for Subcatchment 1S: EX[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.20 cfs @ 7.94 hrs, Volume= 0.069 af, Depth= 1.84"

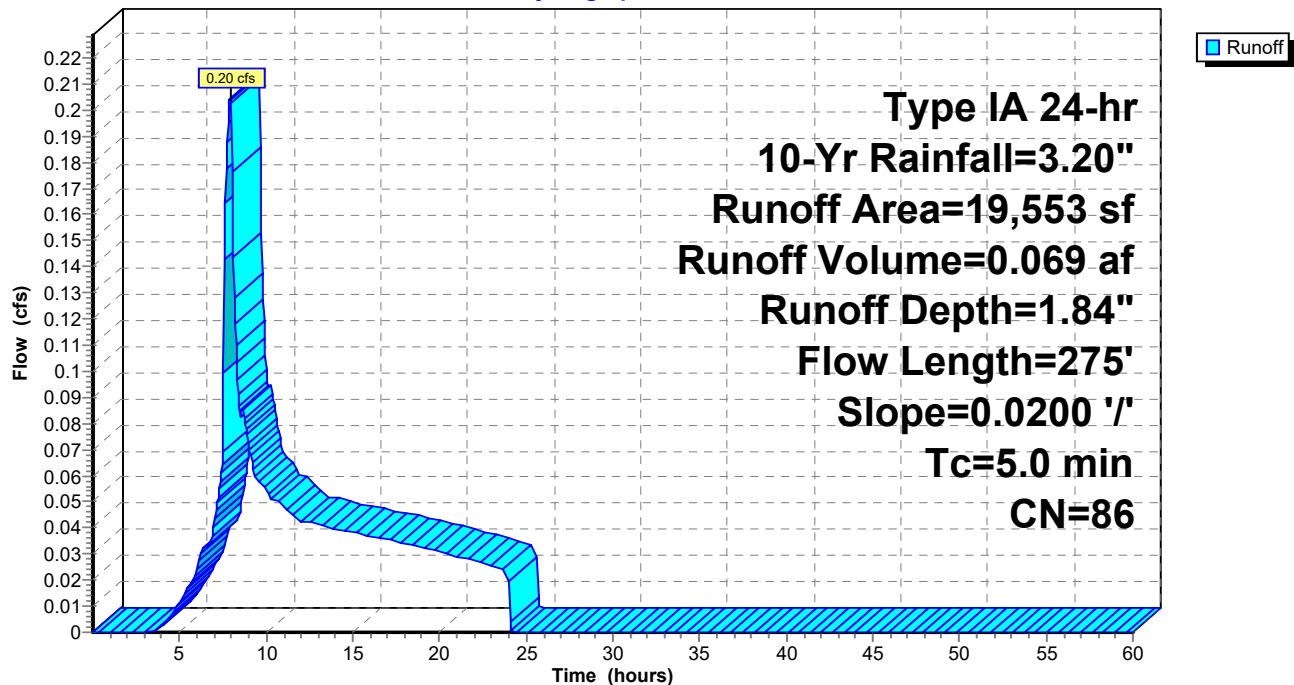
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-60.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 10-Yr Rainfall=3.20"

Area (sf)	CN	Description
19,553	86	<50% Grass cover, Poor, HSG C
19,553	86	100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	275	0.0200	1.40		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.20"
3.3	275	Total, Increased to minimum Tc = 5.0 min			

Subcatchment 1S: EX

Hydrograph



Pre-Development - 00330*Type IA 24-hr 25-Yr Rainfall=3.60"*

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Time span=0.01-60.00 hrs, dt=0.05 hrs, 1201 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: EX

Runoff Area=19,553 sf 0.00% Impervious Runoff Depth=2.19"

Flow Length=275' Slope=0.0200 '/' Tc=5.0 min CN=86 Runoff=0.25 cfs 0.082 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.082 af Average Runoff Depth = 2.19"**100.00% Pervious = 0.449 ac 0.00% Impervious = 0.000 ac**

Pre-Development - 00330

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Type IA 24-hr 25-Yr Rainfall=3.60"

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Page 13

Summary for Subcatchment 1S: EX[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.25 cfs @ 7.93 hrs, Volume= 0.082 af, Depth= 2.19"

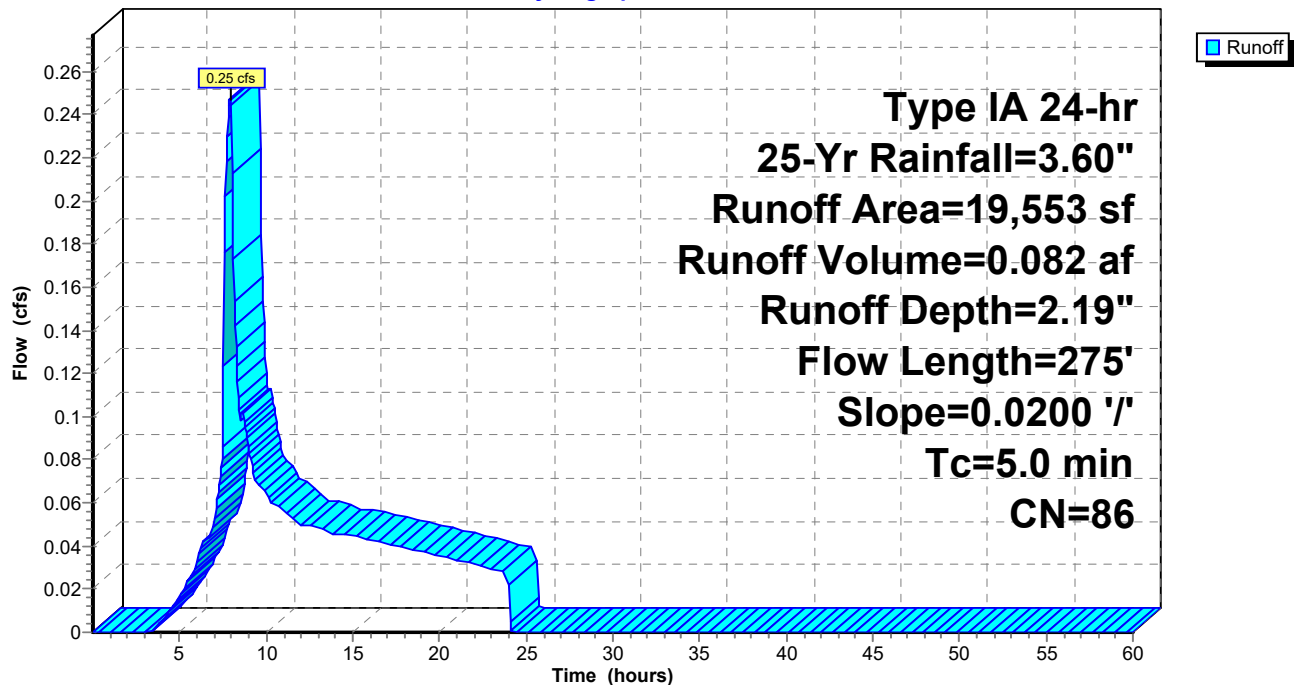
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-60.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 25-Yr Rainfall=3.60"

Area (sf)	CN	Description
19,553	86	<50% Grass cover, Poor, HSG C
19,553	86	100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	275	0.0200	1.40		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.20"
3.3	275	Total, Increased to minimum Tc = 5.0 min			

Subcatchment 1S: EX

Hydrograph



Pre-Development - 00330*Type IA 24-hr 100-Yr Rainfall=4.40"*

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Page 14

Time span=0.01-60.00 hrs, dt=0.05 hrs, 1201 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: EX

Runoff Area=19,553 sf 0.00% Impervious Runoff Depth=2.91"

Flow Length=275' Slope=0.0200 '/' Tc=5.0 min CN=86 Runoff=0.34 cfs 0.109 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.109 af Average Runoff Depth = 2.91"**100.00% Pervious = 0.449 ac 0.00% Impervious = 0.000 ac**

Pre-Development - 00330

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Type IA 24-hr 100-Yr Rainfall=4.40"

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Page 15

Summary for Subcatchment 1S: EX[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.34 cfs @ 7.92 hrs, Volume= 0.109 af, Depth= 2.91"

