PRELIMINARY DRAINAGE ANALYSIS FOR

Compass Points Apartments Salem, Oregon

September 20, 2024





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INTRODUCTION

The Compass Point Apartments is a 120 unit multi-family development project located at 1709 Baxter Road. The parcel of land to be developed includes Tax Lot 200 and 100 of Marion County Assessor's Map 08 3W 14BD. The project site area is approximately 5.04 acres in size. The property is bound by Baxter Road to the south, with Abbie Ave, Mac Street, and Snowball Ave all stubbing to the property boundaries on the west and east. An aerial image can be seen below, with the approximate project area outlined in ORANGE.



Figure 1: Project Site

Green Stormwater Infrastructure (GSI) to the Maximum Extent Feasible (MEF) will be used for the new developed areas per City of Salem Administrative Rules, Chapter 109, Division 004, Stormwater System, (Standards). All facilities will be constructed to meet the City of Salem standards.

EXISTING CONDITIONS

The portion of the property to be developed is roughly square in shape. The property is bound by Baxter Road to the south. Surface conditions consist of lawn, with the property having one residential home and

three additional out-buildings. The topographical high point of the property is at the approximate location of the residential home, with the property sloping away in all directions. The average slope across the property ranges from 3 to 6%. There are no offsite properties draining to or through the subject property.

Given the topography, this property drains to two different drainage basins. The majority of the property drains to the east, with a smaller portion draining to the west. The attached Existing Conditions map shows the area that drains to the west, measuring to be 56,632 square feet. This design considers the development of the multi-family project as well as the accompanying public improvements. For this reason, the area used for the total site in this analysis is 5.21 acres (226,914 square feet). The portion draining to the west is approximately 3.91 acres (170,282 square feet).

There are some existing trees on the property. The majority of the significant trees are in the location of proposed public improvements and will need to be removed.

Time of concentration was calculated separately for the property draining to the east and the west. The worksheets can be found in Appendix C.

Table 1: Pre-developed Drainage Basin Summary

	Con	tributing Ar	rea (ft²)		
Basin	Impervious CN = 98	Pervious CN = 74	Predeveloped CN=72	CN	Tc (min)
West			56,632	72	26.45
East			170,282	72	30.35

SOILS

The preliminary soils information was obtained from the National Resource Conservation Services Web Soil Survey. The soil map and accompanying information can be found in Appendix B. The soils on the site consists of Nekia Silty Clay which is classified as hydrologic soil group C. As required by the City of Salem Stormwater Standards, the existing conditions curve number of HSG C of 72 is used for the analysis.

A geotechnical investigation has not been formalized at this time. For the purposes of preliminary design, it will be assumed that the soil does not allow for infiltration. As such, the facility will not include an output for natural infiltration and the sizing of the facility will be conservative. An percolation test will be conducted and used for the final design.

DEVELOPED CONDITIONS

The multi-family project will consist of 120 living units, varying from 1 bedroom/1 bathroom units to 3 bedroom/2 bathroom units. Additional structures included in the project are a recreation building,

pavilion, covered mail area, and a pump house. A total of 167 parking stalls are proposed as well as 120 bike parking stalls.

The development of the site also includes the construction of Snowline Street around the project, connecting Mac Street to Baxter Road. Abbie Ave will also have a cul-de-sac constructed.

The table below summaries the impervious and pervious surface totals. For this analysis, a curve number of 98 is used for the impervious surfaces and a curve number of 74 is used for the pervious surfaces, which consist of landscaping. A time of concentration of 5 was used for both basins.

	Contri	buting Area	(ft ²)		
Basin	Impervious	Pervious		CN	Tc (min)
	CN = 98	CN=74	TOTAL		
West	23613	12981	36594	89	5
East	135350	54,970	190,320	91	5

Table 2: Developed Drainage Basin Summary

The total area draining to the west does not equal the predeveloped area draining to the west. This will be discussed in the next section, but is a function of grading the total site for accessibility.

EXPLANATION OF DESIGN

The propose site straddles two drainage basins, with a portion draining to the west while the majority drains to the east. The proposed design takes a portion of the proposed project to a facility located in the southwest corner of the property to be treated, detained and outlet to the west. Areas draining to the west include the cul-de-sac, pavilion, Buildings B, C, D, the walkways in front of Building D, and the landscaped area surrounding Buildings C and D. The remaining portion of the property will be routed to a stormwater facility to be located east of Snowline Street.

Because the proposed design is rerouting runoff that historically flows to the west to a different drainage basin, the east facility will be oversized to ensure the flowrate out does not exceed the predeveloped rate for the east basin.

The east facility will be design for this project, including the construction of Snowline Street. Plans for the development of the remaining property are not known at this time. Because of this, the facility is design for this project only. However, the facility could be expanded with a new flow control structure in the future to be used for future development.

Both the east and west facilities will be designed as combination facilities, with the treatment of the stormwater being achieved through the filtration through the growing media. The facilities will use above

ground detention and a flow control structure to restrict the flow to less than or equal to the predeveloped rate for each basin.

STORMWATER ANALYSIS

Stormwater analysis was conducted using HydroCAD 10.20 and the Santa Barbara Unit Hydrograph. This analysis considers the water quality event as well as controlling the ½ the 2, 10, 25, and 100 year storm events to their predeveloped rates. Based on the region, these storms are modeled with the NRCS Type 1A rainfall distribution. The precipitation depths listed in the table below come from the City of Salem Stormwater Design Standards.

Storm Event	24-hour Rainfall Depth (in)
Water Quality	1.38
1/2 - 2 year	1.1
10 year	3.2
25 year	3.6
100 year	4.4

Table 3: City of Salem 24-hour Rainfall Depths (in)

Analysis was done for the west and east basins independently. The flow from each facility is designed to not exceed the predeveloped rate. Because infiltration is not considered in the preliminary design and to provide the most conservative preliminary design, storage is only considered above the growing media.

The table below shows the predeveloped flowrates calculated for both the west and east basins. Please note that these values are based on only the area impacted by this project. This means that the area of property left undeveloped has not been included in any of the analysis and is not artificially inflating the allowable runoff rate.

Storm Event	Basin			
Stormevent	West	East		
1/2 - 2 year	0.003	0.014		
10 year	0.134	0.698		
25 year	0.189	0.984		
100 year	0.312	1.621		

Table 4: Allowable Predeveloped Flowrate (cfs)

WATER QUALITY ANALYSIS

For the analysis of the water quality storm, treatment is assumed to be achieved to the City of Salem standards once the water infiltrates through the growing media. The infiltration rate through the growing media is assumed to be 2 inches per hour.

The east facility is modeled in the preliminary phase as 1,200 square feet, with the growing media at an elevation of 502.00. The west facility is modeled in the preliminary phase as 7,000 square feet, with the growing media at an elevation of 482.00. These elevations are preliminary and subject to change during the final design phase. It is likely that the east facility will require retaining walls do to the topography sloping down in this area. The west facility will likely need some retaining walls as well for the same reason. The slope in both of these areas exceeds 5% for the west and 8% to the east. These are the low points in both directions.

The table below gives a summary of the proposed facilities and the water depth modeled.

Table 5: Water Quality Summary

Basin	Facility Size (ft ²)	Growing Media Elevation	WQ Water Depth (feet)
West	1200	502.00	0.96
East	7000	482.00	0.33

Both facilities are able to treat the stormwater through the growing media.

WATER QUANTITY ANALYSIS

The west and east facilities are both design to detain the stormwater to the predeveloped rate for each basin. The east facility is designed for only the runoff generated from this project. The table below summarizes the facilities.



		Storm Event	Predeveloped Flowrate (cfs)	Orifice#	Orifice Diameter	Orifice 日evation	Developed Flowrate (cfs)	Water Depth (ft)
				;			· · · ·	,
		1/2 - 2 year	0.003	1	0.3	502.00	0.003	1.37
	West	10 year	0.134	2	3.7	504.00	0.134	2.28
	Ň	25 year	0.189	2	3.7	504.00	0.184	2.41
Basin		100 year	0.312	2	3.7	504.00	0.288	2.78
Ba		1/2 - 2 year	0.014	1	0.3	482.00	0.003	1.44
	East	10 year	0.698	2	12	485.00	0.408	3.31
	ш	25 year	0.984	2	12	485.00	0.527	3.36
		100 year	1.621	2	12	485.00	0.92	3.49

Table 6: Flow Control Summary

The maximum water depth for both facilities is less than 3.5 feet. The flows are able to be controlled to at or below the predeveloped flowrates for each basin. The east basin overdetains to allow for some of the area that historically drains to the west to flow to the east, without increasing the overall flowrate into the east basin.

