C.O'Sullivan

PRELIMINARY DRAINAGE REPORT FOR

Hawk's Ridge Apartments Phase 3 Salem, Oregon Pre-App No. 21-113574-PA

> Prepared For: KCH Enterprises, LLC 10355 Liberty Road S Salem, Oregon 97306

> > February 7, 2022



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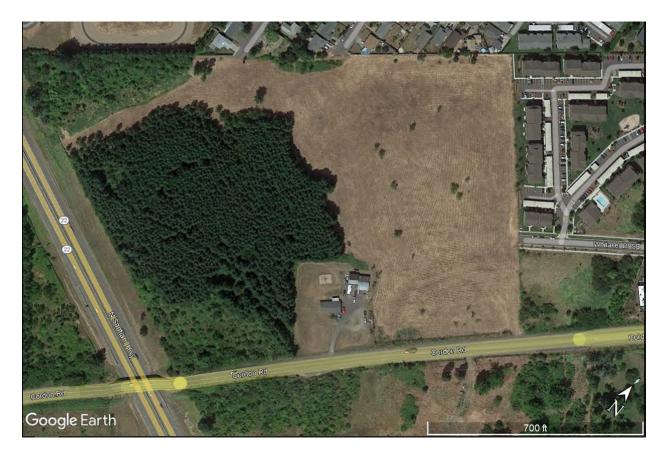
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INTRODUCTION

The Hawks Ridge Apartments Phase 3 is a proposed 396-unit apartment complex adjacent to the existing Reserve At Hawk's Ridge to the Northeast. The location of the site is northwest of Cordon Road and north of N Santiam Hwy. The parcel of land to be developed are Tax Lots 200, 300, 400, 401, and 500 of Marion County Assessor's Map 08 2W 05. A vicinity map and supporting maps are located in Appendix A of this report. An aerial image is below.



Project Site

The development consists of 396 apartments on approximately 23.73-acres. The proposed development will be connected to public water and public sewer. Green Stormwater Infrastructure (GSI) to the Maximum Extent Feasible (MEF) is being used for the new developed areas per City of Salem Administrative Rules, Chapter 109, Division 004, Stormwater System, Appendix 4E and Ordinance Bill No. 8-20 (Standards). All facilities will be constructed to meet the City of Salem standards.

EXISTING CONDITIONS

The parcel is irregular in shape. Surface conditions consists of grass, cultivated crops, and trees. There are no identified wetlands, sensitive areas or waterways located on the property. The site has flat to rolling slopes running northeasterly and northwesterly. The topographic relief is approximately 11-feet with a high point elevation of approximately 226.5-feet. The abutting properties are single family residences with public improvements that include storm water conveyance systems or apartment complexes. Appendix A contains a drainage map of existing and proposed conditions.

Soils

The Soil Conservation Service Soil Survey of Marion County identifies the predominate soils on the site as a: Woodburn silt loam, 0 to 3 percent slopes (map unit WuA) and Dayton silt loam (map unit Da). The Woodburn silt loam is in the hydrologic soil group C and Dayton silt loam is in hydrologic soil group D. Appendix B contains the NRCS soil survey for the site.

WATER QUALITY ANALYSIS

Water quality flow rates will be calculated with HydroCAD 10.10-7a. The SCS TR-20 Unit Hydrograph method will be used to generate the hydrographs. A Type 1A storm and a 24-hour rainfall depth of 1.38 inches per hour will be used to determine the water quality flow rate.

WATER QUALITY DESIGN

The proposed vegetative swale will provide water quality treatment by slowing the stormwater down, allowing for the removal of pollutants through sedimentation, adsorption onto surrounding vegetation, and biological uptake. The facility will be designed per the City of Salem designed standards.

STORMWATER QUANTITY ANALYSIS

Stormwater quantity (Flow Control) is proposed to be handled by on-site detention. Runoff from the developed right-of-way will be routed to the facility that ultimately controls runoff to pre-developed flow rates.

Per Subsection 4.2(p)(3)(A) of the standards, one-half of the post development peak runoff rate of the two-year storm must be equal to or less than one-half of the peak runoff rate of the pre-developed two-year, 24-hour storm. This also applies to the 10-year, 25-year, and 100-year, 24-hour storm events.

The pre-developed flow rates were calculated using HydroCAD 10.10-6a. Table 1 below lists the 24-hour rainfall depths used for the analysis of each storm event. Please note that the 2-year event was halved and then analyzed.

Table	1
-------	---

Storm Event	24-hour Rainfall Depth (in)
2	2.2
10	3.2
25	3.6
100	4.4

For the pre-developed conditions, a time of concentration of 90 minutes was calculated for the site. The time of concentration data is in Appendix C. The calculations are incorporated in the HydroCAD output located in Appendix D. On-site areas were classified as "City of Salem Pre-Development, HSG C" and "City of Salem Pre-Development, HSG D" with a Curve Number (CN) of 72 and 79 respectively. A pre-developed basin map is in Appendix A.

The SCS TR-20 Unit Hydrograph method was used to generate the hydrographs. A Type 1A rainfall distribution was used with the above rainfall depths. Table 2 below identifies the allowable predeveloped release rate for each storm event.

Storm Event	Total Allowable Release Rate (cfs)
Half of 2-year	0.09
10-year	2.30
25-year	3.18
100-year	5.18

Table 2

The post-developed flow rates were calculated using HydroCAD 10.10-7a. An initial time of concentration of 15 minutes was assumed for the developed subdivision. The calculations are incorporated in the HydroCAD output located in Appendix C. The developed site was classified as 64 percent "Impervious, HSG C" with a CN of 98, 32 percent "> 75% Grass cover, HSG C" with a CN of 74, and 4 percent "> 75% Grass cover, HSG D" with a CN of 80. Table 3 below lists the CN values for the 3

developed areas that will contribute storm water runoff to the detention systems. A developed basin map is in Appendix A.

Basin	Impervious Area (Ac) CN = 98	Landscape Area, HSG C (Ac) CN = 74	Landscape Area, HSG D (Ac) CN = 80	TOTAL Area (Ac)	Composite CN
Basin	15.13	7.74	0.86	23.73	90

Table 3

DETENTION SYSTEM

In the detention analysis, the entire development was considered a single basin draining into the drainage facilities. Based on the above design parameters, runoff from developed conditions will be controlled to or below half of the 2-year, 10-year, 25-year, and 100-year pre-developed release rates. The release rates and detention requirements were generated from the HydroCAD software, which can be seen in Appendix D. Table 4 below summarizes the requirements for the storm events.

Storm Event	Release Rate (cfs)	Allowable Release Rate (cfs)	Required Detention Volume (ft³)	Provided Detention Volume (ft³)
Half of 2-year	0.09	0.09	29,132	73,690
10-year	2.26	2.30	65,367	73,690
25-year	3.12	3.19	66,810	73,690
100-year	5.16	5.19	72,661	73,690

Table 4

(Detention Summary)

Flow control is achieved using a series of orifices combined with overflow weirs inside a control structure located within the basin. The sizing of the orifice uses the standard orifice equation provided in the City of Salem Stormwater Management Manual. Table 5 below identifies orifice sizes, elevations, and the water surface elevations. Control Orifice #1 is less than two inches in size so it will need to be contained within a section of well screen or slotted pipe in order to comply with Salem Standards.