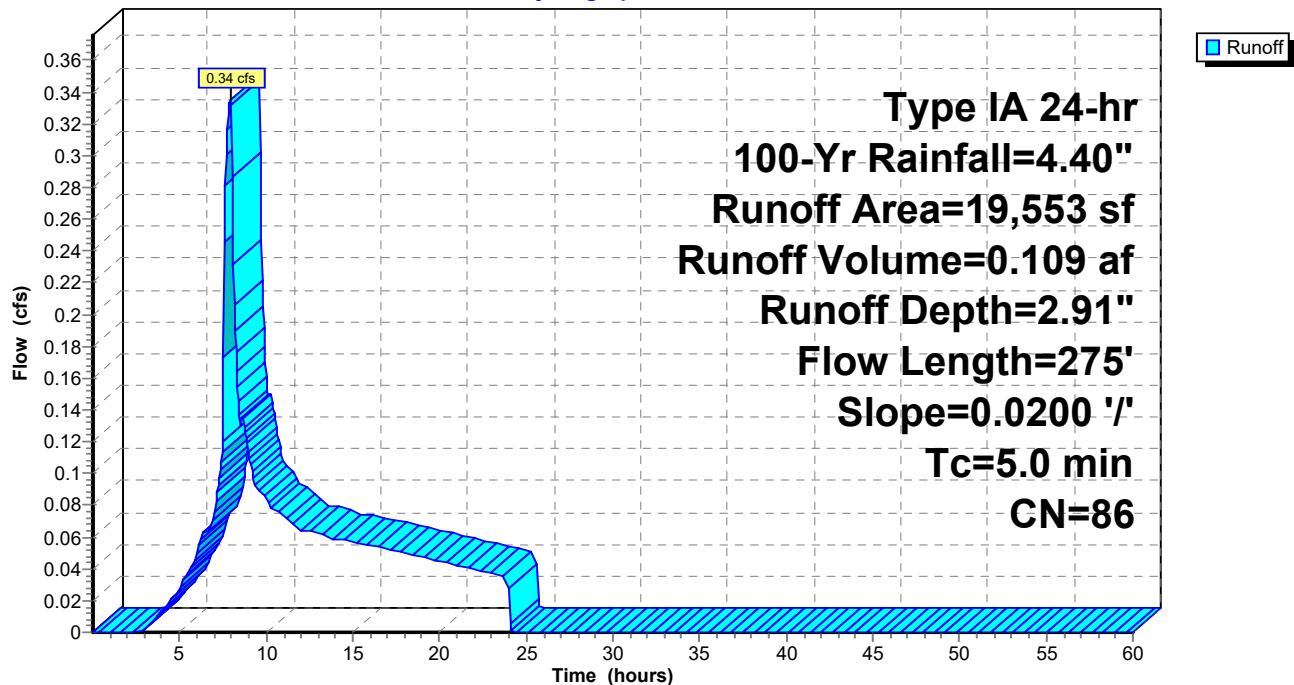
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-60.01 hrs, $dt=0.05$ hrs
Type IA 24-hr 100-Yr Rainfall=4.40"

Area (sf)	CN	Description
19,553	86	<50% Grass cover, Poor, HSG C
19,553	86	100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	275	0.0200	1.40		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.20"
3.3	275	Total, Increased to minimum Tc = 5.0 min			

Subcatchment 1S: EX

Hydrograph



Pre-Development - 00330*Type IA 24-hr WQV Rainfall=1.38"*

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Time span=0.01-60.00 hrs, dt=0.05 hrs, 1201 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: EX

Runoff Area=19,553 sf 0.00% Impervious Runoff Depth=0.41"

Flow Length=275' Slope=0.0200 '/' Tc=5.0 min CN=86 Runoff=0.03 cfs 0.016 af

Total Runoff Area = 0.449 ac Runoff Volume = 0.016 af Average Runoff Depth = 0.41"**100.00% Pervious = 0.449 ac 0.00% Impervious = 0.000 ac**

Pre-Development - 00330

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Type IA 24-hr WQV Rainfall=1.38"

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Page 17

Summary for Subcatchment 1S: EX[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.03 cfs @ 7.99 hrs, Volume= 0.016 af, Depth= 0.41"

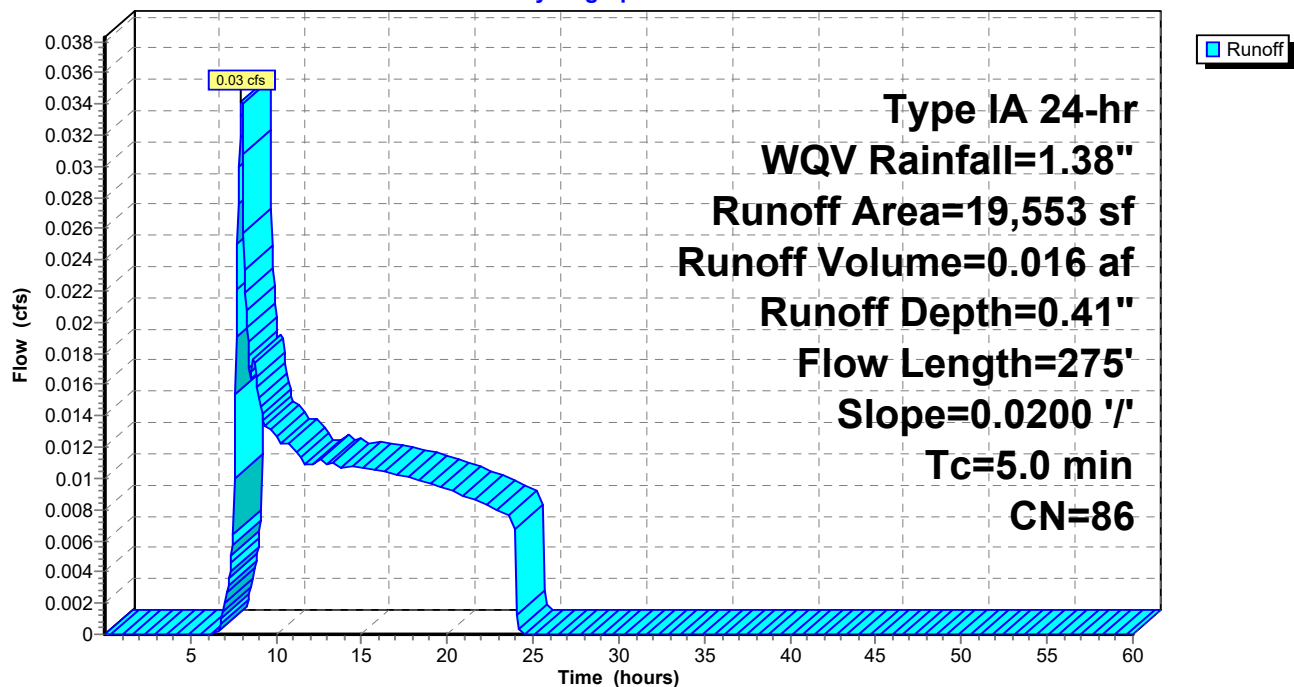
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.01-60.01 hrs, $dt=0.05$ hrs
Type IA 24-hr WQV Rainfall=1.38"

Area (sf)	CN	Description
19,553	86	<50% Grass cover, Poor, HSG C
19,553	86	100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	275	0.0200	1.40		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.20"
3.3	275	Total, Increased to minimum Tc = 5.0 min			

Subcatchment 1S: EX

Hydrograph



APPENDIX C – PLANS

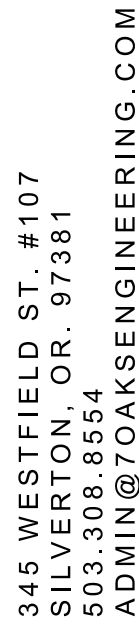
D STREET NE

CHIMNEY

STORMWATER COMBINATION SWALE TOP=205.77

PROPOSED BLDG FF=207.75

JOB #00330



REGISTERED PROFESSIONAL
ENGINEER
96126PE
~~PRELIMINARY~~
OREGON
MAY 12, 2020
STEVEN JOHNSON

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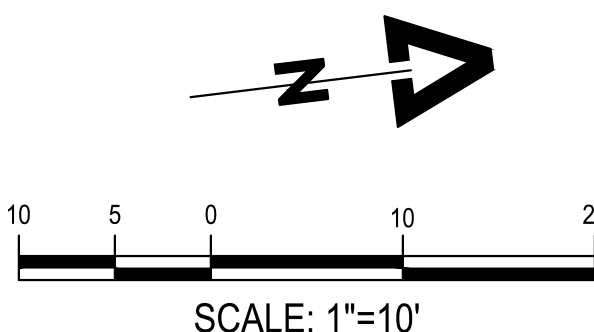
DRAWN BY