OPERATION AND MAINTENANCE

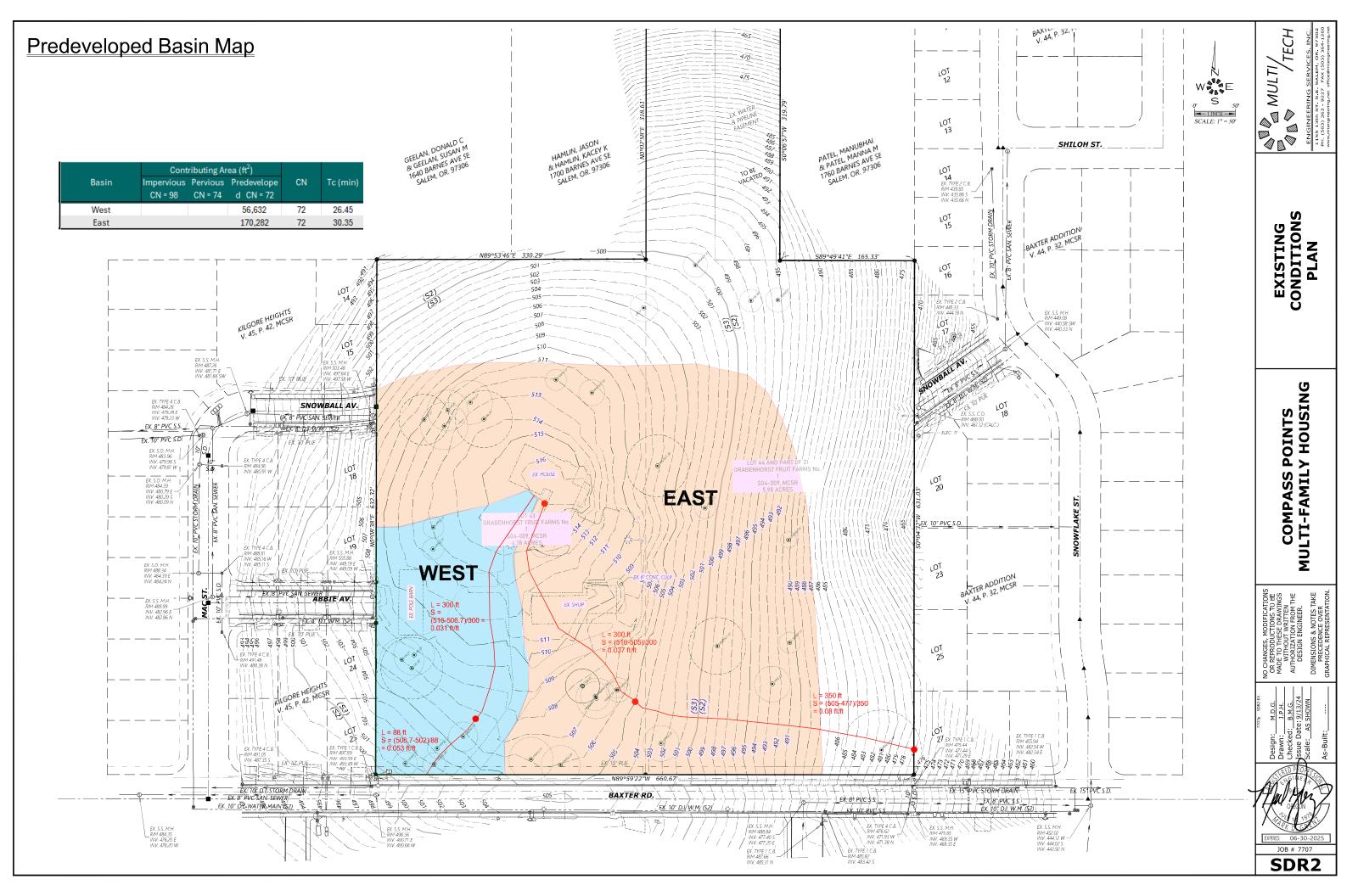
Both facilities would include public stormwater and therefore would be the responsibility of the City of Salem to maintain. The facilities will be placed in easements for the City to access for maintenance. In the future, the east facility could be placed on its own parcel, but that is not proposed at this time, since the facility may be used in the future for additional stormwater and may need to get larger.

CONCLUSIONS

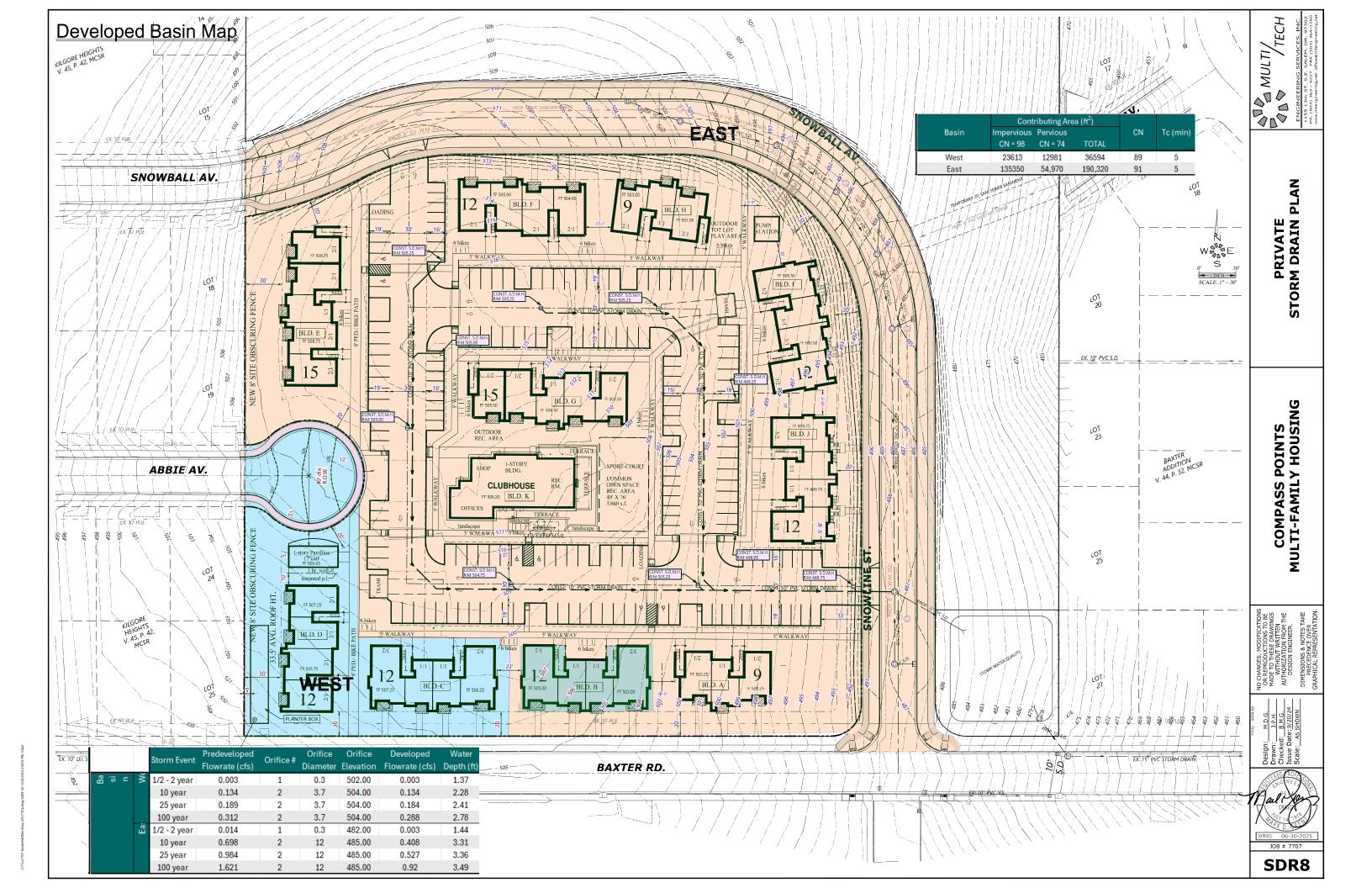
This report demonstrates a preliminary feasibility for the Compass Point Apartments. Additional design work will need to be done during the final design phase in order to more fulling comply with the City of Salem Design Standards. This will likely include acquiring design exceptions for the retaining walls that will likely be needed in the stormwater facilities and for redirecting some of the flow from the west basin to the east. If there are any questions, please contact Natalie Janney at <u>NJanney@mtengineering.net</u>.

APPENDIX A: MAPS





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APPENDIX B: SOIL INFORMATION



inter per				
	Area of Interest (AOI) Area of Interest (AOI)	Spo Sto	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:20,000.
Soils		Ner Ver	Very Stony Spot	Warning: Soil Map may not be valid at this scale.
7	Soil Map Unit Polygons		Wet Spot	Enlargement of maps beyond the scale of mapping can cause
,	Soil Map Unit Lines		Other	misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of
	Soil Map Unit Points		Special Line Features	contrasting soils that could have been shown at a more detailed
pecial Pc	Special Point Features	Water Features	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	scale.
9 E	Blowout Dorrow Dit	Str	Streams and Canals	Please rely on the bar scale on each map sheet for map
X		Transportation		measurements.
ж	Clay Spot	t Rails	ils	Source of Map: Natural Resources Conservation Service
\diamond	Closed Depression		Interstate Highways	Web Soil Survey URL: Coordinate Svstem: Web Mercator (EPSG:3857)
≫	Gravel Pit	SU	US Routes	
**	Gravelly Spot	Ma	Major Roads	projection, which preserves direction and shape but distorts
Ø	Landfill	Loc	Local Roads	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more
~	Lava Flow	Background		accurate calculations of distance or area are required.
4	Marsh or swamp	Ae	Aerial Photography	This product is generated from the USDA-NRCS certified data as
60	Mine or Quarry			Coil Curror Arno: Marian County Arno Corren
0	Miscellaneous Water			Survey Area. Marion County Area, Oregon Survey Area Data: Version 21, Sep 8, 2023
0	Perennial Water			Soil map units are labeled (as space allows) for map scales
>	Rock Outcrop			1:50,000 or larger.
+	Saline Spot			Date(s) aerial images were photographed: May 17, 2023—Jun 3 2003
•••	Sandy Spot			o, 505 The orthorhoto or other base man on which the soil lines were
Ŵ	Severely Eroded Spot			compiled and digitized probably differs from the background
0	Sinkhole			imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.
A	Slide or Slip			-
Q	Sodic Spot			

USDA Natural Resources Conservation Service

Web Soil Survey National Cooperative Soil Survey

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
NeB	Nekia silty clay loam, 2 to 7 percent slopes	3.9	41.0%
NeC	Nekia silty clay loam, 7 to 12 percent slopes	5.7	59.0%
Totals for Area of Interest		9.6	100.0%



Marion County Area, Oregon

NeB-Nekia silty clay loam, 2 to 7 percent slopes

Map Unit Setting

National map unit symbol: 24qt Elevation: 300 to 1,000 feet Mean annual precipitation: 40 to 60 inches Mean annual air temperature: 52 to 54 degrees F Frost-free period: 190 to 210 days Farmland classification: All areas are prime farmland

Map Unit Composition

Nekia and similar soils: 85 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Nekia

Setting

Landform: Hills Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Linear Parent material: Residuum weathered from tuffs and basalt

Typical profile

H1 - 0 to 9 inches: silty clay loam

- H2 9 to 36 inches: clay
- H3 36 to 40 inches: unweathered bedrock

Properties and qualities

Slope: 2 to 7 percent Depth to restrictive feature: 20 to 40 inches to lithic bedrock Drainage class: Well drained Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water supply, 0 to 60 inches: Low (about 5.2 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 3e Hydrologic Soil Group: C Ecological site: R002XC012OR - Red Hill Group Forage suitability group: Well drained < 15% Slopes (G002XY002OR)



Other vegetative classification: Well drained < 15% Slopes (G002XY002OR) *Hydric soil rating:* No

Minor Components

Aquults

Percent of map unit: 2 percent Landform: Hills Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Marion County Area, Oregon Survey Area Data: Version 21, Sep 8, 2023