Table	5
-------	---

Control Orifice (#)	Release Rate (cfs)	Orifice Diameter (inches)	Elevation (feet)	W.S. Elevation (feet)
1	0.09	1.75	215.60	216.97
2	2.26	7.25	215.60	218.59
3	3.12	8.50	215.60	218.65
4	5.16	10.75	215.60	218.92
	Orifice (#) 1 2 3	Orifice (#) (cfs) 1 0.09 2 2.26 3 3.12	Orifice (#)(cfs)Diameter (inches)10.091.7522.267.2533.128.50	Orifice (#)(cfs)Diameter (inches)(feet)10.091.75215.6022.267.25215.6033.128.50215.60

(Orifice Summary)

In the event the control structure experiences a failure, a secondary emergency overflow escape route has been incorporated into the facility that outlets into an existing drainage way via a weir in the southeast corner. This overflow is at an elevation of 219 and the control structure also contains an overflow weir that is at an elevation of 218.95.

WATER QUALITY DESIGN

Water quality treatment for the proposed development will be via a vegetative swale. The flow rate was calculated with HydroCAD 10.10-7a. The SCS TR-20 Unit Hydrograph method was used to generate the hydrographs. A Type 1A storm and a 24-hour rainfall depth of 1.38 inches per hour was used to determine the water quality flow rate of 0.63 cfs from the control structure. The release rate was generated from the HydroCAD software, which can be seen in Appendix E. The water quality system will treat 80 percent of the annual rainfall.

VEGETATIVE SWALE ANALYSIS

The proposed vegetative swale is approximately 100 feet in length. It provides water quality treatment by slowing the stormwater down, allowing for the removal of pollutants through sedimentation, adsorption onto surrounding vegetation, and biological uptake. The swale was designed per the city designed standards using the following criteria:

Bottom Width – Minimum	2 feet	
Maximum Water Depth - Treatment	4 inches	
Maximum Water Depth - Conveyance	12 inches	
Side Slopes	3:1	
Manning's "n" Treatment	0.25	
Mannings's "n" Conveyance	0.030	
Minimum & Maximum Slope	0.5% - 6%	
Maximum Velocity	0.9 feet per second	
Hydraulic Residence Time	> 9 minutes	

The program Hydraulic Toolbox 4.4 from the Federal Highway Administration (FHWA) was used to analyze the swale. The analysis yields an average velocity of 0.183 feet per second. With a 100-foot-long swale, a hydraulic residence time is calculated to be 546 seconds or 9.1 minutes, which exceeds the required 9-minute residence time. Both the average velocity and the hydraulic residence time meet the parameters established in the City of Salem Design Standards. Below contains the computer program generated output table.

Turney Transmidel	Define	Parameter	Value	Unit
Type: Trapezoidal	Denne	Flow	0.630	cfs
Side Slope 1 (Z1): 3.0	H : 1V	Depth	0.315	ft
Side Slope 2 (Z2): 3.0	H : 1V	Area of Flow	3.446	sq ft
Channel Width (B): 10.0	(ft)	Wetted Perimeter	11.991	ft
Pipe Diameter (D): 0.0	(ft)	Hydraulic Radius	0.287	ft
		Average Velocity	0.183	fps
Longitudinal Slope: 0.00	5 (ft/ft)	Top Width (T)	11.889	ft
🗖 Override Default		Froude Number	0.060	
Manning's Roughness: 0.25	00	Critical Depth	0.050	ft
🔲 Use Lining		Critical Velocity	1.253	fps
Lining Type: Woven Paper N	let 👻	Critical Slope	2.49639	ft/ft
,		Critical Top Width	10.297	ft
		Max Shear Stress	0.098	lb/ft^2
		Avg Shear Stress	0.090	Ib/ft^2
Enter Flow: 0.630	(cfs)			
C Enter Depth: 0.315	(ft)			
Calculate				

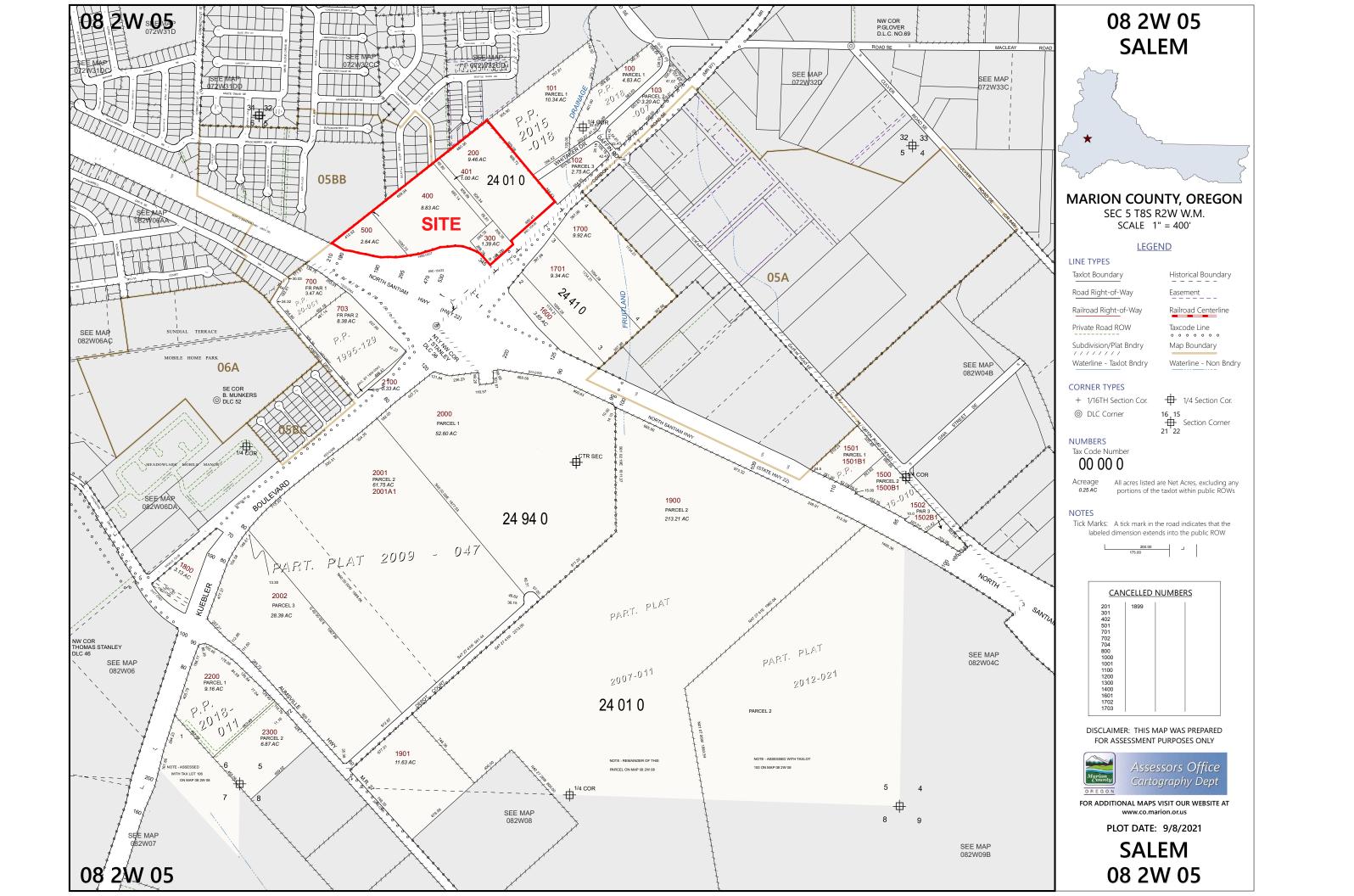
The swale was also analyzed for conveyance using the City of Salem design parameters. The allowable 100-year outflow of 5.18 cfs was used to determine the swale capacity requirements. Below contains the computer program generated output table. The design is exceeding the standards.