SALEM OR, 97301

2

D STREET NE

Call the Oregon One-Call Center
DIAL 811 or 1-800-332-2344



D STREET NE

EXISTING SOAB (205.90RIM)
IE (10" CONC. E) 201.4
IE (10" CONC. W) 201.3

PROPOSED 6" STORM DRAIN CONNECTION
(±201.51INV-10"
201.67INV-6"

EXISTING 8" CAST IRON
WATER MAIN

EXISTING 10"
STORM DRAIN
(S=0.004)

EXISTING 12"
CONC. SEWER MAIN
(S=0.0019)

PROPOSED 1"
IRRIGATION SERVICE
PROPOSED 2"
DOMESTIC SERVICE
PROPOSED 4"
FIRE SERVICE
PROPOSED FIRE HYDRANT

PROPOSED 6"
SEWER SERVICE
(±194.9)INV-12"
195.15INV-6"

EXISTING LOT LINE

EXISTING LOT LINE

22.00'
PROP ACCESS EASE

PROPOSED ROW

6.00'
DEDICATION

PROPOSED IRRIGATION
POINT OF CONNECTION

PROPOSED BUILDING
POINT OF CONNECTION

PROPOSED FIRE RISER

PROPOSED 676-1-WA FIRE
VAULT WITH
ATTACHED FDC

10.00'
PROP PUE

PROPOSED SEWER P.O.C.
202.00INV

PROPOSED SEWER P.O.C.
202.29INV

PROPOSED SEWER P.O.C.
202.50INV

PROPOSED SEWER P.O.C.
202.75INV

PROPOSED SEWER P.O.C.
202.95INV

PROPOSED SEWER P.O.C.
202.11INV

PROPOSED SEWER P.O.C.
202.46INV

PROPOSED SEWER P.O.C.
202.72INV

PROPOSED SEWER P.O.C.
202.95INV

PROPOSED SEWER P.O.C.
202.11INV

PROPOSED SEWER P.O.C.
202.46INV

PROPOSED SEWER P.O.C.
202.72INV

PROPOSED SEWER P.O.C.
202.95INV

PROPOSED SEWER P.O.C.
202.11INV

PROPOSED SEWER P.O.C.
202.46INV

PROPOSED SEWER P.O.C.
202.72INV

PROPOSED SEWER P.O.C.
202.95INV

PROPOSED BLDG
FF=207.75

PROPOSED SEWER P.O.C.
202.00INV

PROPOSED SEWER P.O.C.
202.29INV

PROPOSED SEWER P.O.C.
202.50INV

PROPOSED SEWER P.O.C.
202.75INV

PROPOSED SEWER P.O.C.
202.95INV

PROPOSED SEWER CO
198.21INV

PROPOSED SEWER CO
201.96INV

PROPOSED SEWER CO
202.21INV

PROPOSED SEWER CO
202.46INV

PROPOSED SEWER CO
202.72INV

PROPOSED 6"SEWER
(S=0.010 MIN)

EXISTING LOT LINE

STORMWATER
COMBINATION
SWALE
TOP=205.77

PROPOSED SD INLET
205.77TG
203.61INV

PROPOSED SD CO
202.95INV

PROPOSED STORMWATER
INFRASTRUCTURE

EXISTING LOT LINE

NOTICE TO EXCAVATORS:

ATTENTION: OREGON LAW REQUIRES YOU TO FOLLOW RULES ADOPTED BY THE OREGON UTILITY NOTIFICATION CENTER. THOSE RULES ARE SET FORTH IN OAR 952-001-0010 THROUGH OAR 952-001-0090. YOU MAY OBTAIN COPIES OF THE RULES BY CALLING THE CENTER.

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THE EXISTENCE AND LOCATION OF ANY UNDERGROUND UTILITIES OR STRUCTURES SHOWN IN THESE PLANS ARE OBTAINED BY A SEARCH OF AVAILABLE RECORDS, AND TO THE BEST OF OUR KNOWLEDGE, THERE ARE NOT EXISTING UTILITIES EXCEPT THOSE SHOWN ON THESE PLANS. THE CONTRACTOR IS REQUIRED TO TAKE ALL PRECAUTIONARY MEASURES TO PROTECT THE UTILITIES SHOWN, AND ANY OTHER LINES OR STRUCTURES NOT SHOWN ON THESE PLANS, AND IS RESPONSIBLE FOR THE PROTECTION OF THESE LINES OR STRUCTURES.

CONSTRUCTION CONTRACTOR AGREES THAT IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, CONSTRUCTION CONTRACTOR WILL BE REQUIRED TO ASSUME SOLE AND COMPLETE RESPONSIBILITY FOR JOB SITE CONDITIONS DURING THE COURSE OF CONSTRUCTION FOR THE PROJECT, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY; THAT THIS REQUIREMENTS SHALL BE MADE TO APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS, AND CONSTRUCTION CONTRACTOR FURTHER AGREES TO DEFEND, INDEMNIFY, AND HOLD HARMLESS THE CITY, ITS EMPLOYEES, AND AGENTS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT.

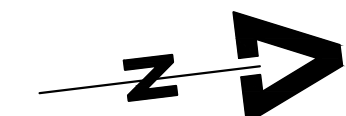
THE CONTRACTOR SHALL BE RESPONSIBLE TO REPORT DISCREPANCIES IN PLANS AND/OR FIELD CONDITIONS IMMEDIATELY TO THE DESIGN ENGINEER FOR RESOLUTION PRIOR TO CONSTRUCTION, AND SHALL BE RESPONSIBLE FOR DISCREPANCIES NOT SO REPORTED AND RESOLVED.

LEGEND:

- SD PROPOSED DRAIN LINE
SS PROPOSED SEWER
W PROPOSED WATER
+++++ APPROXIMATE LIMITS OF UTILITY REMOVAL
□ PROPOSED WATER METER
• PROPOSED CLEANOUT

UTILITY GENERAL NOTES:

- REFER TO SEPARATE UTILITY PURVEYOR FOR ELECTRICAL AND GAS SERVICES.
- ALL EXISTING UTILITIES SHALL BE PROTECTED IN PLACE UNLESS OTHERWISE SPECIFICALLY CALLED FOR ON THE PLANS.
- THE ENGINEER OF RECORD SHALL BE CONTACTED IF ANY DISCREPANCIES ARISE IN THE FIELD.



10 5 0 10 20
SCALE: 1"=10'

7 OAKS
ENGINEERING

345 WESTFIELD ST. #107
SALEM, OR 97361
503.518.8855
ADMIN@7OAKSENGINEERING.COM

STAMP:



NO	DATE	ISSUE DESCRIPTION

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CONTRACTOR SHALL VERIFY ALL EXISTING CONDITIONS PRIOR TO PROCEEDING WITH CONSTRUCTION AND NOTIFY ARCHITECT IMMEDIATELY OF ANY DISCREPANCIES OR CONFLICTS.

QC BY:

DRAWN BY:

PROJECT NAME:
MULTI-FAMILY DEVELOPMENT
PROJECT ADDRESS:
3021 & 3027 D STREET NE
SALEM OR, 97301

SHEET TITLE:
**PRELIMINARY
WET UTILITY
PLAN**

DATE:
08/20/2024

SHEET NUMBER:
3

JOB #00330

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LEGEND:

HYDROLOGY SUBAREA BOUNDARY LINE



SUB-AREA LABEL

ENGINEERED METHOD SUMMARY										
PRE VS. POST CONSTRUCTION FLOW RATES										
FACILITY ID	PEAK FLOW RATE (CFS)									
	HALF OF THE 2 YEAR STORM		5 YEAR STORM		10 YEAR STORM		25 YEAR STORM		100 YEAR STORM	
PROJECT SITE	PRE	POST	PRE	POST	PRE	POST	PRE	POST	PRE	POST
A	0.1	0.08	0.16	0.09	0.2	0.09	0.25	0.1	0.34	0.27

*Number were taken to the 100th place, and rounded accordingly.