Marion County Area, Oregon

NeC-Nekia silty clay loam, 7 to 12 percent slopes

Map Unit Setting

National map unit symbol: 24qv Elevation: 300 to 1,000 feet Mean annual precipitation: 40 to 60 inches Mean annual air temperature: 52 to 54 degrees F Frost-free period: 190 to 210 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Nekia and similar soils: 86 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Nekia

Setting

Landform: Hills Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Linear Parent material: Residuum weathered from tuffs and basalt

Typical profile

H1 - 0 to 9 inches: silty clay loam

- H2 9 to 36 inches: clay
- H3 36 to 40 inches: unweathered bedrock

Properties and qualities

Slope: 7 to 12 percent Depth to restrictive feature: 20 to 40 inches to lithic bedrock Drainage class: Well drained Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water supply, 0 to 60 inches: Low (about 5.2 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 3e Hydrologic Soil Group: C Ecological site: R002XC012OR - Red Hill Group Forage suitability group: Well drained < 15% Slopes (G002XY002OR)

USDA

Other vegetative classification: Well drained < 15% Slopes (G002XY002OR) *Hydric soil rating:* No

Minor Components

Aquults

Percent of map unit: 2 percent Landform: Hills Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Marion County Area, Oregon Survey Area Data: Version 21, Sep 8, 2023

APPENDIX C: TIME OF CONCENTRATION

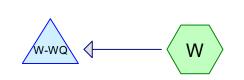
Worksheet 3: Time of Concentration (T_c) or travel time (T_t)

Project Compass Points Apartments	^{By} N. Janney		Date 9/16/2024
Location Baxter Road, Salem, Oregon	Checked		Date
Check one: I Present Developed Check one: I T _c T _t through subarea Notes: Space for as many as two segments per flow typ Include a map, schematic, or description of flow		ach worksheet.	
Sinerenalienwe egopisiesen: senore anno.		1	
Segment ID	East	West	
1. Surface description (table 3-1)	Pre-developed	Pre-develop	bed
2. Manning's roughness coefficient, n (table 3-1)	0.15	0.15	
3. Flow length, L (total L † 300 ft) ft	300	300	
4. Two-year 24-hour rainfall, P ₂ in	2.2	2.2	
5. Land slope, s ft/ft	0.037	0.031	
6. $T_t = \frac{0.007 \text{ (nL)}^{0.8}}{P_2^{0.5} \text{ s}^{0.4}}$ Compute T_t hr	0.370	0.398] =[]
Simblew concernates how			
Segment ID	East	West	
7. Surface description (paved or unpaved)	Pre-developed	Pre-develope	ed
8. Flow length, Lft	350	88	
9. Watercourse slope, s ft/ft	0.080	0.053	
10. Average velocity, V (figure 3-1) ft/s	0.72	0.57	
11. $T_t = _L$ Compute T_t hr	0.135	0.042	
Statement flow			
Segment ID			
12. Cross sectional flow area, a ft ²			
13. Wetted perimeter, p_W ft			
14. Hydraulic radius, r= — Compute r ft			
15 Channel slope, s ^p w ft/ft			
16. Manning's roughness coefficient, n			
17. V = $1.49 r^{2/3} s^{1/2}$ Compute Vft/s			
n 18. F low l ength, L ft			
19. $T_t = \frac{L}{3600 \text{ V}}$ Compute T_t	-	+	
3600 V 20. Watershed or subarea T_c or T_t (add T_t in steps 6, 11, an	d 19)		Hr

T(east) = 0.370 + 0.135 = 0.505 hours = 30.35 min

 $= T(west) = 0.398 + 0.0.42 = 0.0.440 \text{ hours} = 0.210 \text{ V} \text{ TR-55, Second E}^{26.45 \text{ min}}$

APPENDIX D: WATER QUALITY HYDROGRAPHS



West - WQ

West - POST



East - POST

West - WQ

 Subcat
 Reach
 Pond
 Link
 Routing Diagram for Prelim Hydrographs

 Prepared by Multi/Tech Engineering Service, Printed 9/20/2024
 Prepared by Multi/Tech Engineering Service, Printed 9/20/2024

 HydroCAD® 10.20-5a
 s/n 00948 © 2023 HydroCAD Software Solutions LLC

Summary for Subcatchment E: East - POST

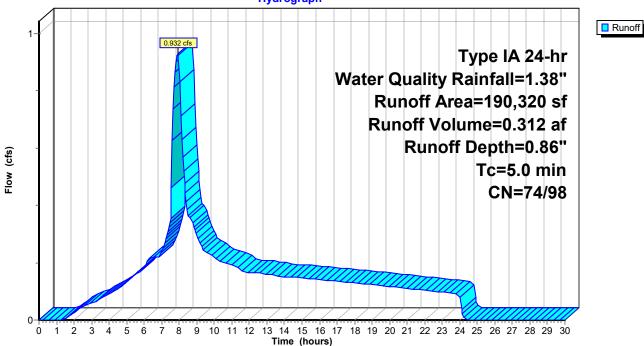
[49] Hint: Tc<2dt may require smaller dt

7.91 hrs, Volume= 0.312 af, Depth= 0.86" Runoff 0.932 cfs @ = Routed to Pond E-WQ : West - WQ

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr Water Quality Rainfall=1.38"

Ar	ea (sf)	CN	Description				
1	35,350	98	Roofs, HSG	S C			
	54,970	74	>75% Gras	s cover, Go	bod, HSG C		
1	90,320	91	Weighted A	verage			
4	54,970	74	28.88% Pervious Area				
1	35,350	98	98 71.12% Impervious Area				
Tc (min)	Length (feet)	Slop (ft/ft	,	Capacity (cfs)	Description		
5.0					Direct Entry,		

Subcatchment E: East - POST



Hydrograph

Summary for Pond E-WQ: West - WQ

[92] Warning: Device #2 is above defined storage

Inflow Area =	4.369 ac, 71.	12% Impervious, Inflow De	epth = 0.86" for Water Quality event
Inflow =	0.932 cfs @	7.91 hrs, Volume=	0.312 af
Outflow =	0.324 cfs @	7.85 hrs, Volume=	0.312 af, Atten= 65%, Lag= 0.0 min
Discarded =	0.324 cfs @	7.85 hrs, Volume=	0.312 af
Primary =	0.000 cfs @	0.00 hrs, Volume=	0.000 af

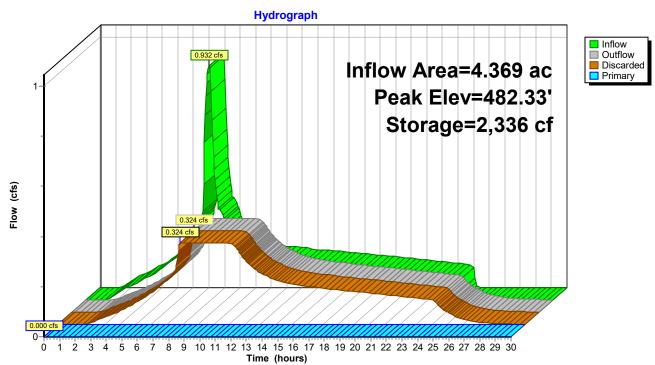
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 482.33' @ 8.86 hrs Surf.Area= 7,000 sf Storage= 2,336 cf

Plug-Flow detention time= 83.7 min calculated for 0.312 af (100% of inflow) Center-of-Mass det. time= 83.8 min (794.0 - 710.2)

Volume #1	Invert 482.00'	Avail.Stor 28,00	0 0	Description Stage Data (Pri	smatic) Listed below (Recalc)		
Elevatior (feet) 482.00 486.00)	rf.Area <u>(sq-ft)</u> 7,000 7,000	Inc.Store (cubic-feet) 0 28,000	Cum.Store (cubic-feet) 0 28,000			
#1	Routing Discarded Primary	Invert 482.00' 503.00'	Outlet Devices 2.000 in/hr Exf 18.0" Horiz. Or Limited to weir	rifice/Grate C	= 0.600		
Discarded OutFlow Max=0.324 cfs @ 7.85 hrs HW=482.22' (Free Discharge)							

1=Exfiltration (Exfiltration Controls 0.324 cfs)

Primary OutFlow Max=0.000 cfs @ 0.00 hrs HW=482.00' (Free Discharge)



Pond E-WQ: West - WQ

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Page 5

Summary for Subcatchment W: West - POST

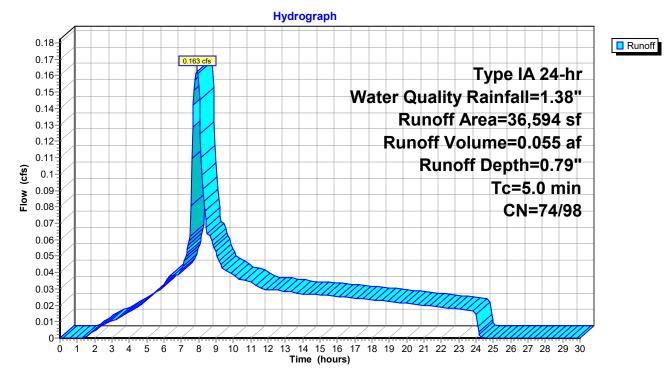
[49] Hint: Tc<2dt may require smaller dt

0.163 cfs @ 7.91 hrs, Volume= 0.055 af, Depth= 0.79" Runoff = Routed to Pond W-WQ : West - WQ

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr Water Quality Rainfall=1.38"

A	rea (sf)	CN	Description		
	23,613	98	Roofs, HSG	G C	
	12,981	74	>75% Gras	s cover, Go	ood, HSG C
	36,594 89 Weighted Average				
	12,981 74 35.47% Pervious Area				
	23,613	98	64.53% Imp	pervious Are	ea
Tc (min)	Length (feet)	Slop (ft/f		Capacity (cfs)	Description
5.0			, , , ,		Direct Entry,

Subcatchment W: West - POST



Summary for Pond W-WQ: West - WQ

Inflow Area =	0.840 ac, 64.	53% Impervious, Inflow De	pth = 0.79" for Water Quality event
Inflow =	0.163 cfs @	7.91 hrs, Volume=	0.055 af
Outflow =	0.028 cfs @	5.75 hrs, Volume=	0.055 af, Atten= 83%, Lag= 0.0 min
Discarded =	0.028 cfs @	5.75 hrs, Volume=	0.055 af
Primary =	0.000 cfs @	0.00 hrs, Volume=	0.000 af