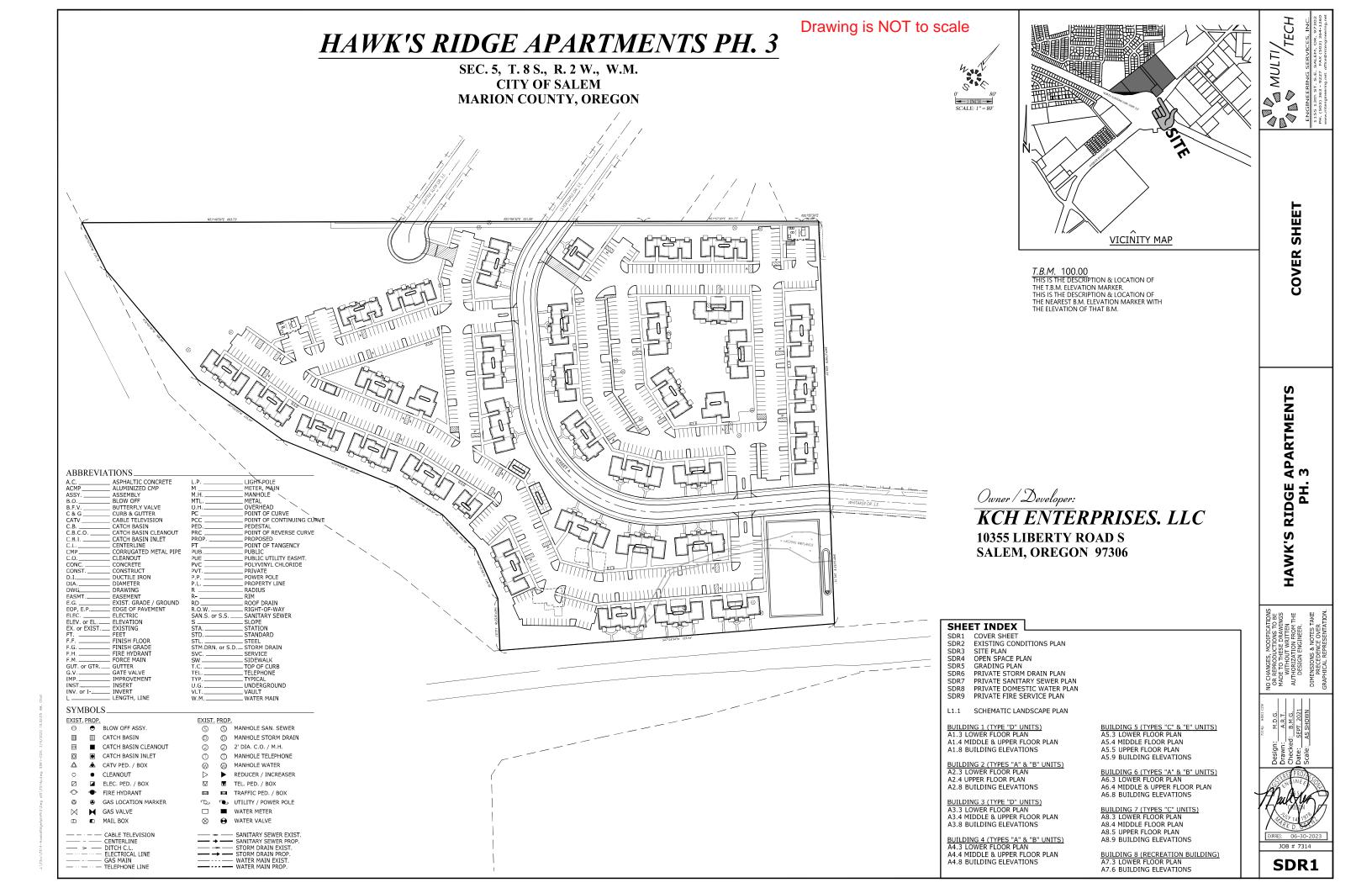
100-yr conveyance				×
Type: Trapezoidal 💌	Define	Parameter	Value	Unit
	-	Flow	5.180	cfs
Side Slope 1 (Z1): 3.0	H : 1V	Depth	0.312	ft
Side Slope 2 (Z2): 3.0	H : 1V	Area of Flow	3.414	sq ft
Channel Width (B): 10.0	(ft)	Wetted Perimeter	11.974	ft
Pipe Diameter (D): 0.0	(ft)	Hydraulic Radius	0.285	ft
		Average Velocity	1.517	fps
Longitudinal Slope: 0.005	(ft/ft)	Top Width (T)	11.873	ft
🗖 Override Default	_	Froude Number	0.499	
Manning's Roughness: 0.0300		Critical Depth	0.199	ft
🔲 Use Lining		Critical Velocity	2.462	fps
Lining Type: Woven Paper Net	-	Critical Slope	0.02312	ft/ft
		Critical Top Width	11.191	ft
		Max Shear Stress	0.097	lb/ft^2
		Avg Shear Stress	0.089	lb/ft^2
Enter Flow: 5.180	(cfs)			
C Enter Depth: 0.312	(ft)			
	(5)			
Calculate				
Plot Comp	ute Curves	OK		Cancel