CATCHMENT AND FACILITY TABLE			
AREA	TOTAL AREA (SF)/(AC.)	IMPERVIOUS AREA (SF)	PERVIOUS AREA (SF)
A	19,553	13,687	5,866



10 5 0 10 20
SCALE: 1"=10'

7 OAKS
ENGINEERING

345 WESTFIELD ST. #107
SALEM, OR. 97361
503.481.8655
ADMIN@7OAKSENGINEERING.COM

STAMP:



NO	DATE	ISSUE DESCRIPTION

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CONTRACTOR SHALL VERIFY ALL EXISTING CONDITIONS PRIOR TO PROCEEDING WITH CONSTRUCTION AND NOTIFY ARCHITECT IMMEDIATELY OF ANY DISCREPANCIES OR CONFLICTS.

QC BY:

DRAWN BY:

PROJECT NAME:

MULTI-FAMILY DEVELOPMENT

PROJECT ADDRESS:

3021 & 3027 D STREET NE

SALEM OR, 97301

SHEET TITLE:

PRELIMINARY
STORMWATER
PLAN

DATE:

08/20/2024

SHEET NUMBER:

4

JOB #00330

(NOTE: THE TELEPHONE NUMBER FOR THE OREGON UTILITY NOTIFICATION CENTER IS 503-232-1987).

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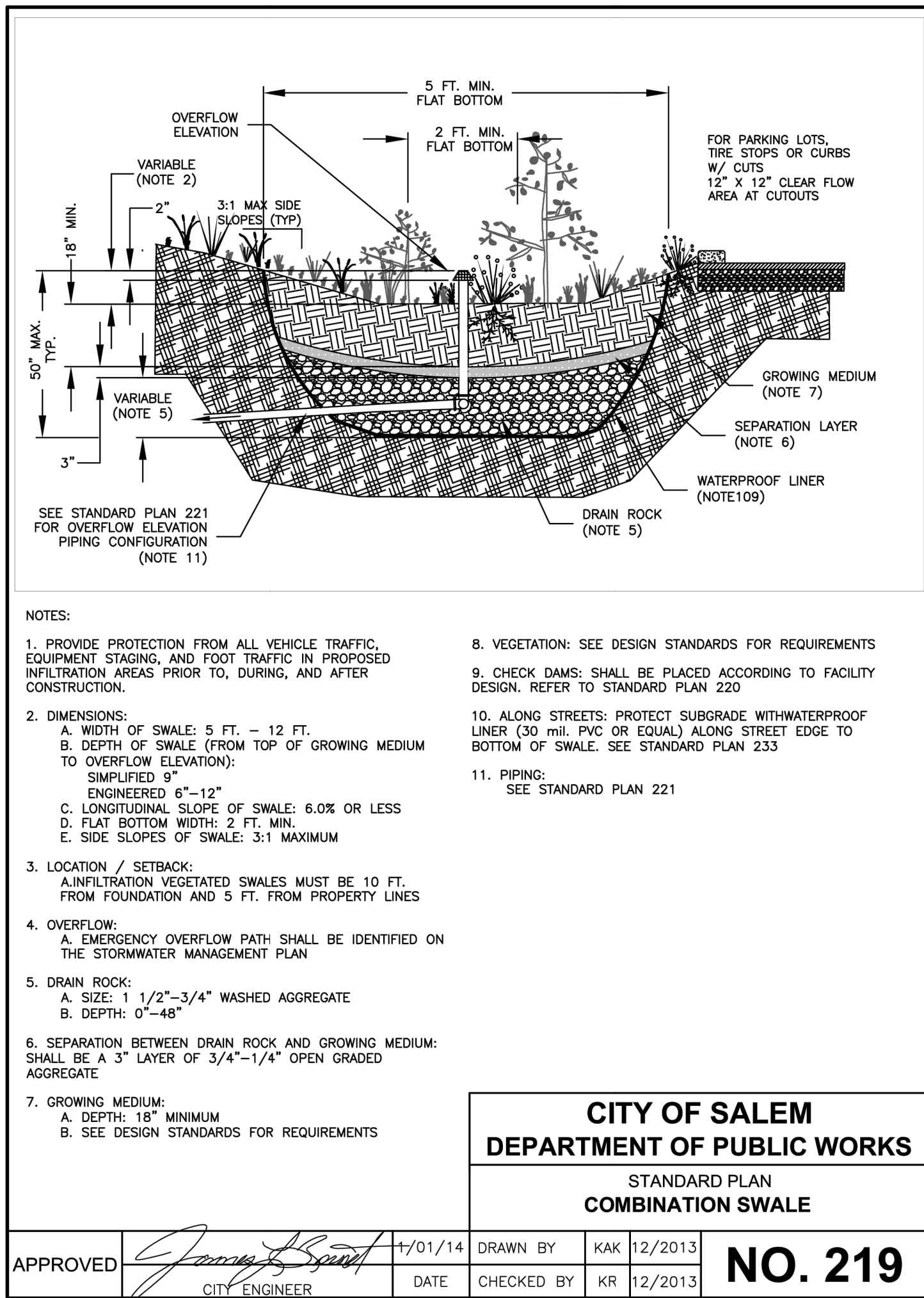
Call the Oregon One-Call Center
DIAL 811 or 1-800-332-2344

ENGINEER'S NOTICE TO CONTRACTOR:

THE EXISTENCE AND LOCATION OF ANY UNDERGROUND UTILITIES OR STRUCTURES SHOWN IN THESE PLANS ARE OBTAINED BY A SEARCH OF AVAILABLE RECORDS, AND TO THE BEST OF OUR KNOWLEDGE, THERE ARE NOT EXISTING UTILITIES EXCEPT THOSE SHOWN ON THESE PLANS. THE CONTRACTOR IS REQUIRED TO TAKE ALL PRECAUTIONARY MEASURES TO PROTECT THE UTILITIES SHOWN, AND ANY OTHER LINES OR STRUCTURES NOT SHOWN ON THESE PLANS, AND IS RESPONSIBLE FOR THE PROTECTION OF ANY DAMAGE TO THESE LINES OR STRUCTURES.

CONSTRUCTION CONTRACTOR AGREES THAT IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, CONSTRUCTION CONTRACTOR WILL BE REQUIRED TO ASSUME SOLE AND COMPLETE RESPONSIBILITY FOR JOB SITE CONDITIONS DURING THE COURSE OF CONSTRUCTION FOR THE PROJECT, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY; THAT THIS REQUIREMENTS SHALL BE MADE TO APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS, AND CONSTRUCTION CONTRACTOR FURTHER AGREES TO DEFEND, INDEMNIFY, AND HOLD HARMLESS THE CITY, ITS EMPLOYEES, AND AGENTS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT.

THE CONTRACTOR SHALL BE RESPONSIBLE TO REPORT DISCREPANCIES IN PLANS AND/OR FIELD CONDITIONS IMMEDIATELY TO THE DESIGN ENGINEER FOR RESOLUTION PRIOR TO CONSTRUCTION, AND SHALL BE RESPONSIBLE FOR DISCREPANCIES NOT SO REPORTED AND RESOLVED.



7OAKS
ENGINEERING

345 WESTFIELD ST. #107
SILVERTON, OR. 97381
503.308.8554
ADMIN@7OAKSENGINEERING.COM

STAMP:

[illegible]

NO CHANGES, MODIFICATIONS OR
REPRODUCTIONS TO BE MADE TO THESE
DRAWINGS WITHOUT WRITTEN
AUTHORIZATION FROM THE DESIGN
ENGINEER.

DIMENSIONS AND NOTES TAKE
PRECEDENCE OVER GRAPHICAL
REPRESENTATION.