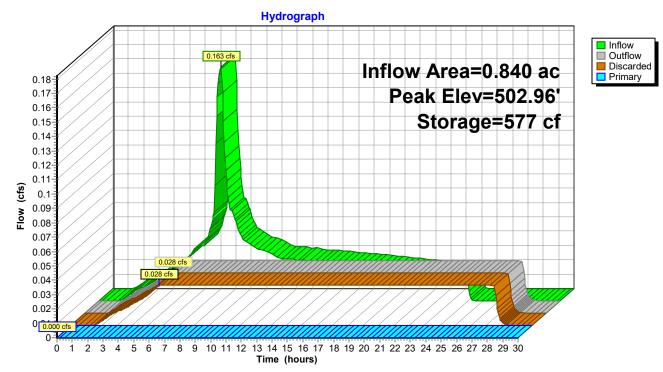
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 502.96' @ 13.51 hrs Surf.Area= 600 sf Storage= 577 cf

Plug-Flow detention time= 228.5 min calculated for 0.055 af (100% of inflow) Center-of-Mass det. time= 228.5 min (943.0 - 714.5)

Volume	Invert	Avail.Sto	rage Storage	e Description	
#1	502.00'	1,80	00 cf Custor	n Stage Data (Pri	smatic) Listed below (Recalc)
Elevatio (fee 502.0 505.0	et) 00	urf.Area (sq-ft) 600 600	Inc.Store (cubic-feet) 0 1,800	Cum.Store (cubic-feet) 0 1,800	
Device	Routing	Invert	Outlet Devic	es	
#1	Discarded	502.00'		Exfiltration over S	
#2	Primary	503.00'		Orifice/Grate C eir flow at low hea	C= 0.600 ads

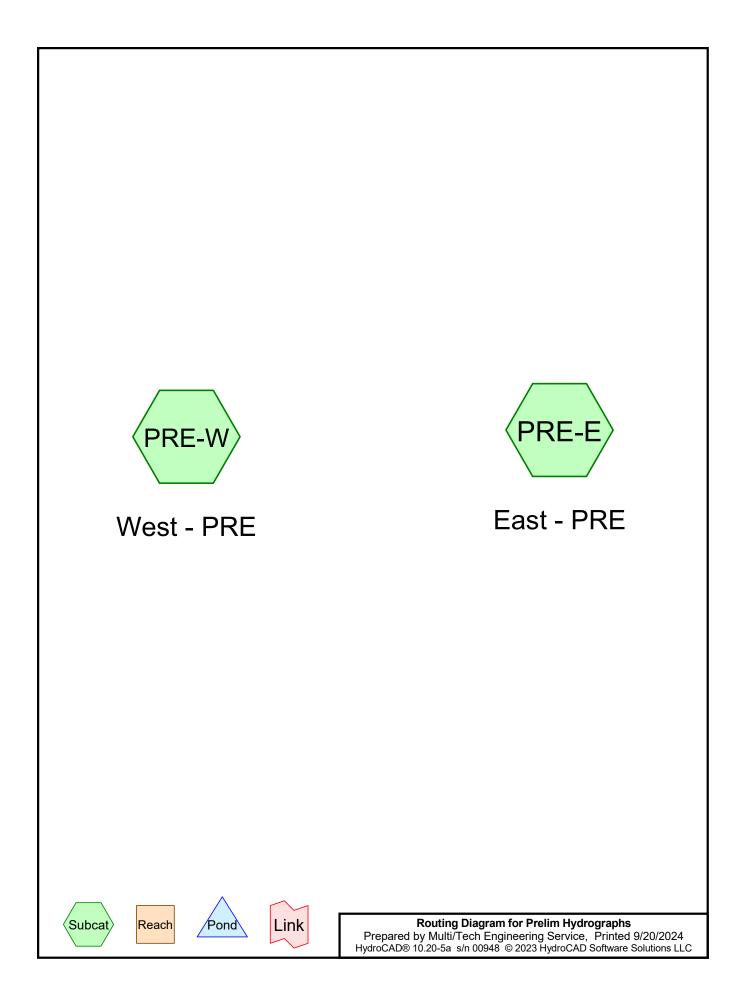
Discarded OutFlow Max=0.028 cfs @ 5.75 hrs HW=502.03' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.028 cfs)

Primary OutFlow Max=0.000 cfs @ 0.00 hrs HW=502.00' (Free Discharge) ←2=Orifice/Grate (Controls 0.000 cfs)



Pond W-WQ: West - WQ

APPENDIX E: PREDEVELOPED HYDROGRAPHS



Summary for Subcatchment PRE-E: East - PRE

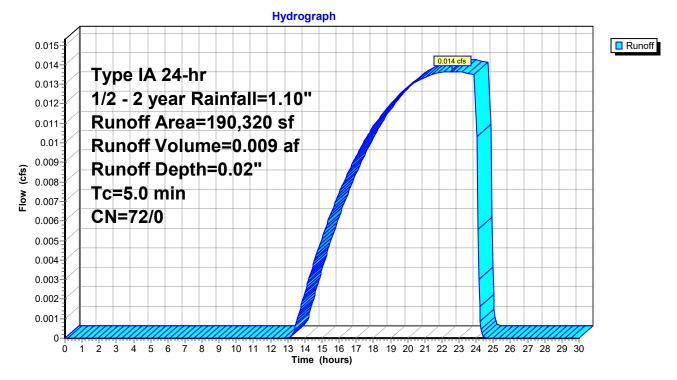
[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.014 cfs @ 22.60 hrs, Volume= 0.009 af, Depth= 0.02"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 1/2 - 2 year Rainfall=1.10"

	Area (sf)	CN	Description		
*	190,320	72	City of Sale	m, Predeve	eloped HSG C
	190,320 72 100.00% Pervious Area				ea
	Tc Length (min) (feet)	Slop (ft/f	be Velocity ft) (ft/sec)	Capacity (cfs)	Description
	5.0				Direct Entry,

Subcatchment PRE-E: East - PRE

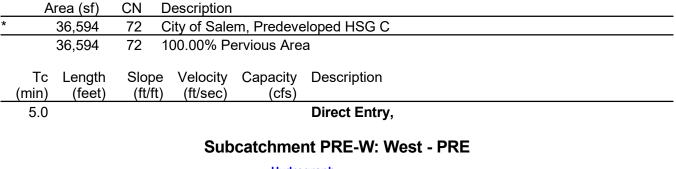


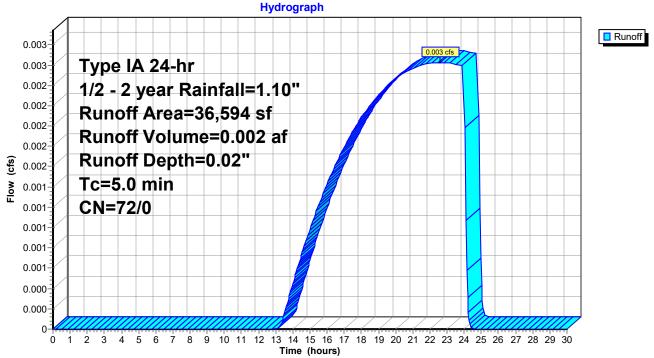
Summary for Subcatchment PRE-W: West - PRE

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.003 cfs @ 22.60 hrs, Volume= 0.002 af, Depth= 0.02"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 1/2 - 2 year Rainfall=1.10"





Summary for Subcatchment PRE-E: East - PRE

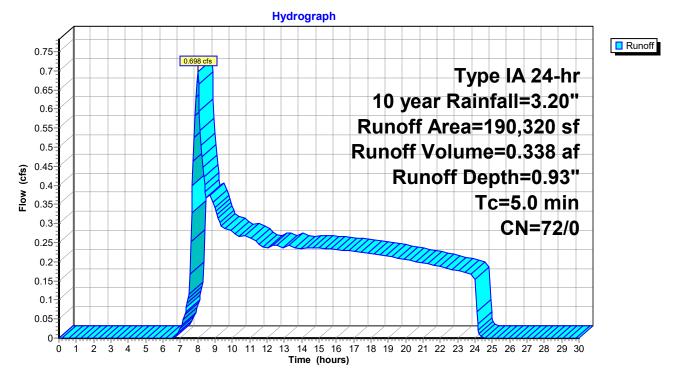
[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.698 cfs @ 8.00 hrs, Volume= 0.338 af, Depth= 0.93"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 10 year Rainfall=3.20"

	Area (sf)	CN	Description					
*	190,320	72	72 City of Salem, Predeveloped HSG C					
	190,320 72 100.00% Pervious Area			ervious Are	a			
	Tc Length (min) (feet)	Slop (ft/f	,	Capacity (cfs)	Description			
	5.0				Direct Entry,			

Subcatchment PRE-E: East - PRE



Summary for Subcatchment PRE-W: West - PRE

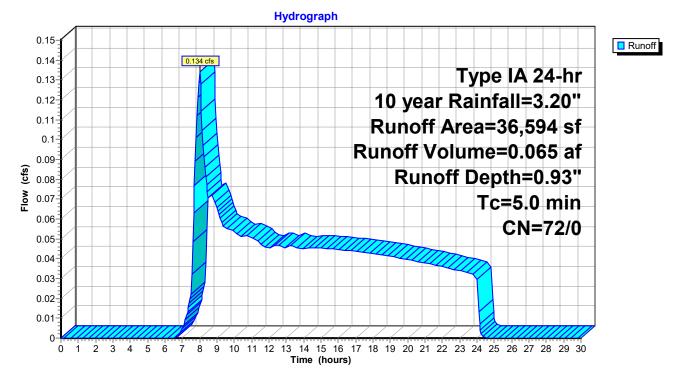
[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.134 cfs @ 8.00 hrs, Volume= 0.065 af, Depth= 0.93"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 10 year Rainfall=3.20"

	Area (sf)	CN	Description					
*	36,594	72	2 City of Salem, Predeveloped HSG C					
	36,594	72	100.00% Pe	ervious Are	a			
	Tc Length (min) (feet)	Slop (ft/1	,	Capacity (cfs)	Description			
	5.0				Direct Entry,			