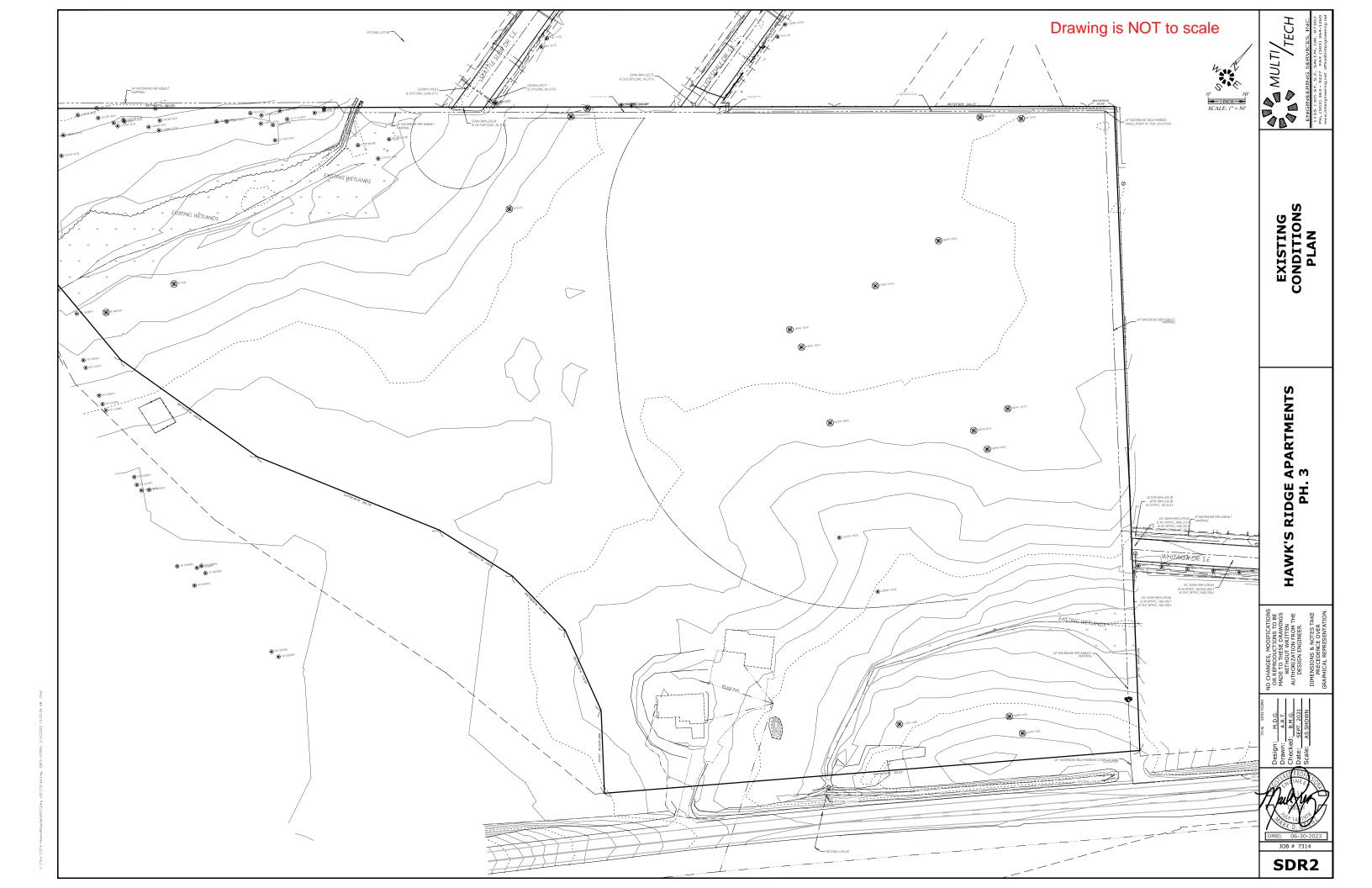
CONCLUSION

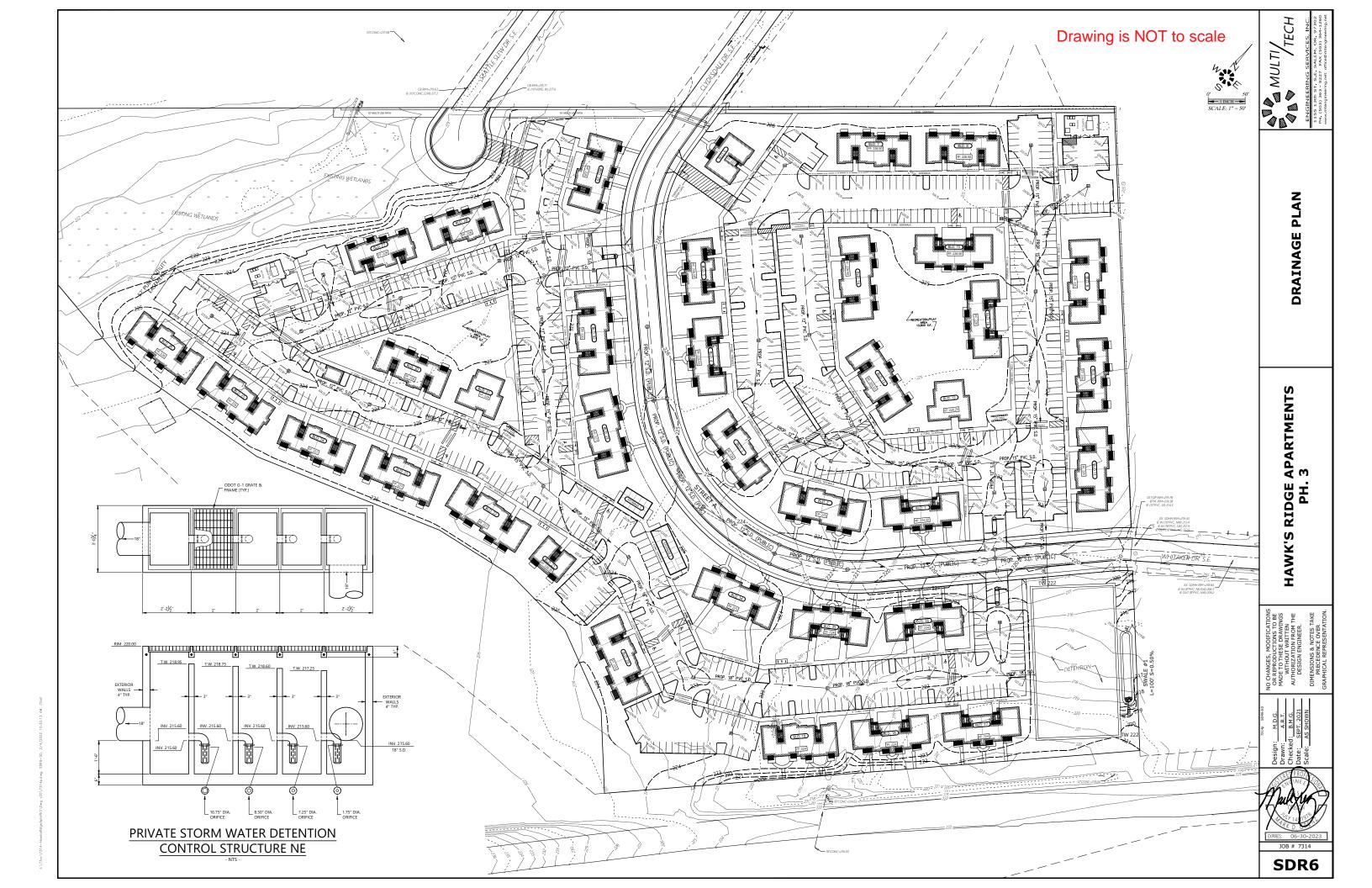
Based on the presented information, the proposed design will meet the water quality and quantity standards. If there are any questions regarding this analysis or the design, please contact Matthew Hendrick at Multi/Tech Engineering by phone at (503) 363-9227 or via e-mail at mhendrick@mtengineering.net.