THESE DRAWINGS MAY HAVE BEEN
REPRODUCED AT A SIZE DIFFERENT
THAN ORIGINALLY DRAWN. OWN
ENGINEER ASSUME NO RESPONSIBILITY
FOR USE OF INCORRECT SCALE

CONTRACTOR SHALL VERIFY ALL EXISTING
CONDITIONS PRIOR TO PROCEEDING WITH
CONSTRUCTION AND NOTIFY ARCHITECT
IMMEDIATELY OF ANY DISCREPANCIES OR
CONFLICTS.

QC BY

DRAWN BY

PROJECT NAME:

MULTI-FAMILY DEVELOPMENT

PROJECT ADDRESS:
3021 & 3027 D STREET NE

SALEM OR, 97301

SHEET TITLE:

STORMWATER DETAILS

DATE: 08/20/2024

SHEET NUMBER:

5

JOB #00330

APPENDIX D – SUPPORTING SOILS REPORT

Marion County Area, Oregon

WuA—Woodburn silt loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 24s3

Elevation: 150 to 350 feet

Mean annual precipitation: 40 to 45 inches

Mean annual air temperature: 52 to 54 degrees F

Frost-free period: 200 to 210 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Woodburn and similar soils: 85 percent

Minor components: 1 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Woodburn

Setting

Landform: Terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty alluvium and mixed mineralogy loess

Typical profile

H1 - 0 to 17 inches: silt loam

H2 - 17 to 32 inches: silty clay loam

H3 - 32 to 68 inches: silt loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water

(Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 25 to 32 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 12.0 inches)

Interpretive groups

Land capability classification (irrigated): 2w

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C

Ecological site: R002XC008OR - Valley Terrace Group

Forage suitability group: Moderately Well Drained < 15% Slopes
(G002XY004OR)

Other vegetative classification: Moderately Well Drained < 15%
Slopes (G002XY004OR)

May 22, 2024

Landon Hattan
Skyline Builders
1280 Fir Street S
Salem, Oregon 97302

RE: SITE INFILTRATION TESTING
3021 D STREET NE
SALEM, OREGON
BRANCH ENGINEERING INC. PROJECT No. 24- 147

Branch Engineering Inc (BEI) visited the subject site, see Site Vicinity Map (Figure 1), on May 8, 2024 to conduct site infiltration testing in the two test sites shown on Figure 2 that had been previously set up on May 1, 2024. The results presented herein are for preliminary design of any on-site stormwater system and should be verified by the design engineer of record (EOR) for final design and at the time of construction. The following is a summary of our site visit and test results.

SITE SOILS

Four test pits were excavated using a rubber-tracked excavator on the site in the approximate locations shown on the attached Figure-2. Two of the pits (1 and 4 labeled as IT-1 and IT-2) were set up for preliminary infiltration testing of the subsurface soils at depth of 56- to 58-inches below surface grade (BSG). The observed soils were visually classified using the American Society of Testing and Materials (ASTM) Method D-2488. The soils observed in the test pits were generally consistent in material composition with about 1.5-feet of either soft topsoil overlying a clayey silt alluvium that was moist and medium stiff that extended to the maximum depth investigated.

A nearby Oregon Water Resources Department (OWRD) well logs, see attached, describe a similar soil type as what BEI observed to a depth over 20-feet BGS. The NRCS Web Soil Survey of Marion County maps the site soils as terrace deposits of Woodburn silt loam derived from silty alluvium and mixed mineralogy loess.

GROUNDWATER

We did not encounter any groundwater during our on-site explorations to a depth of 7-feet BGS and the well log Mari 66067 shows no groundwater to a depth of 22-feet. A 1961 well log from the area indicates a static groundwater depth of 19-feet BGS with first encountered groundwater appearing to be at 50-feet BGS.

INFILTRATION TESTING

Site infiltration testing was conducted on May 8, 2024 in general accordance with the procedures set forth in the Salem Administrative Rules 109-004 Appendix C for the encased falling head method. The soil is assumed to be laterally homogeneous and that sidewall infiltration is negligible as a 6-inch diameter, open-ended, plastic standpipe was used for containment of the water column. Standing water remained in the standpipe from the initial pre-saturation of the test holes seven days prior to testing. Additional water was to the test standpipes to create a 24- to 28-inch hydraulic head on the

soil and measured one hour later with no detectable change in the water level. The measured infiltration rate in both test holes is considered to be zero.

Table 1: Infiltration Test Results

<i>Test ID</i>	<i>Soil Description</i>	<i>Test Depth (inches)</i>	<i>Infiltration Rate (in/hr)</i>
IT-1	Light Brown - Clayey Silt (ML/CL)	56	0
IT-2	Light Brown - Clayey Silt (ML/CL)	58	0

CONCLUSIONS

The infiltration rates measured in the field are zero, this rate is considered preliminary and should be confirmed by the EOR for final design of the stormwater facility as soil type and consistency may vary with distance from the test location.

Although not considered feasible based on our preliminary results, any areas proposed for infiltration shall not be subjected to compaction of the soil by vehicle traffic, storage of materials, or other means that can influence the rate of infiltration in those areas. It is the client/design professional's responsibility to determine that the stormwater facility meets these requirements for sizing, setbacks, and overflow routing.

LIMITATIONS

This report has been prepared for the exclusive use of the addressee and their designated representatives for use in design of the proposed development. The analysis and recommendations contained herein were prepared in general accordance with the standards of practice for the area at the time of this report's preparation, and may not be suitable for purposes other than those described in this report.

Subsurface explorations indicate soil conditions at specific locations and depths and do not necessarily reflect soil and groundwater variations that may exist at other locations at the site; however, site conditions were generally consistent in all our explorations. If design changes are made that may affect the results of our testing, development plans change, or at least a year passes between our investigation and the site development, we reserve the right to review the changes for applicability.

We assume no responsibility or liability for engineering, inspection, or testing performed by others and no warranty, expressed or implied, is given. Use of this report constitutes an agreement and consent by the addressee and their designated representatives to the limitations listed above.

If you have any questions regarding the test method, please contact the undersigned.
Sincerely,

Branch Engineering Inc,

A handwritten signature in blue ink, appearing to read "Ronald J. Derrick".

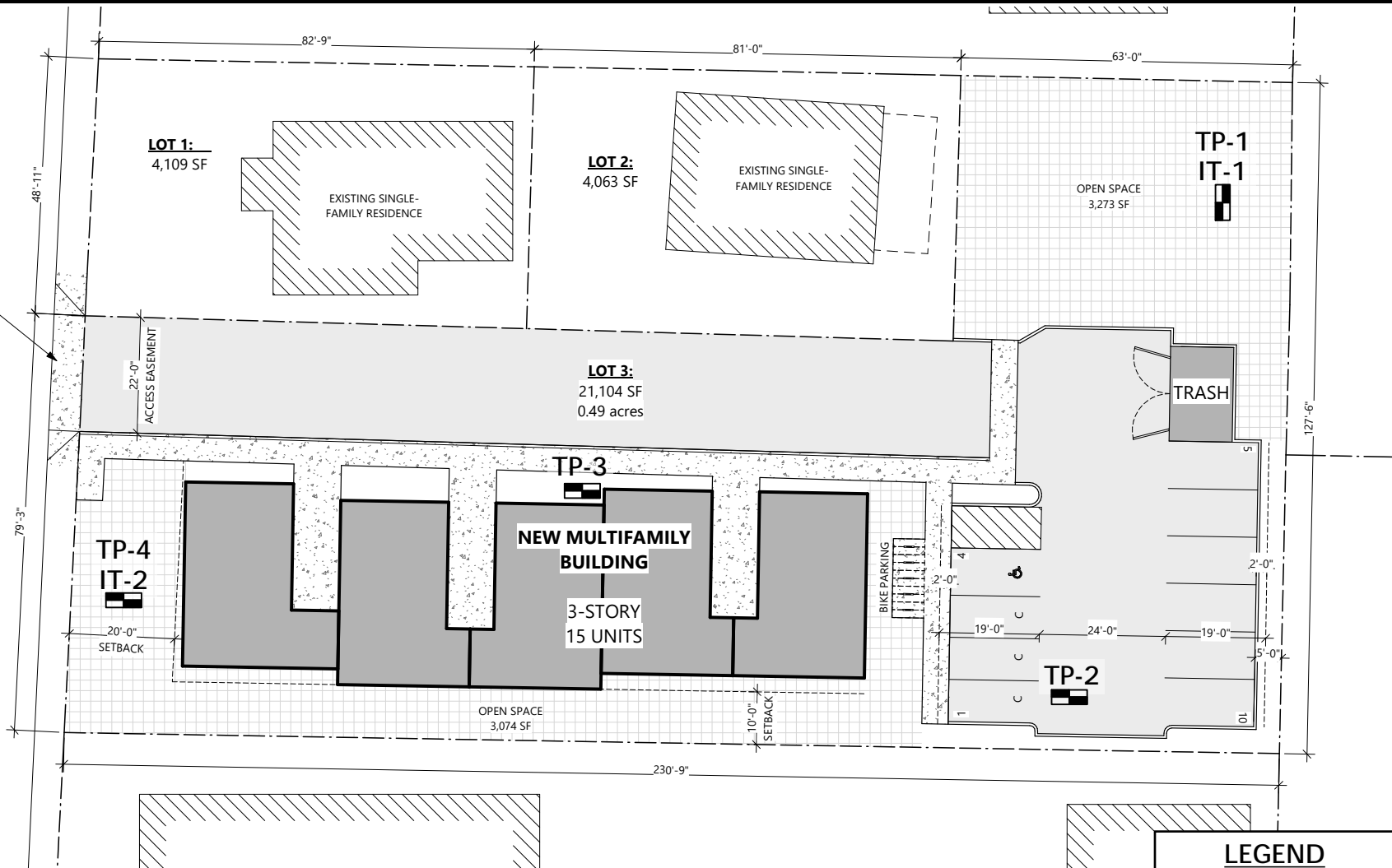
Ronald J. Derrick, P.E., G.E.
Principal Geotechnical Engineer