Subcatchment PRE-W: West - PRE

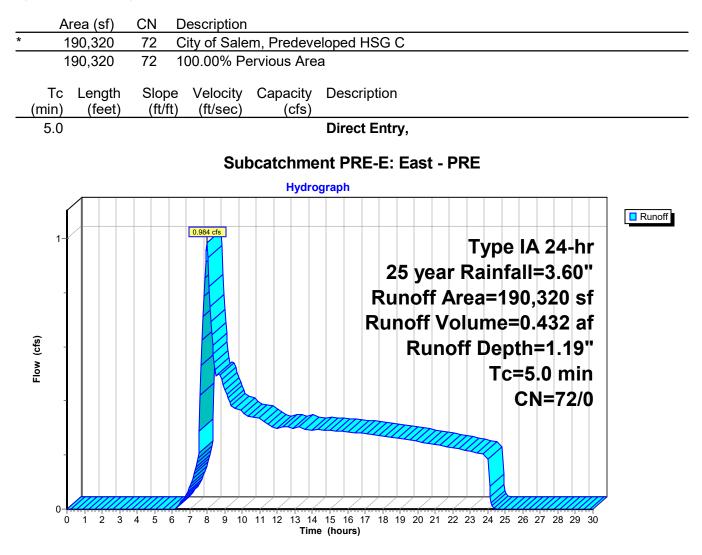


Summary for Subcatchment PRE-E: East - PRE

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.984 cfs @ 7.99 hrs, Volume= 0.432 af, Depth= 1.19"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 25 year Rainfall=3.60"



Summary for Subcatchment PRE-W: West - PRE

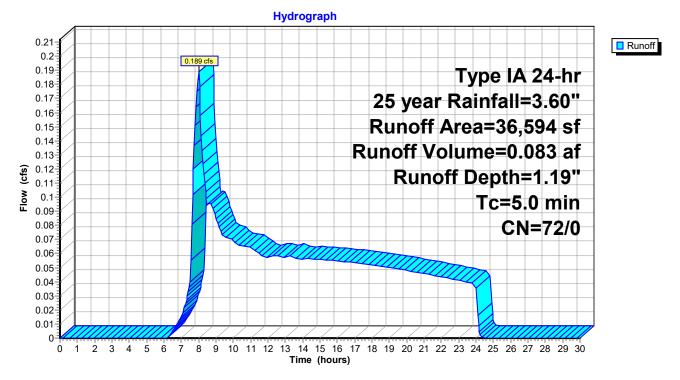
[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.189 cfs @ 7.99 hrs, Volume= 0.083 af, Depth= 1.19"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 25 year Rainfall=3.60"

	A	rea (sf)	CN I	Description					
*		36,594	72 (City of Salem, Predeveloped HSG C					
		36,594	72 ⁻	72 100.00% Pervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	5.0					Direct Entry,			

Subcatchment PRE-W: West - PRE

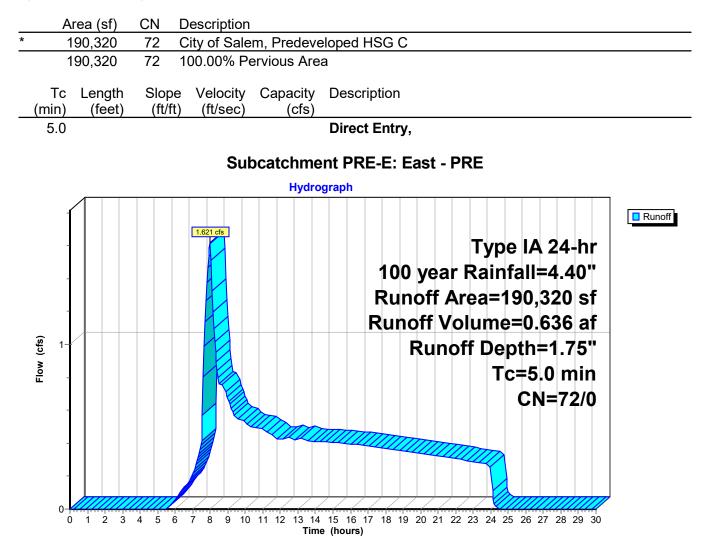


Summary for Subcatchment PRE-E: East - PRE

[49] Hint: Tc<2dt may require smaller dt

Runoff = 1.621 cfs @ 7.99 hrs, Volume= 0.636 af, Depth= 1.75"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 100 year Rainfall=4.40"



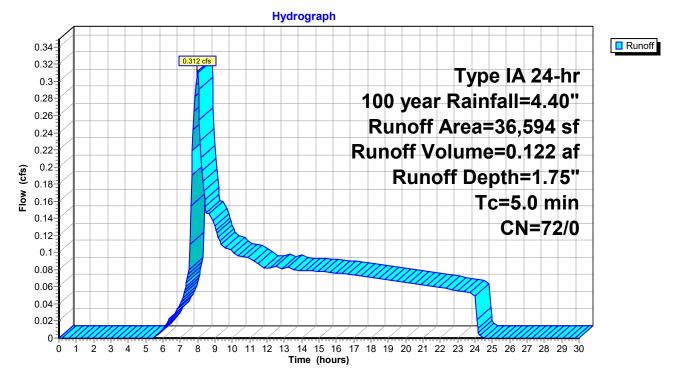
[49] Hint: Tc<2dt may require smaller dt

Runoff 0.312 cfs @ 7.99 hrs, Volume= 0.122 af, Depth= 1.75" =

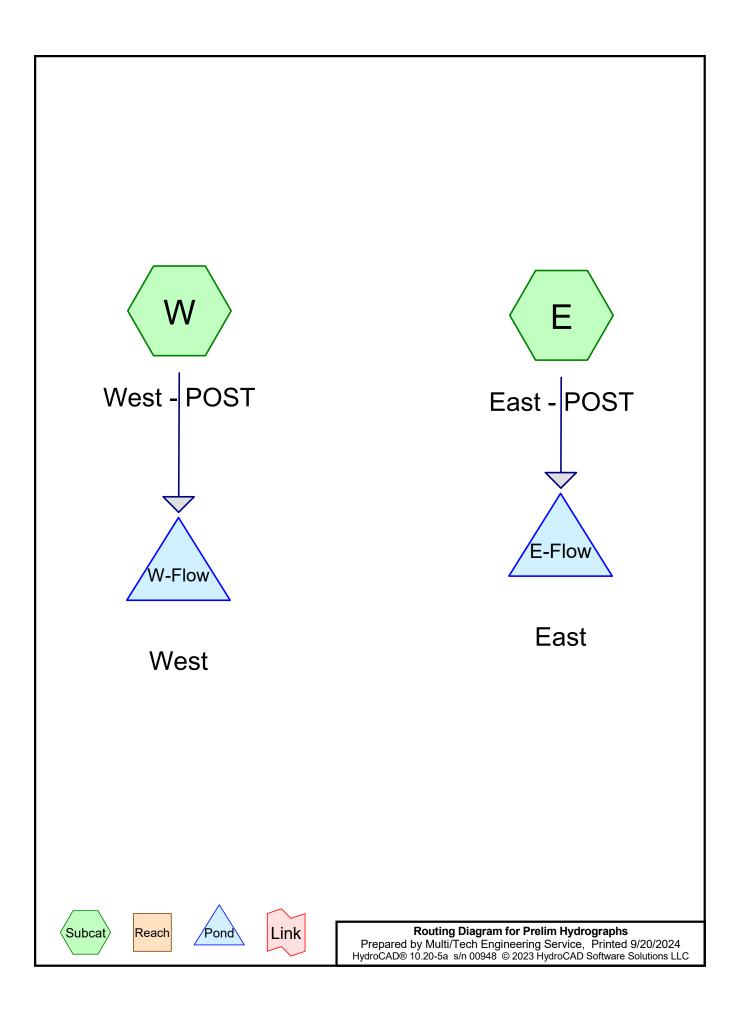
Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 100 year Rainfall=4.40"

_	Area (sf)	CN	Description						
*	36,594	72	City of Sale	City of Salem, Predeveloped HSG C					
	36,594	72	72 100.00% Pervious Area						
	Tc Length (min) (feet)	Slop (ft/f	,	Capacity (cfs)	Description				
_	5.0	-			Direct Entry,				

Subcatchment PRE-W: West - PRE



APPENDIX F: WATER QUANTITY HYDROGRAPHS



Summary for Subcatchment E: East - POST

[49] Hint: Tc<2dt may require smaller dt

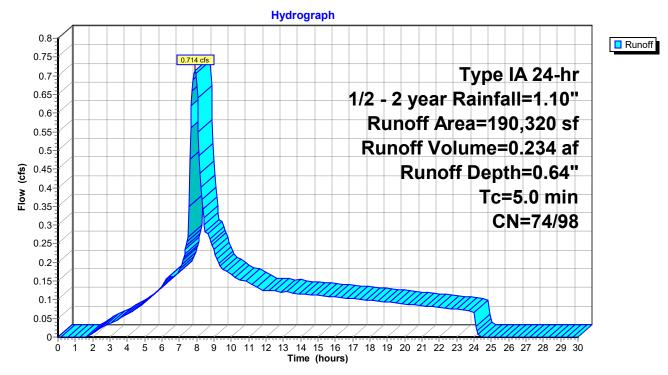
Runoff = 0.714 cfs @ 7.92 hrs, Volume= Routed to Pond E-Flow : East

0.234 af, Depth= 0.64"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 1/2 - 2 year Rainfall=1.10"

Are	ea (sf)	CN	Description				
13	35,350	98	Roofs, HSC	G C			
5	54,970	74	>75% Gras	s cover, Go	ood, HSG C		
19	90,320	91	Weighted Average				
5	54,970	74	28.88% Per	rvious Area	3		
13	35,350	98	71.12% Imp	pervious Are	rea		
Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)	Description		
5.0					Direct Entry,		