Appendix A









Appendix B



United States Department of Agriculture

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Marion County Area, Oregon

Hawks Ridge Apts.



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



	MAP L	EGEND)	MAP INFORMATION		
Area of Int	Area of Interest (AOI)		Spoil Area	The soil surveys that comprise your AOI were mapped at		
	Area of Interest (AOI)	۵	Stony Spot	1:20,000.		
Soils		0	Very Stony Spot	Warning: Soil Map may not be valid at this scale.		
	Soil Map Unit Polygons	\$2	Wet Spot			
~	Soil Map Unit Lines	Δ	Other	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil		
	Soil Map Unit Points		Special Line Features	line placement. The maps do not show the small areas of		
•	Point Features Blowout	Water Fea	atures	contrasting soils that could have been shown at a more detailed scale.		
စ္		~	Streams and Canals			
×	Borrow Pit	Transport	ation	Please rely on the bar scale on each map sheet for map		
×	Clay Spot	+++	Rails	measurements.		
\diamond	Closed Depression	~	Interstate Highways	Source of Map: Natural Resources Conservation Service		
X	Gravel Pit	~	US Routes	Web Soil Survey URL:		
00	Gravelly Spot	\sim	Major Roads	Coordinate System: Web Mercator (EPSG:3857)		
Ø	Landfill	~	Local Roads	Maps from the Web Soil Survey are based on the Web Mercator		
Α.	Lava Flow	Backgrou	Ind	projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the		
عليه	Marsh or swamp	Mar.	Aerial Photography	Albers equal-area conic projection, should be used if more		
Ŕ	Mine or Quarry			accurate calculations of distance or area are required.		
0	Miscellaneous Water			This product is generated from the USDA-NRCS certified data as		
0	Perennial Water			of the version date(s) listed below.		
\sim	Rock Outcrop			Soil Survey Area: Marion County Area, Oregon		
+	Saline Spot			Survey Area Data: Version 19, Oct 27, 2021		
°.°	Sandy Spot			Soil map units are labeled (as space allows) for map scales		
-	Severely Eroded Spot			1:50,000 or larger.		
0	Sinkhole			Date(s) aerial images were photographed: Aug 1, 2018—Aug		
š	Slide or Slip			31, 2018		
ø	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.		

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Da	Dayton silt loam	2.6	9.4%
WuA	Woodburn silt loam, 0 to 3 percent slopes	25.2	90.6%
Totals for Area of Interest		27.9	100.0%

Soil Information for All Uses

Soil Properties and Qualities

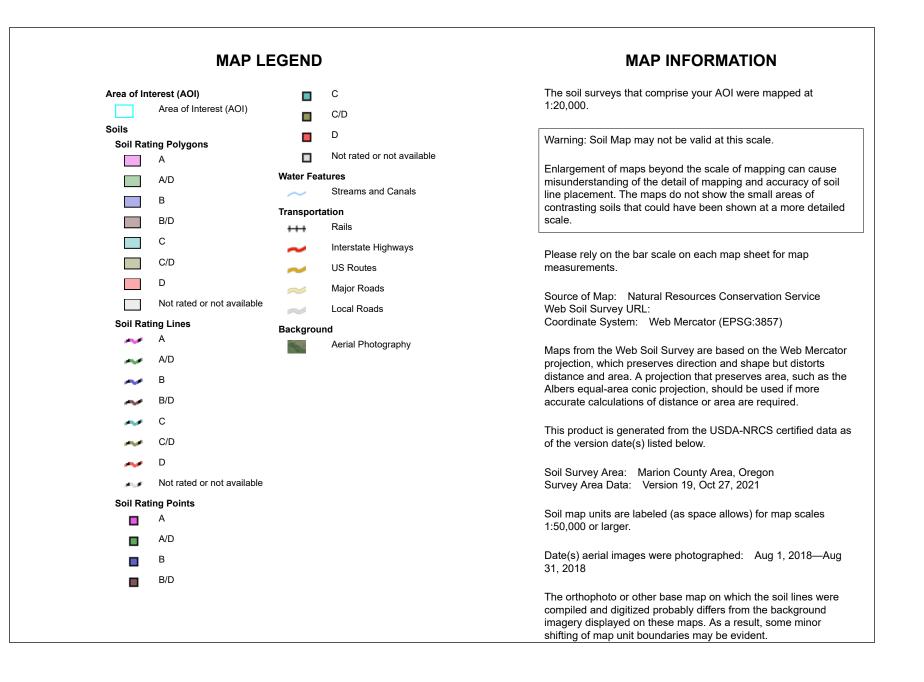
The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

Hydrologic Soil Group (Hawks Ridge Apts)





Table—Hydrologic Soil Group (Hawks Ridge Apts)

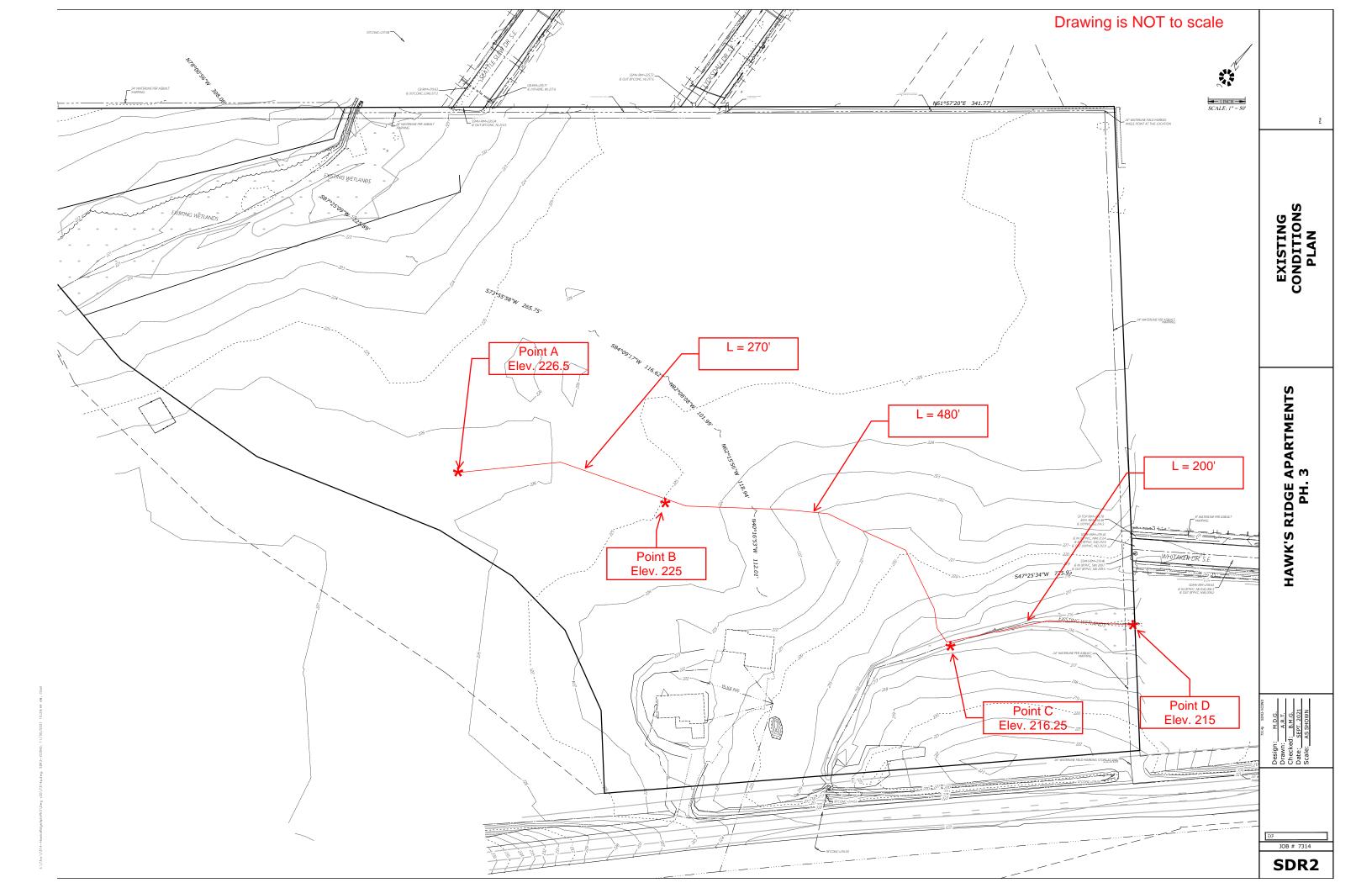
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
Da	Dayton silt loam	D	2.6	9.4%
WuA	Woodburn silt loam, 0 to 3 percent slopes	С	25.2	90.6%
Totals for Area of Interes	st	27.9	100.0%	