ATTACHED:


Figure-1, Site Vicinity Map
Figure-2, Site Exploration Map
ORWD Well Logs (3)
USDA NRCS Site Soil Mapping and Soil Description

**D STREET
(50' ROW)**

NEW APPROACH.



LEGEND

 BEI TEST PIT
EXPLORATION/
INFILTRATION TEST
LOCATION

0 15 30
Feet



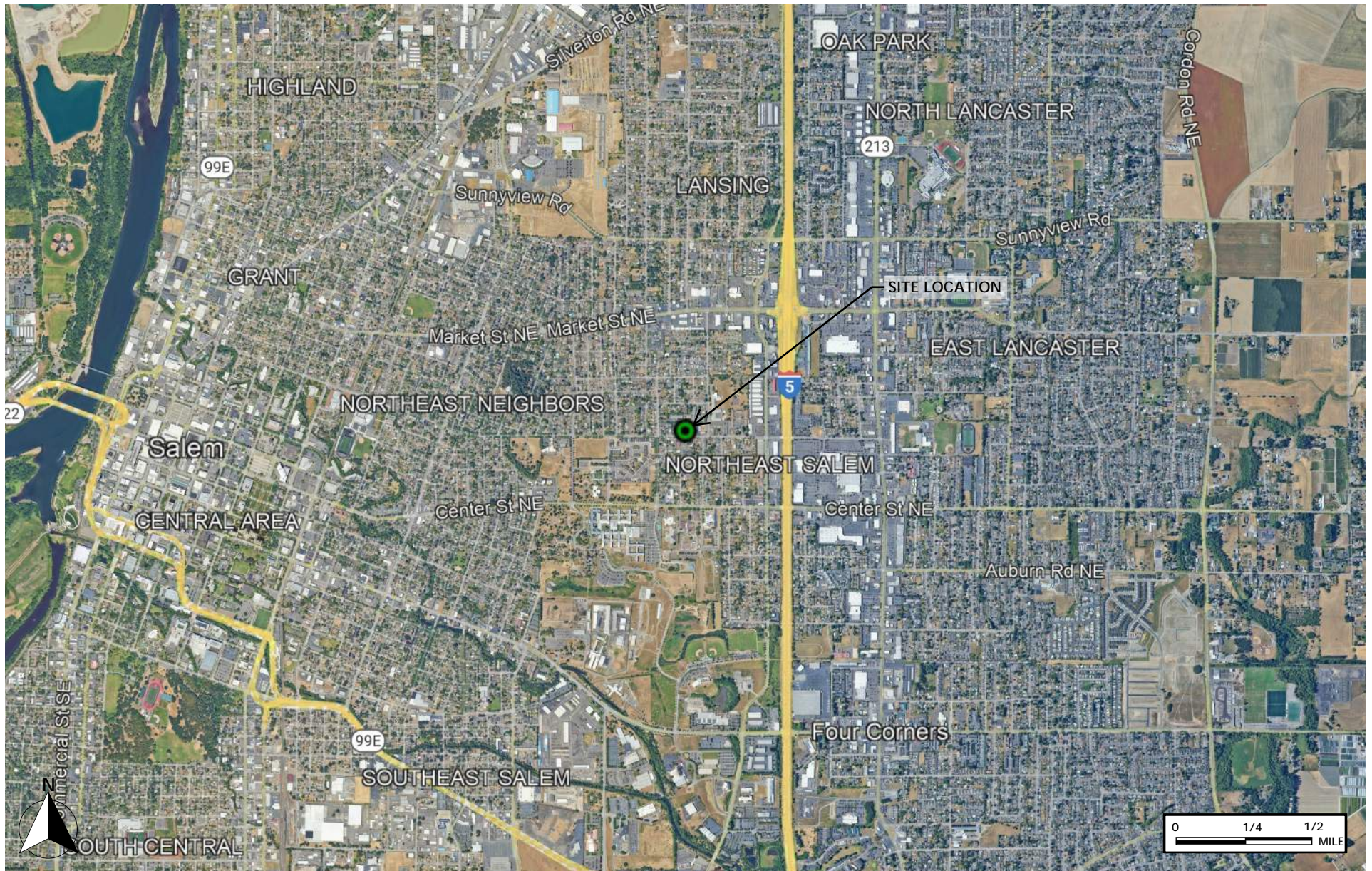
SOURCE: LIFT ARCHITECTURE, NEW MULTIFAMILY 3021 D STREET, SEET A1.01, 4/4/2024



SITE PLAN — D STREET MULTIFAMILY
3021 D STREET NE, SALEM, OREGON

FIGURE-2

PROJECT NO. 24-147



SOURCE: GOOGLE EARTH PRO®



VICINITY MAP — D STREET MULTIFAMILY
3021 D STREET NE, SALEM, OREGON

FIGURE-1

PROJECT NO. 24-147

RECEIVED

AUG 1961

MARI... 8058
MARI

WATER WELL REPORT

State Well No. 7/3W-24Q

File Original and
First Copy with the
STATE ENGINEER,
SALEM, OREGON

STATE ENGINEER
SALEM, OREGON

STATE OF OREGON

State Permit No.

(1) OWNER:

Name WALTER R. HOELCHER
Address 3281 D. ST
SALEM ORE

(2) LOCATION OF WELL:

County MARION Owner's number, if any—
1/4 1/4 Section T. 7S R. 3W W.M.
Bearing and distance from section or subdivision corner
3281 D. ST. SALEM ORE

Garden City Addition to City of Salem
Lot # 13

(3) TYPE OF WORK (check):

New Well ☒ Deepening ☐ Reconditioning ☐ Abandon ☐
If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic ☒ Industrial ☐ Municipal ☐
Irrigation ☐ Test Well ☐ Other ☐

(5) TYPE OF WELL:

Rotary ☐ Driven ☐
Cable ☒ Jetted ☐
Dug ☐ Bored ☐

(6) CASING INSTALLED:

Threaded ☐ Welded ☒
4" Diam. from 0 ft. to 90 ft. Gage 4"
" Diam. from ft. to ft. Gage
" Diam. from ft. to ft. Gage

(7) PERFORATIONS:

Perforated? ☐ Yes ☒ No

Type of perforator used

SIZE of perforations	in. by	in.
perforations from ft. to ft.		
perforations from ft. to ft.		
perforations from ft. to ft.		
perforations from ft. to ft.		
perforations from ft. to ft.		

(8) SCREENS:

Well screen installed ☐ Yes ☒ No

Manufacturer's Name

Type Model No.
Slot size Set from ft. to ft.
Diam. Slot size Set from ft. to ft.