Subcatchment E: East - POST

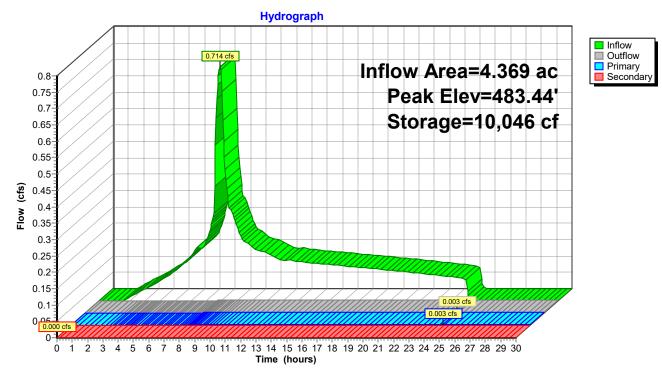


Summary for Pond E-Flow: East

Inflow Area =	4.369 ac, 71.12% Impervious, Inflow De	pth = 0.64" for 1/2 - 2 year event					
Inflow = 0.714 cfs @ 7.92 hrs, Volume= 0.234 af							
Outflow =	0.003 cfs @ 24.29 hrs, Volume=	0.005 af, Atten= 100%, Lag= 982.6 min					
Primary =	0.003 cfs @ 24.29 hrs, Volume=	0.005 af					
Secondary =	0.000 cfs @ 0.00 hrs, Volume=	0.000 af					
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 483.44' @ 24.29 hrs Surf.Area= 7,000 sf Storage= 10,046 cf							
Plug-Flow detention time= 951.3 min calculated for 0.005 af (2% of inflow) Center-of-Mass det. time= 417.2 min(1,133.7 - 716.4)							

Volume	Invert	Avail.Stor	rage Storage	e Description			
#1	482.00'	28,00	0 cf Custon	n Stage Data	(Prismatic)) Listed below (Recalc)	
Elevatio (fee	t)	f.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Sto (cubic-fee			
482.0	-	7,000	0	28.0	0		
486.0	U	7,000	28,000	28,00	00		
Device	Routing	Invert	Outlet Device	es			
#1	Primary	482.00'	0.3" Horiz. C	Prifice/Grate	C= 0.600	Limited to weir flow at low heads	
#2	Secondary	485.00'	12.0" Vert. C	Prifice/Grate	C= 0.600	Limited to weir flow at low heads	
Primary OutFlow Max=0.003 cfs @ 24.29 hrs HW=483.44' (Free Discharge)							

Secondary OutFlow Max=0.000 cfs @ 0.00 hrs HW=482.00' (Free Discharge) —2=Orifice/Grate (Controls 0.000 cfs)



Pond E-Flow: East

Summary for Subcatchment W: West - POST

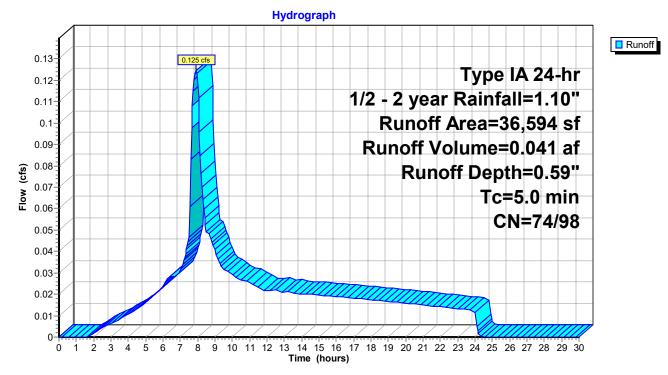
[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.125 cfs @ 7.92 hrs, Volume= Routed to Pond W-Flow : West 0.041 af, Depth= 0.59"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 1/2 - 2 year Rainfall=1.10"

A	rea (sf)	CN	Description				
	23,613	98	Roofs, HSC	G C			
	12,981	74	>75% Gras	s cover, Go	ood, HSG C		
	36,594	89	Weighted Average				
	12,981	74 35.47% Pervious Area					
	23,613	98	64.53% Imp	pervious Are	rea		
Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)	Description		
5.0					Direct Entry,		

Subcatchment W: West - POST



Summary for Pond W-Flow: West

Inflow Area =	0.840 ac, 64.53% Impervious, Inflow Dep	oth = 0.59" for 1/2 - 2 year event
Inflow =	0.125 cfs @ 7.92 hrs, Volume=	0.041 af
Outflow =	0.003 cfs @ 24.16 hrs, Volume=	0.005 af, Atten= 98%, Lag= 974.4 min
Primary =	0.003 cfs @ 24.16 hrs, Volume=	0.005 af
Secondary =	0.000 cfs @ 0.00 hrs, Volume=	0.000 af

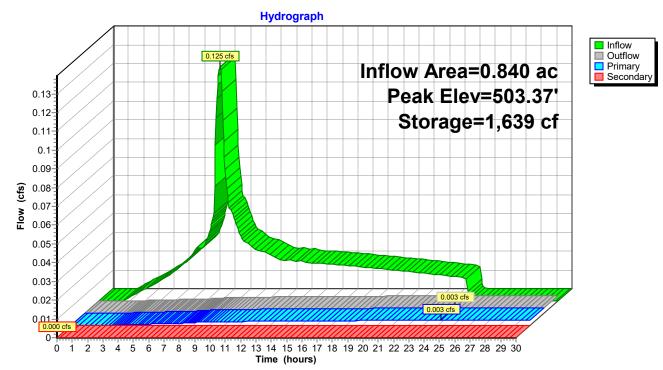
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 503.37' @ 24.16 hrs Surf.Area= 1,200 sf Storage= 1,639 cf

Plug-Flow detention time= 832.6 min calculated for 0.005 af (12% of inflow) Center-of-Mass det. time= 409.6 min (1,128.7 - 719.1)

Volume	Invert	Avail.Sto	rage Storage I	Description	
#1	502.00'	3,60	00 cf Custom	Stage Data (Prisma	atic) Listed below (Recalc)
Elevatior (feet		rf.Area (sq-ft)	Inc.Store (cubic-feet)		
502.00)	1,200	0	0	
505.00)	1,200	3,600	3,600	
Device	Routing	Invert	Outlet Devices	6	
#1	Primary	502.00'	0.3" Horiz. Or	ifice/Grate C= 0.6	600 Limited to weir flow at low heads
#2	Secondary	504.00'	3.7" Vert. Orif	ice/Grate C= 0.60	00 Limited to weir flow at low heads
Primary OutFlow Max=0.003 cfs @ 24.16 hrs HW=503.37' (Free Discharge)					

1=Orifice/Grate (Orifice Controls 0.003 cfs @ 5.63 fps)

Secondary OutFlow Max=0.000 cfs @ 0.00 hrs HW=502.00' (Free Discharge) 2=Orifice/Grate (Controls 0.000 cfs)



Pond W-Flow: West

Summary for Subcatchment E: East - POST

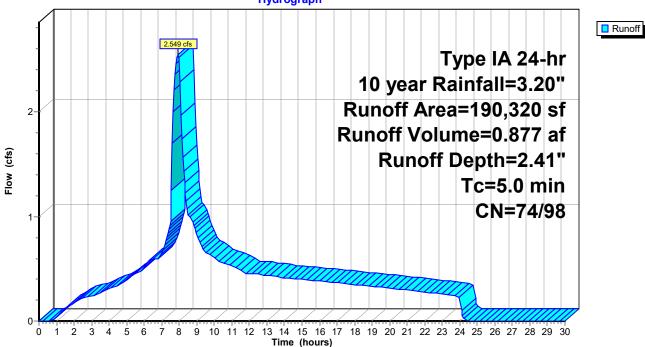
[49] Hint: Tc<2dt may require smaller dt

Runoff = 2.549 cfs @ 7.92 hrs, Volume= Routed to Pond E-Flow : East 0.877 af, Depth= 2.41"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 10 year Rainfall=3.20"

A	rea (sf)	CN	Description				
1	35,350	98	Roofs, HSG	G C			
	54,970	74	>75% Gras	s cover, Go	bod, HSG C		
1	90,320	91	1 Weighted Average				
	54,970	74	28.88% Per	vious Area	l		
1	35,350	98	98 71.12% Impervious Area				
Tc (min)	Length (feet)	Slop (ft/f		Capacity (cfs)	Description		
5.0					Direct Entry,		

Subcatchment E: East - POST



Hydrograph

Summary for Pond E-Flow: East

Inflow Area =	4.369 ac, 71.12% Impervious, In	flow Depth = 2.41" for 10 year event
Inflow =	2.549 cfs @ 7.92 hrs, Volume=	0.877 af
Outflow =	0.408 cfs @ 14.40 hrs, Volume=	0.387 af, Atten= 84%, Lag= 388.9 min
Primary =	0.004 cfs @ 14.40 hrs, Volume=	0.008 af
Secondary =	0.404 cfs @ 14.40 hrs, Volume=	0.379 af

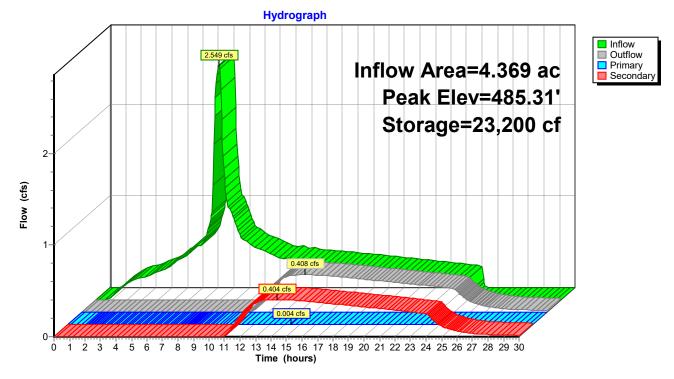
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 485.31' @ 14.40 hrs Surf.Area= 7,000 sf Storage= 23,200 cf

Plug-Flow detention time= 690.9 min calculated for 0.387 af (44% of inflow) Center-of-Mass det. time= 398.6 min (1,089.6 - 691.0)

Volume	Invert	Avail.Sto	rage Storage	e Description				
#1	482.00'	28,00	000 cf Custom Stage Data		(Prismatic)	Listed below (Recalc)		
Elevatio		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Sto (cubic-fe				
482.0	0	7,000	0		0			
486.0	0	7,000	28,000	00 28,000				
Device	Routing	Invert	Outlet Devic	es				
#1	Primary	482.00'	0.3" Horiz. (Drifice/Grate	C= 0.600	Limited to weir flow at low heads		
#2	Secondary	485.00'	12.0" Vert. 0	Drifice/Grate	C= 0.600	Limited to weir flow at low heads		
Primary	Primary OutFlow Max=0.004 cfs @ 14.40 hrs HW=485.31' (Free Discharge)							

1=Orifice/Grate (Orifice Controls 0.004 cfs @ 8.77 fps)

Secondary OutFlow Max=0.404 cfs @ 14.40 hrs HW=485.31' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.404 cfs @ 1.91 fps)