Rating Options—Hydrologic Soil Group (Hawks Ridge Apts)

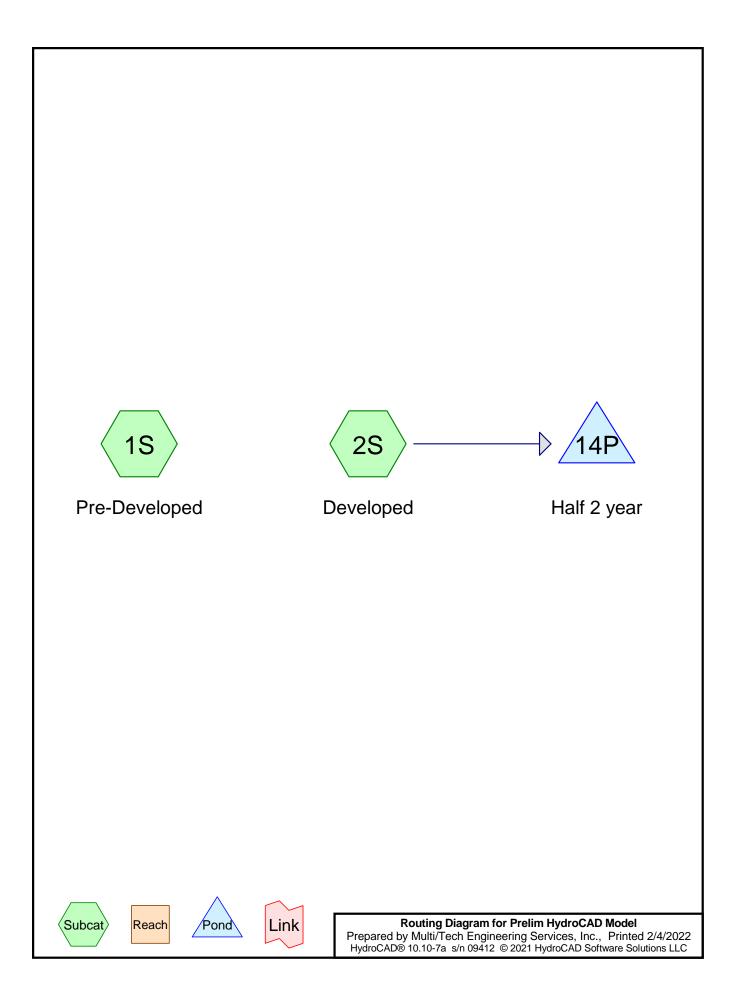
Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher Appendix C

Worksheet 3: Time of Concentration (T_c) or travel time (T_t)

Project Hawks Ridge Apts. Phase 3	^{By} C. O'Sullivan	Date 11/2021						
Location Salem, Oregon	Checked	Date						
Check one: \Box Present \Box Developed Check one: \Box T _c \Box T _t through subarea								
Notes: Space for as many as two segments per flow typ Include a map, schematic, or description of flow								
Sheet flow (Applicable to Tc only)								
Segment ID								
1. Surface description (Table 4D-4)	0.00							
2. Manning's roughness coefficient, n (Table 4D-4)	0.30							
3. Flow length, L (total L † 300 ft) ft	2.2							
 Two-year 24-hour rainfall, P₂ in Land slope, s ft/ft 	0.0056							
	1.300 +	= 1.300						
6. $T_t = \frac{0.007 \text{ (nL)}^{0.8}}{P_2^{0.5} \text{ s}^{0.4}}$ Compute T_t hr								
Shallow concentrated flow								
Segment ID	B-C C-D							
7. Surface description (paved or unpaved)	Cultivated crops Cultivated crops	,						
8. Flow length, Lft	480 200							
9. Watercourse slope, s ft/ft	0.018 0.006							
10. Average velocity, V (figure 3-1) ft/s	1.2 0.65							
11. $T_t = \underline{L}$ Compute T_t hr	0.111 + 0.085	5 = 0.196						
Channel flow								
Segment ID								
12. Cross sectional flow area, a ft ²								
 13. Wetted perimeter, p_W ft 14. Hydraulic radius, r= ^a/₋ Compute r ft 								
14. Hydraulic radius, r= — Compute r								
16. Manning's roughness coefficient, n								
17. $V = 1.49 r^{2/3} s^{1/2}$ Compute Vft/s								
18. F low l ength, L ft								
19. $T_t = \frac{L}{3600 \text{ V}}$ Compute T_t hr	+							
3600 V 20. Watershed or subarea T_c or T_t (add T_t in steps 6, 11, an	nd 19)	Hr 1.496						



Appendix D

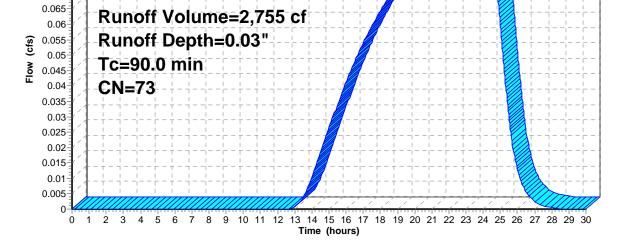


Summary for Subcatchment 1S: Pre-Developed

Runoff 0.09 cfs @ 23.30 hrs, Volume= 2,755 cf, Depth= 0.03" _

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr Half 2 Year Rainfall=1.10"