(9) CONSTRUCTION:

Was well gravel packed? ☐ Yes ☒ No Size of gravel:
Gravel placed from ft. to ft.
Was a surface seal provided? ☒ Yes ☐ No To what depth? 1'- ft.
Material used in seal—SAHITARY SEAL
Did any strata contain unusable water? ☒ Yes ☐ No
Type of water? IRON Depth of strata 50' to 51'
Method of sealing strata off CASEP

(10) WATER LEVELS:

Static level 19 ft. below land surface Date 7-19-61
Artesian pressure lbs. per square inch Date

Log Accepted by:

[Signed] W. R. Hoelcher July 27, 1961
(Owner)

(11) WELL TESTS:

Drawdown is amount water level is lowered below static level

Was a pump test made? ☐ Yes ☐ No If yes, by whom?

Yield:	gal./min. with	ft. drawdown after	hrs.
"	"	"	"
"	"	"	"

Bailer test 15 gal./min. with 65 ft. drawdown after 1 hrs.

Artesian flow g.p.m. Date

Temperature of water 53° Was a chemical analysis made? ☐ Yes ☒ No

(12) WELL LOG:

Diameter of well 4" inches.

Depth drilled 90' ft. Depth of completed well 90' ft.

Formation: Describe by color, character, size of material and structure, and show thickness of aquifers and the kind and nature of the material in each stratum penetrated, with at least one entry for each change of formation.

MATERIAL	FROM	TO
TOPSOIL	0	2
YELLOW CLAY	2	30
BLUE CLAY	30	35
CONGLOMERATE	35	50
WATER GRAVEL	50	51
CONGLOMERATE	51	55
YELLOW CLAY	55	58
SAND FINE GRAIN	58	59
CONGLOMERATE	59	84
SAND FINE GRAIN	84	85
CONGLOMERATE	85	89
WATER GRAVEL #1"	89	90

Work started 7-17-1961 Completed 7-19-1961

(13) PUMP:

Manufacturer's Name
Type: jet H.P. 1

Well Driller's Statement:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME J. A. SHOOD + SONS
(Person, firm, or corporation) (Type or print)
Address 2505 BROOKS ST. SALEM O.

Driller's well number

[Signed] J. A. Shood
(Well Driller)

License No. 6 Date 7-18-1961

STATE OF OREGON
GEOTECHNICAL HOLE REPORT
(as required by OAR 690-240-0035)

MARI 66067

(1) OWNER/PROJECT Hole Number B1

PROJECT NAME/NBR: 3194 Knox, Ruby Garner

First Name Ruby Last Name Garner

Company _____

Address 3194 Knox Ave NE

City Salem State Or Zip 97301

(2) TYPE OF WORK ☒ New ☐ Deepening ☒ Abandonment
☐ Alteration (repair/recondition)

(3) CONSTRUCTION

☐ Rotary Air ☐ Hand Auger ☐ Hollow stem auger
☐ Rotary Mud ☐ Cable ☒ Push Probe
☐ Other _____

(4) TYPE OF HOLE:

☒ Uncased Temporary ☐ Cased Permanent
☐ Uncased Permanent ☐ Slope Stability
☐ Other _____

Other: _____ RECEIVED BY OWRD

(5) USE OF HOLE

soil testing
AUG 26 2016
SALEM, OR

(6) BORE HOLE CONSTRUCTION Special Standard ☐ (Attach copy)

Depth of Completed Hole 22.00 ft.

BORE HOLE			SEAL			sacks/lbs	
Dia	From	To	Material	From	To	Amt	
2.25	0	22					

Backfill placed from _____ ft. to _____ ft. Material _____
Filter pack from _____ ft. to _____ ft. Material _____ Size _____

(7) CASING/SCREEN

Casing	Screen	Dia	+	From	To	Gauge	Stl	Plstc	Wld	Thrd
<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	.75		0	10	40	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>	.75		10	22	40	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>						<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>						<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

(8) WELL TESTS

☐ Pump ☐ Bailer ☐ Air ☐ Flowing Artesian

Yield gal/min	Drawdown	Drill stem/Pump depth	Duration(hr)

Temperature NA °F Lab analysis ☐ Yes By _____

Supervising Geologist/Engineer _____

Water quality concerns? ☐ Yes (describe below)

From	To	Description	Amount	Units

(9) LOCATION OF HOLE (legal description)

County MARION Twp 7 S N/S Range 3 W E/W WM

Sec 24 SW 1/4 of the SW 1/4 Tax Lot 05400

Tax Map Number _____ Lot _____

Lat _____ " or _____ DMS or DD

Long _____ " or _____ DMS or DD

☒ Street address of hole ☐ Nearest address

3194 Knox Ave NE Salem Oregon

(10) STATIC WATER LEVEL

	Date	SWL(psi)	+	SWL(ft)
Existing Well / Predeepening				<u>N/A</u>
Completed Well				<u>N/A</u>

Flowing Artesian? ☐

WATER BEARING ZONES Depth water was first found N/A

SWL Date	From	To	Est Flow	SWL(psi)	+	SWL(ft)
						<u>N/A</u>

(11) SUBSURFACE LOG

Ground Elevation _____

Material	From	To
Top soil fill	0	2
brown silty clay	2	8
light brown silty clay	8	22

Date Started 12-05-2015 Completed 12-05-2015

(12) ABANDONMENT LOG:

Material	From	To	Amt	sacks/lbs
Bentonite Chips	0	22	35	P

Date Started 12-05-2015 Completed 12-05-2015

Professional Certification (to be signed by an Oregon licensed water or monitoring well constructor, Oregon registered geologist or professional engineer).

I accept responsibility for the construction, deepening, alteration, or abandonment work performed during the construction dates reported above. All work performed during this time is in compliance with Oregon geotechnical hole construction standards. This report is true to the best of my knowledge and belief.

License/Registration Number 10587 Date 12/15/15

First Name Karl Last Name Van Zandt

Affiliation Enviroprobe NW LLC

MARI 66067

Knox Street

Property line

House

Garage

B1

RECEIVED BY OWRD

JAN 15 2016

SALEM, OR

Scale in feet

0 5 10 15

North

● Sample

□ Tank

ENVIROPROBE NW LLC
Salem, Oregon

Site Diagram-3194 Knox Ave NE
Salem, Oregon

Figure 1

STATE OF OREGON
GEOTECHNICAL HOLE REPORT
 (as required by OAR 690-240-0035)

3/16/2016

(1) OWNER/PROJECT Hole Number B8PROJECT NAME/NBR: 5-648/DAS - SALEM

First Name _____ Last Name _____
 Company OREGON DEPARTMENT OF ADMINISTRATIVE SERVICES
 Address 155 COTTAGE ST NE
 City SALEM State OR Zip 97301

(2) TYPE OF WORK ☒ New ☐ Deepening ☒ Abandonment
☐ Alteration (repair/recondition)

(3) CONSTRUCTION

☐ Rotary Air ☐ Hand Auger ☐ Hollow stem auger
☒ Rotary Mud ☐ Cable ☐ Push Probe
☐ Other _____

(4) TYPE OF HOLE:

☒ Uncased Temporary ☐ Cased Permanent
☐ Uncased Permanent ☐ Slope Stability
☐ Other _____
 Other: _____

(5) USE OF HOLE

GEOTECHNICAL

(6) BORE HOLE CONSTRUCTION Special Standard ☐ (Attach copy)Depth of Completed Hole 20.00 ft.