Pond E-Flow: East

Summary for Subcatchment W: West - POST

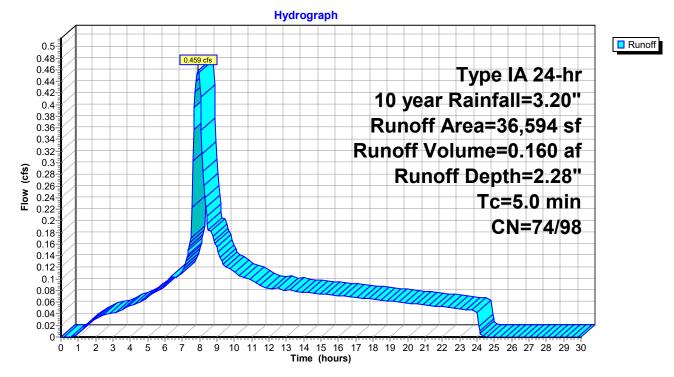
[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.459 cfs @ 7.92 hrs, Volume= Routed to Pond W-Flow : West 0.160 af, Depth= 2.28"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 10 year Rainfall=3.20"

A	rea (sf)	CN	Description					
	23,613	98	Roofs, HSG	G C				
	12,981	74	>75% Gras	s cover, Go	bod, HSG C			
	36,594	89	Weighted A	Weighted Average				
	12,981	74	35.47% Pervious Area					
	23,613	98	64.53% Impervious Area					
Tc (min)	Length (feet)	Slop (ft/f	,	Capacity (cfs)	Description			
5.0					Direct Entry,			

Subcatchment W: West - POST



Summary for Pond W-Flow: West

Inflow Area =	0.840 ac, 64.	53% Impervious, Inflow De	pth = 2.28" for 10 year event
Inflow =	0.459 cfs @	7.92 hrs, Volume=	0.160 af
Outflow =	0.134 cfs @	9.23 hrs, Volume=	0.105 af, Atten= 71%, Lag= 78.1 min
Primary =	0.004 cfs @	9.23 hrs, Volume=	0.007 af
Secondary =	0.130 cfs @	9.23 hrs, Volume=	0.098 af

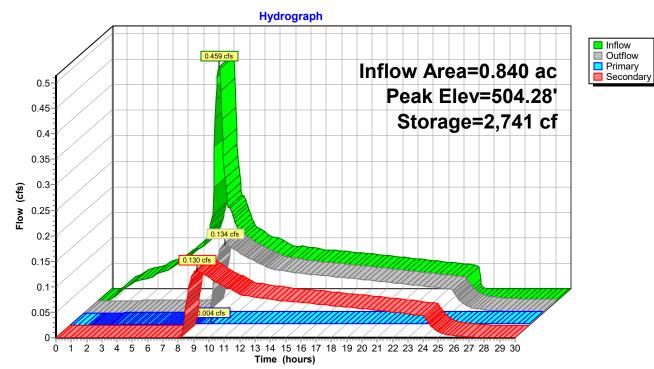
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 504.28' @ 9.23 hrs Surf.Area= 1,200 sf Storage= 2,741 cf

Plug-Flow detention time= 431.9 min calculated for 0.105 af (66% of inflow) Center-of-Mass det. time= 223.6 min (921.9 - 698.3)

Volume	Invert	Avail.Stor	rage Storage [Description		
#1	502.00'	3,60	00 cf Custom	Stage Data (Prisma	atic) Listed below (Recalc)	
Elevation (feet)		f.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
502.00)	1,200	0	0		
505.00)	1,200	3,600	3,600		
Device I	Routing	Invert	Outlet Devices	;		
#1 I	Primary	502.00'	0.3" Horiz. Ori	fice/Grate C= 0.6	600 Limited to weir flow at low heads	
#2 \$	Secondary	504.00'	3.7" Vert. Orifi	ce/Grate C= 0.60	00 Limited to weir flow at low heads	
Primary OutFlow Max=0.004 cfs @ 9.23 hrs HW=504.28' (Free Discharge)						

1=Orifice/Grate (Orifice Controls 0.004 cfs @ 7.28 fps)

Secondary OutFlow Max=0.131 cfs @ 9.23 hrs HW=504.28' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.131 cfs @ 1.81 fps)



Pond W-Flow: West

Summary for Subcatchment E: East - POST

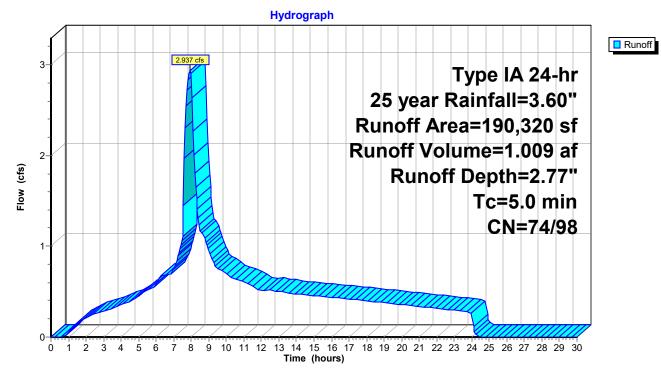
[49] Hint: Tc<2dt may require smaller dt

Runoff = 2.937 cfs @ 7.92 hrs, Volume= Routed to Pond E-Flow : East 1.009 af, Depth= 2.77"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 25 year Rainfall=3.60"

Are	a (sf)	CN	Description			
135	5,350	98	Roofs, HSG	S C		
54	4,970	74	>75% Gras	s cover, Go	ood, HSG C	
190	0,320	91	Weighted Average			
54	4,970	74	28.88% Pervious Area			
135	5,350	98	71.12% Impervious Area			
Tc L (min)	_ength (feet)	Slop (ft/f	,	Capacity (cfs)	Description	
5.0					Direct Entry,	

Subcatchment E: East - POST



Summary for Pond E-Flow: East

Inflow Area =	4.369 ac, 71.12% Impervious, Inflow De	pth = 2.77" for 25 year event
Inflow =	2.937 cfs @ 7.92 hrs, Volume=	1.009 af
Outflow =	0.527 cfs @ 11.72 hrs, Volume=	0.519 af, Atten= 82%, Lag= 228.5 min
Primary =	0.004 cfs @_ 11.72 hrs, Volume=	0.009 af
Secondary =	0.523 cfs @ 11.72 hrs, Volume=	0.510 af

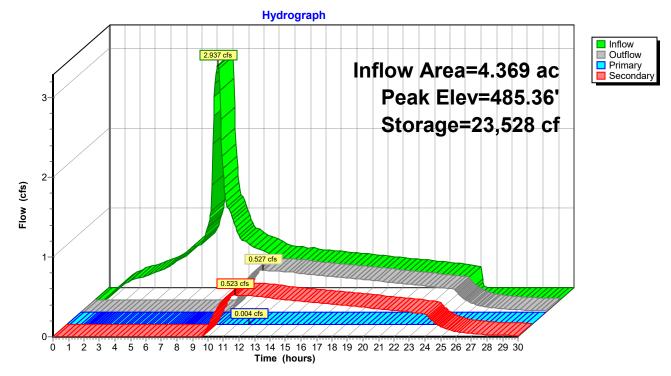
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 485.36' @ 11.72 hrs Surf.Area= 7,000 sf Storage= 23,528 cf

Plug-Flow detention time= 604.5 min calculated for 0.518 af (51% of inflow) Center-of-Mass det. time= 337.8 min (1,026.4 - 688.6)

Volume	Invert	Avail.Sto	rage Storage	e Description				
#1	482.00'	28,00	00 cf Custon	n Stage Data	(Prismatic)	Listed below (Recalc)		
Elevatior (feet		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Sto (cubic-fe				
482.00	D	7,000	0		0			
486.00	C	7,000	28,000	28,0	00			
Device	Routing	Invert	Outlet Devic	es				
#1	Primary	482.00'	0.3" Horiz. C	Drifice/Grate	C= 0.600	Limited to weir flow at low heads		
#2	Secondary	485.00'	12.0" Vert. C	Drifice/Grate	C= 0.600	Limited to weir flow at low heads		
Primary	Primary OutFlow Max=0.004 cfs @ 11.72 hrs HW=485.36' (Free Discharge)							

1=Orifice/Grate (Orifice Controls 0.004 cfs @ 8.83 fps)

Secondary OutFlow Max=0.523 cfs @ 11.72 hrs HW=485.36' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.523 cfs @ 2.05 fps)



Pond E-Flow: East

Summary for Subcatchment W: West - POST

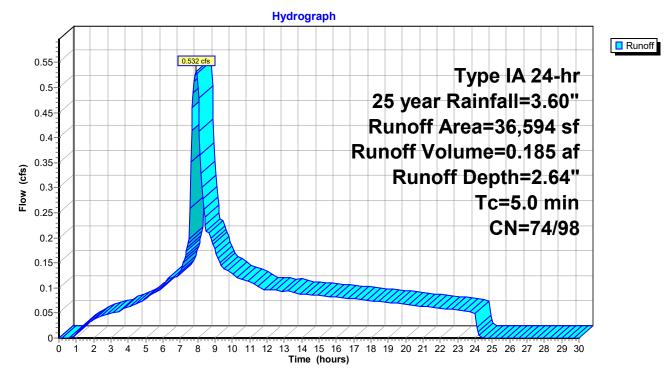
[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.532 cfs @ 7.92 hrs, Volume= Routed to Pond W-Flow : West 0.185 af, Depth= 2.64"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 25 year Rainfall=3.60"

A	rea (sf)	CN	Description			
	23,613	98	Roofs, HSG	G C		
	12,981	74	>75% Gras	s cover, Go	ood, HSG C	
	36,594	89	Weighted A	verage		
	12,981	74	35.47% Pervious Area			
	23,613	98	64.53% Imp	pervious Are	rea	
Tc	Length	Slop		Capacity	Description	
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)		
5.0					Direct Entry,	

Subcatchment W: West - POST



Summary for Pond W-Flow: West

Inflow Area =	0.840 ac, 64.	53% Impervious, Inflow De	pth = 2.64" for 25 year event
Inflow =	0.532 cfs @	7.92 hrs, Volume=	0.185 af
Outflow =	0.184 cfs @	8.92 hrs, Volume=	0.130 af, Atten= 65%, Lag= 59.9 min
Primary =	0.004 cfs @	8.92 hrs, Volume=	0.007 af
Secondary =	0.181 cfs @	8.92 hrs, Volume=	0.123 af