Area (ac)) CN	Desc	cription		
* 21.100) 72	COS	S Pre-Deve	loped, HSC	G C
* 2.630) 79	COS	S Pre-Deve	loped, HSC	G D
23.730) 73	Weig	ghted Aver	age	
23.730)	100.	00% Pervi	ous Area	
	ngth feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	•
90.0					Direct Entry, TR-55 Worksheet
			Sub	ocatchme	ent 1S: Pre-Developed
			Sub		ent 1S: Pre-Developed ^{ograph}
0.095			Suk		ograph +-+-+-+-+-+-+-+-+-+-+-+-+-+-+-+-+-+-+-
0.09 0.085		 			ograph ┾╴┼╴┼╴┼╴┼╴┾╴┼╴┼╴┼╴┼╴┼╴┼╴┼╴┼╴┼╴┼╴┤
0.09					ograph



Summary for Subcatchment 2S: Developed

Runoff	=	1.71 cfs @	8.11 hrs,	Volume=	33,371 cf,	Depth= 0.39"
Routed	d to Pond	d 14P : Half 2 y	year			·

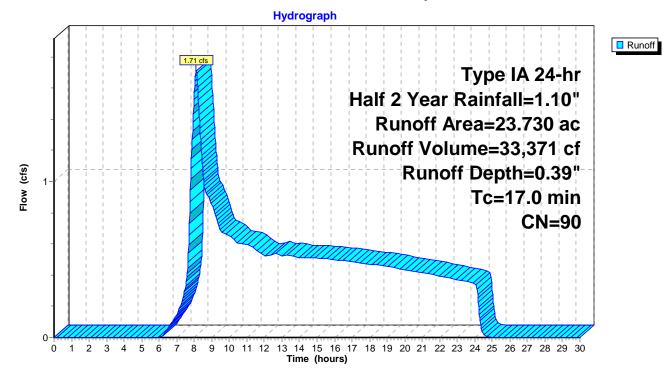
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr Half 2 Year Rainfall=1.10"

_	Area	(ac)	CN	Desc	Description					
	15.	130	98	Pave	Paved parking, HSG D					
	0.	860	80	>75%	% Grass co	over, Good	, HSG D			
_	7.	740	74	>75%	% Grass co	over, Good	, HSG C			
	23.	730	90 Weighted Average							
	8.	.600 36.24% Pervious Area								
	15.	130		63.7	6% Imperv	vious Area				
	Та	المعم	416	Clana	Valasitu	Conositu	Description			
	ŢĊ	Leng		Slope	Velocity	Capacity	Description			
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	170						Direct Entry, Direct Entry			



Direct Entry, Direct Entry

Subcatchment 2S: Developed



Summary for Pond 14P: Half 2 year

[44] Hint: Outlet device #2 is below defined storage

Inflow Area	a =	1,033,679 sf, 63.76% Impervious, Inflow Depth = 0.39" for Half 2 Ye	ear event
Inflow	=	1.71 cfs @ 8.11 hrs, Volume= 33,371 cf	
Outflow	=	0.09 cfs @ 24.32 hrs, Volume= 6,048 cf, Atten= 95%, Lag=	= 972.3 min
Primary	=	0.09 cfs @ 24.32 hrs, Volume= 6,048 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Peak Elev= 216.97' @ 24.32 hrs Surf.Area= 22,434 sf Storage= 29,132 cf

Plug-Flow detention time= 723.1 min calculated for 6,043 cf (18% of inflow) Center-of-Mass det. time= 347.1 min (1,209.5 - 862.3)

Volume	Invert	Avail.Stor	age Stor	brage Description
#1 #2	215.65' 215.66'	,	9 cf 18.0	stom Stage Data (Prismatic) Listed below (Recalc) 000" Round Pipe Storage 475.0' S= 0.0035 '/'
		96,70	8 cf Tota	tal Available Storage
Elevatior (feet		urf.Area (sq-ft)	Inc.Stor (cubic-fee	
215.65	5	21,855		0 0
216.00		21,887	7,65	
217.00		21,970	21,92	
218.00	-	22,053	22,01	
219.00		22,137	22,09	
220.00	0	22,220	22,17	79 95,868
Device	Routing	Invert	Outlet De	evices
#1	Primary	215.60'	L= 12.0' Inlet / Ou	Round Culvert RCP, rounded edge headwall, Ke= 0.100 utlet Invert= $215.60' / 215.58'$ S= $0.0017 '/$ Cc= 0.900 B, Flow Area= 1.77 sf
#2	Device 1	215.60'	1.750" Ve	Vert. Orifice/Grate C= 0.600 to weir flow at low heads
#3	Device 1	217.00'	4.0' long Head (fee	g x 0.5' breadth Broad-Crested Rectangular Weir eet) 0.20 0.40 0.60 0.80 1.00 nglish) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.09 cfs @ 24.32 hrs HW=216.97' (Free Discharge)

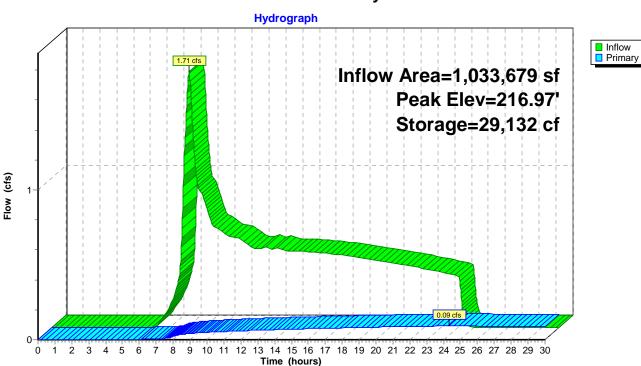
-1=Culvert (Passes 0.09 cfs of 5.49 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.09 cfs @ 5.48 fps)

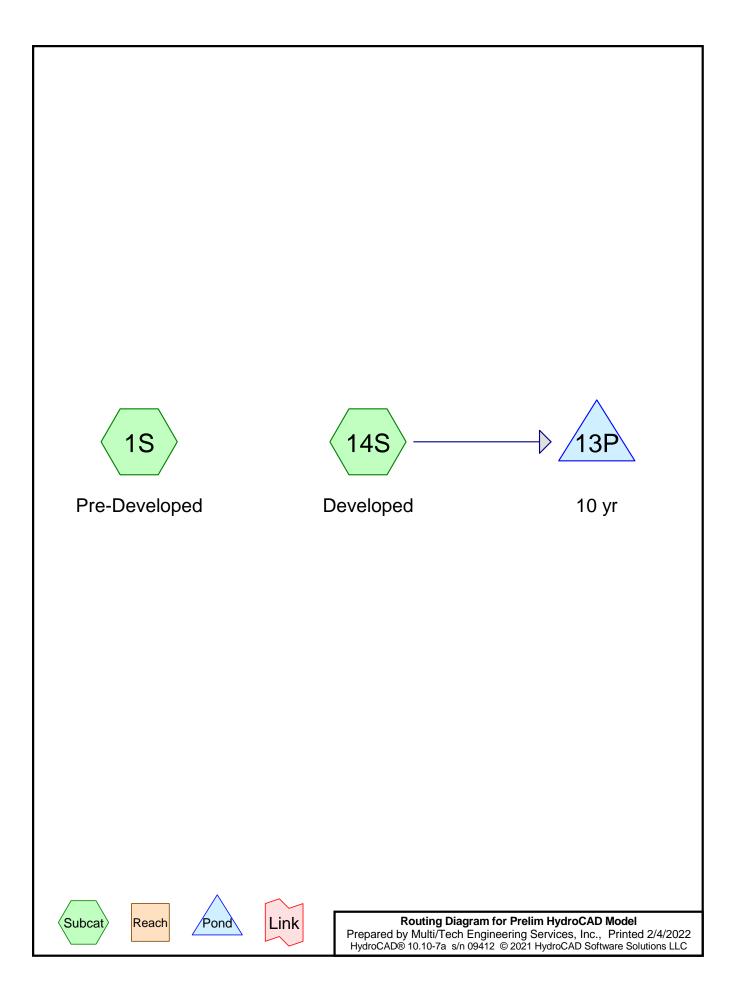
-3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Prelim HydroCAD Model