BORE HOLE			SEAL			sacks/	
Dia	From	To	Material	From	To	Amt	lbs
3.87	0	20	Bentonite Chips	0	20	3	S

Backfill placed from _____ ft. to _____ ft. Material _____
 Filter pack from _____ ft. to _____ ft. Material _____ Size _____

(7) CASING/SCREEN

Casing	Screen	Dia	+	From	To	Gauge	Stl	Plstc	Wld	Thrd
<input type="checkbox"/>	<input type="checkbox"/>						<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>						<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>						<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>						<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>						<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

(8) WELL TESTS

☐ Pump ☐ Bailer ☐ Air ☐ Flowing Artesian
 Yield gal/min _____ Drawdown _____ Drill stem/Pump depth _____ Duration(hr) _____

Temperature _____ °F Lab analysis ☐ Yes By _____

Supervising Geologist/Engineer _____

Water quality concerns? ☐ Yes (describe below) TDS amount _____
 From _____ To _____ Description _____ Amount _____ Units _____

(9) LOCATION OF HOLE (legal description)

County MARION Twp 7.00 S N/S Range 3.00 W E/W WM
 Sec 24 SE 1/4 of the SW 1/4 Tax Lot 100
 Tax Map Number _____ Lot _____
 Lat _____ " or 44.94238889 DMS or DD
 Long _____ " or -123.00056944 DMS or DD
☐ Street address of hole ☒ Nearest address

901 PARK AVE NE SALEM, OR**(10) STATIC WATER LEVEL**

Date _____ SWL(psi) _____ + SWL(ft) _____
 Existing Well / Predeepening _____
 Completed Well _____

Flowing Artesian? ☐
 WATER BEARING ZONES Depth water was first found _____

SWL Date	From	To	Est Flow	SWL(psi)	+	SWL(ft)

(11) SUBSURFACE LOG Ground Elevation _____

Material	From	To
Silt & Some Clay	0	10
Sandy Silt	10	20

Date Started 3/10/2016 Completed 3/10/2016**(12) ABANDONMENT LOG:**

Material	From	To	Amt	sacks/
Bentonite Chips	0	20	3	S

Date Started 3/10/2016 Completed 3/10/2016

Professional Certification (to be signed by an Oregon licensed water or monitoring well constructor, Oregon registered geologist or professional engineer).

I accept responsibility for the construction, deepening, alteration, or abandonment work performed during the construction dates reported above. All work performed during this time is in compliance with Oregon geotechnical hole construction standards. This report is true to the best of my knowledge and belief.

License/Registration Number 10607 Date 3/16/2016

First Name ADONIS Last Name PABLO
 Affiliation WESTERN STATES SOIL CONSERVATION

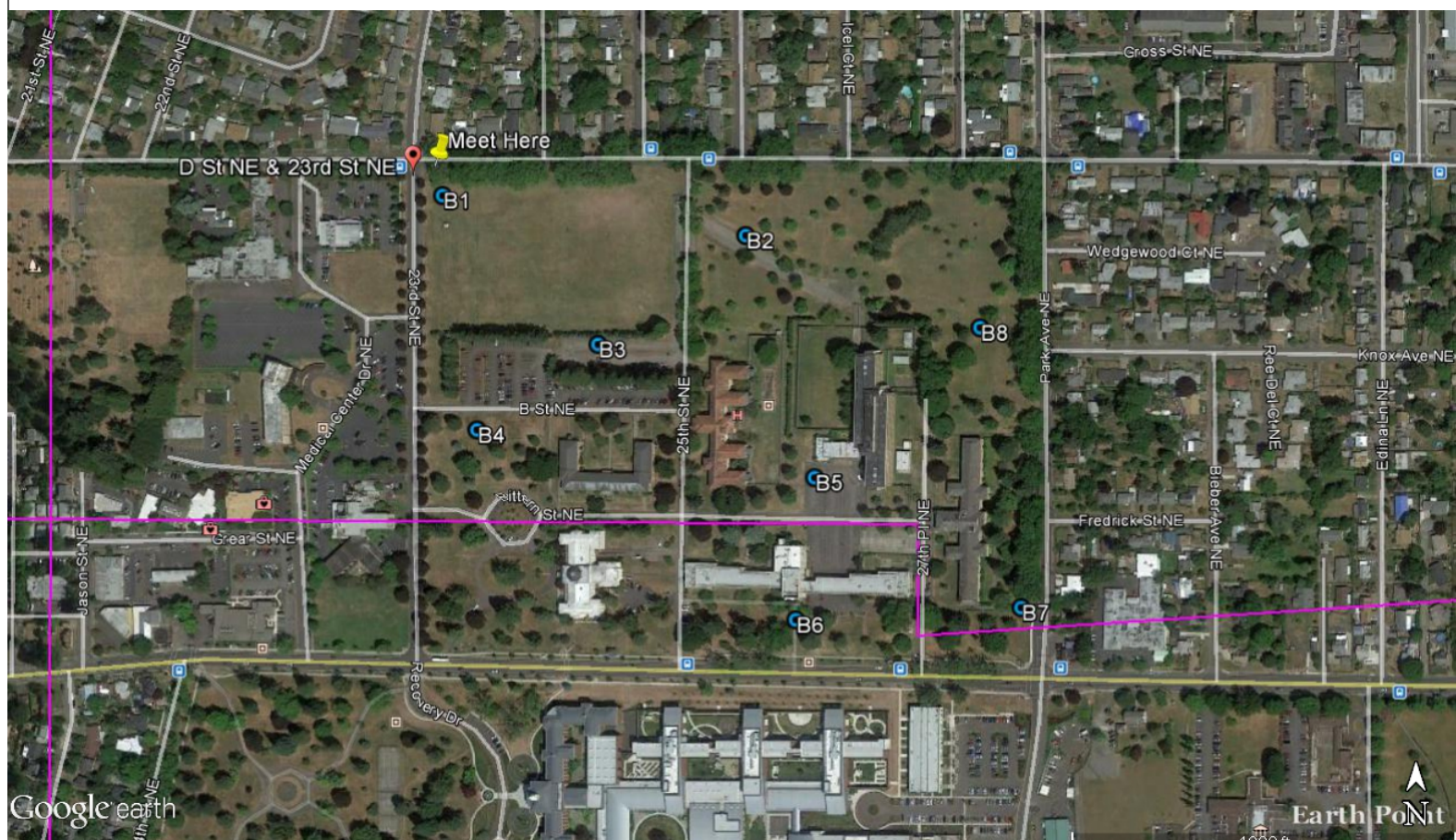
ORIGINAL - WATER RESOURCES DEPARTMENT

THIS REPORT MUST BE SUBMITTED TO THE WATER RESOURCES DEPARTMENT WITHIN 30 DAYS OF COMPLETION OF WORK

Form Version:

3/16/2016

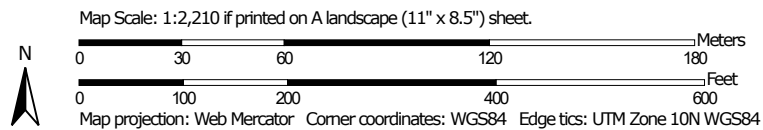
Map of Hole



Soil Map—Marion County Area, Oregon
(3021 D Street NE, Salem OR)



Soil Map may not be valid at this scale.




Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey


5/21/2024
Page 1 of 3

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Marion County Area, Oregon

Survey Area Data: Version 21, Sep 8, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 17, 2023—Jun 3, 2023

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Am	Amity silt loam	3.8	16.0%
WuA	Woodburn silt loam, 0 to 3 percent slopes	19.8	84.0%
Totals for Area of Interest		23.5	100.0%

Marion County Area, Oregon

WuA—Woodburn silt loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 24s3

Elevation: 150 to 350 feet

Mean annual precipitation: 40 to 45 inches

Mean annual air temperature: 52 to 54 degrees F

Frost-free period: 200 to 210 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Woodburn and similar soils: 85 percent

Minor components: 1 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Woodburn

Setting

Landform: Terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty alluvium and mixed mineralogy loess

Typical profile

H1 - 0 to 17 inches: silt loam

H2 - 17 to 32 inches: silty clay loam

H3 - 32 to 68 inches: silt loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water

(Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 25 to 32 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 12.0 inches)

Interpretive groups

Land capability classification (irrigated): 2w

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C

Ecological site: R002XC008OR - Valley Terrace Group

Forage suitability group: Moderately Well Drained < 15% Slopes
(G002XY004OR)

Other vegetative classification: Moderately Well Drained < 15%
Slopes (G002XY004OR)

Hydric soil rating: No

Minor Components

Aquolls, somewhat poorly drained

Percent of map unit: 1 percent

Landform: Terraces

Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Marion County Area, Oregon

Survey Area Data: Version 21, Sep 8, 2023

Hydric soil rating: No

Minor Components

Aquolls, somewhat poorly drained

Percent of map unit: 1 percent

Landform: Terraces

Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Marion County Area, Oregon

Survey Area Data: Version 21, Sep 8, 2023