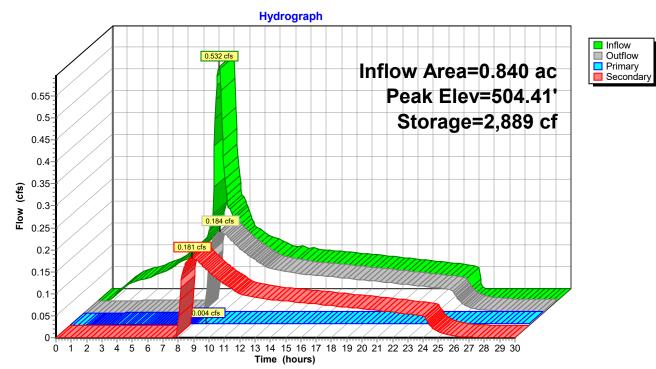
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 504.41' @ 8.92 hrs Surf.Area= 1,200 sf Storage= 2,889 cf

Plug-Flow detention time= 380.7 min calculated for 0.130 af (70% of inflow) Center-of-Mass det. time= 195.2 min (891.2 - 696.0)

Volume	Invert	Avail.Sto	rage Storage	Description		
#1	502.00'	3,60	00 cf Custom	Stage Data (Prismat	ic) Listed below (Recalc)	
Elevatior (feet		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
502.00	0	1,200	0	0		
505.00	0	1,200	3,600	3,600		
Device	Routing	Invert	Outlet Device	s		
#1	Primary	502.00'	0.3" Horiz. O	rifice/Grate C= 0.60	0 Limited to weir flow at low heads	
#2	Secondary	504.00'	3.7" Vert. Ori	fice/Grate C= 0.600	Limited to weir flow at low heads	
Primary OutFlow Max=0.004 cfs @ 8.92 hrs HW=504.41' (Free Discharge)						

1=Orifice/Grate (Orifice Controls 0.004 cfs @ 7.47 fps)

Secondary OutFlow Max=0.181 cfs @ 8.92 hrs HW=504.41' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.181 cfs @ 2.42 fps)



Pond W-Flow: West

Summary for Subcatchment E: East - POST

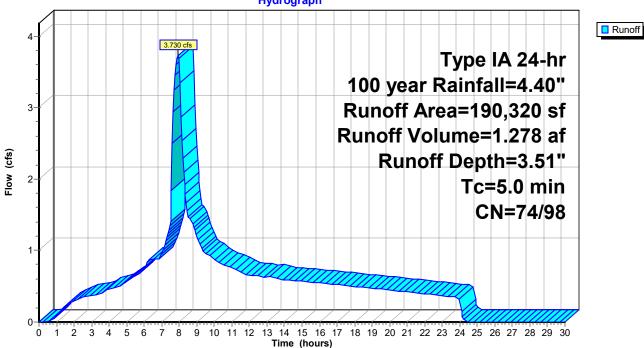
[49] Hint: Tc<2dt may require smaller dt

Runoff = 3.730 cfs @ 7.91 hrs, Volume= Routed to Pond E-Flow : East 1.278 af, Depth= 3.51"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 100 year Rainfall=4.40"

Area	(sf) C	N D	escription			
135,3	350 9	98 F	Roofs, HSG	i C		
54,9	970 7	74 >	75% Grass	s cover, Go	ood, HSG C	
190,3	320 9	91 V	Weighted Average			
54,9	970 7	74 2	28.88% Pervious Area			
135,3	350 9	98 7	1.12% Imp	ervious Are	rea	
	ngth S feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.0					Direct Entry,	

Subcatchment E: East - POST



Hydrograph

Summary for Pond E-Flow: East

Inflow Area =	4.369 ac, 71.	12% Impervious, Inflow De	pth = 3.51" for 100 year event
Inflow =	3.730 cfs @	7.91 hrs, Volume=	1.278 af
Outflow =	0.920 cfs @	9.79 hrs, Volume=	0.787 af, Atten= 75%, Lag= 112.8 min
Primary =	0.004 cfs @	9.79 hrs, Volume=	0.009 af
Secondary =	0.916 cfs @	9.79 hrs, Volume=	0.778 af

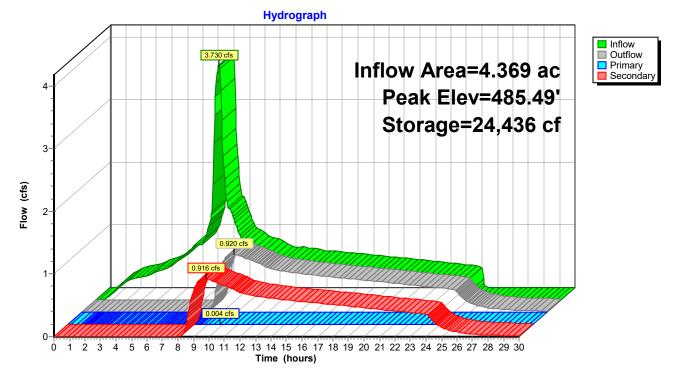
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 485.49' @ 9.79 hrs Surf.Area= 7,000 sf Storage= 24,436 cf

Plug-Flow detention time= 487.1 min calculated for 0.787 af (62% of inflow) Center-of-Mass det. time= 259.9 min (944.4 - 684.5)

Volume	Invert	Avail.Sto	rage Storage	e Description		
#1	482.00'	28,00	00 cf Custon	n Stage Data	(Prismatic)	Listed below (Recalc)
Elevatio (feet		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Sto (cubic-fe		
482.0	0	7,000	0		0	
486.0	0	7,000	28,000	28,0	00	
Device	Routing	Invert	Outlet Devic	es		
#1	Primary	482.00'	0.3" Horiz. C	Drifice/Grate	C= 0.600	Limited to weir flow at low heads
#2	Secondary	485.00'	12.0" Vert. C	Drifice/Grate	C= 0.600	Limited to weir flow at low heads
Primary OutFlow Max=0.004 cfs @ 9.79 hrs HW=485.49' (Free Discharge)						

1=Orifice/Grate (Orifice Controls 0.004 cfs @ 9.00 fps)

Secondary OutFlow Max=0.915 cfs @ 9.79 hrs HW=485.49' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.915 cfs @ 2.39 fps)



Pond E-Flow: East

Summary for Subcatchment W: West - POST

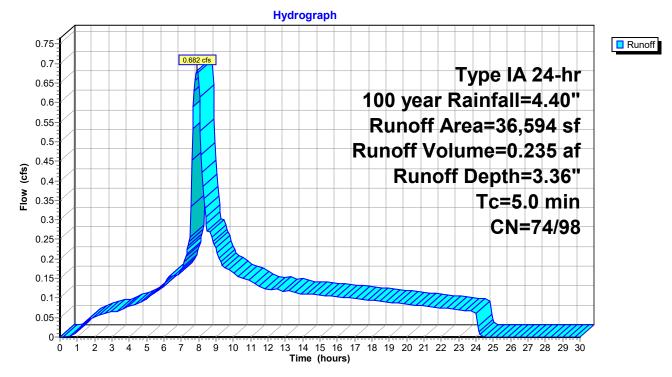
[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.682 cfs @ 7.92 hrs, Volume= Routed to Pond W-Flow : West 0.235 af, Depth= 3.36"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 100 year Rainfall=4.40"

A	rea (sf)	CN	Description			
	23,613	98	Roofs, HSG	G C		
	12,981	74	>75% Gras	s cover, Go	ood, HSG C	
	36,594	89	Weighted A	verage		
	12,981	74	35.47% Pervious Area			
	23,613	98	64.53% Imp	pervious Are	rea	
Tc (min)	Length (feet)	Slop (ft/f		Capacity (cfs)	Description	
5.0					Direct Entry,	

Subcatchment W: West - POST



Summary for Pond W-Flow: West

Inflow Area =	0.840 ac, 64.	53% Impervious, Inflow De	pth = 3.36" for 100 year event
Inflow =	0.682 cfs @	7.92 hrs, Volume=	0.235 af
Outflow =	0.288 cfs @	8.45 hrs, Volume=	0.180 af, Atten= 58%, Lag= 31.9 min
Primary =	0.004 cfs @	8.45 hrs, Volume=	0.008 af
Secondary =	0.285 cfs @	8.45 hrs, Volume=	0.173 af

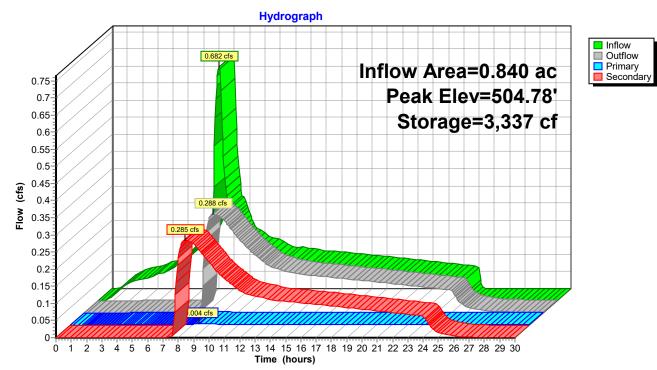
Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 504.78' @ 8.45 hrs Surf.Area= 1,200 sf Storage= 3,337 cf

Plug-Flow detention time= 313.7 min calculated for 0.180 af (77% of inflow) Center-of-Mass det. time= 163.1 min (854.9 - 691.8)

Volume	Invert	Avail.Sto	rage Storage [Description			
#1	502.00'	3,60	00 cf Custom	Stage Data (Prisma	tic) Listed below (Recalc)		
Elevatior (feet		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
502.00)	1,200	0	0			
505.00)	1,200	3,600	3,600			
Device	Routing	Invert	Outlet Devices	i			
#1	Primary	502.00'	0.3" Horiz. Ori	fice/Grate C= 0.6	00 Limited to weir flow at low heads		
#2	Secondary	504.00'	3.7" Vert. Orif	ice/Grate C= 0.60	0 Limited to weir flow at low heads		
Primary OutFlow Max=0.004 cfs @ 8.45 hrs HW=504.78' (Free Discharge)							

1=Orifice/Grate (Orifice Controls 0.004 cfs @ 8.03 fps)

Secondary OutFlow Max=0.285 cfs @ 8.45 hrs HW=504.78' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.285 cfs @ 3.81 fps)



Pond W-Flow: West