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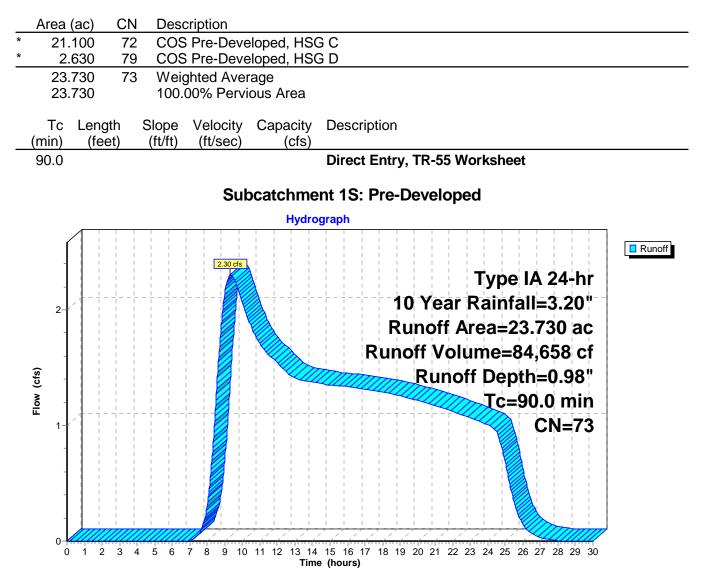


Pond 14P: Half 2 year



Runoff 2.30 cfs @ 9.31 hrs, Volume= 84,658 cf, Depth= 0.98" _

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr 10 Year Rainfall=3.20"



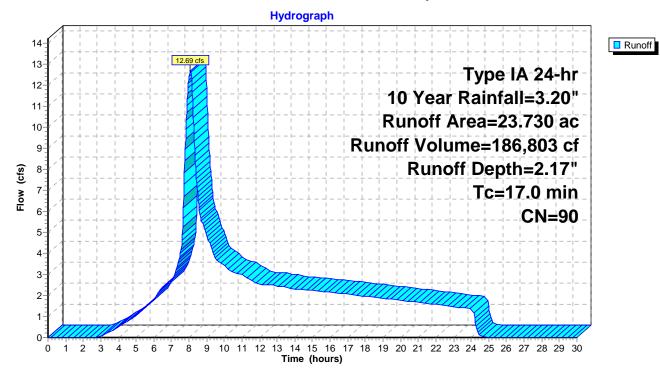
Impervious and total area from AutoCAD

Runoff	=	12.69 cfs @	8.07 hrs, Volume=	186,803 cf, Depth= 2.17"
Routed	d to Po	ond 13P : 10 yr		

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr 10 Year Rainfall=3.20"

Ar	rea (a	ac) (CN	Desc	ription		
	15.1	30	98	Pave	d parking	HSG D	
	0.8	60	80	>75%	6 Grass co	over, Good,	HSG D
	7.7	40	74	>75%	6 Grass co	over, Good,	HSG C
	23.730 90 Weighted Average						
	8.600 36.24% Pervious Area			4% Pervio	us Area		
	15.1	30		63.76	5% Imperv	vious Area	
(m		Length (feet)		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	<i>.</i> 0			<u> </u>			Direct Entry, Direct Entry





Summary for Pond 13P: 10 yr

[44] Hint: Outlet device #2 is below defined storage

Inflow Area	a =	1,033,679 sf, 63.76% Impervious, Inflow Depth = 2.17" for 10 Year event
Inflow	=	12.69 cfs @ 8.07 hrs, Volume= 186,803 cf
Outflow	=	2.26 cfs @ 14.70 hrs, Volume= 166,461 cf, Atten= 82%, Lag= 397.9 min
Primary	=	2.26 cfs @ 14.70 hrs, Volume= 166,461 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Peak Elev= 218.59' @ 14.70 hrs Surf.Area= 22,153 sf Storage= 65,367 cf

Plug-Flow detention time= 383.9 min calculated for 166,461 cf (89% of inflow) Center-of-Mass det. time= 312.7 min (1,070.3 - 757.5)

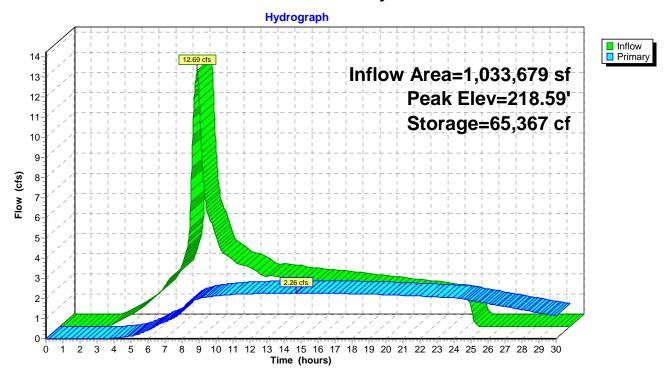
Volume	Invert	Avail.Sto	rage Sto	age Description	
#1 #2	215.65' 215.66'	,	39 cf 18.0	tom Stage Data 00" Round Pipe 75.0' S= 0.0035	
		96,70	08 cf Tota	I Available Stora	ge
Elevatio		urf.Area (sq-ft)	Inc.Stor (cubic-fee		
215.6		21,855		0	0
216.0		21,887	7,65	,	
217.0		21,970	21,92		
218.0		22,053	22,01		
219.0		22,137	22,09		
220.0	00	22,220	22,17	9 95,8	58
Device	Routing	Invert	Outlet De	vices	
#1	Primary	215.60'	18.000"	Round Culvert	
			L= 12.0'	RCP, rounded e	dge headwall, Ke= 0.100
					0' / 215.58' S= 0.0017 '/' Cc= 0.900
				Flow Area= 1.7	
#2	Device 1	215.60'		ert. Orifice/Grate	
				weir flow at low	
#3	Device 1	218.60'	•		road-Crested Rectangular Weir
			· ·	et) 0.20 0.40 0.6	
			Coef. (Er	glish) 2.80 2.92	3.08 3.30 3.32
					· · · · ·

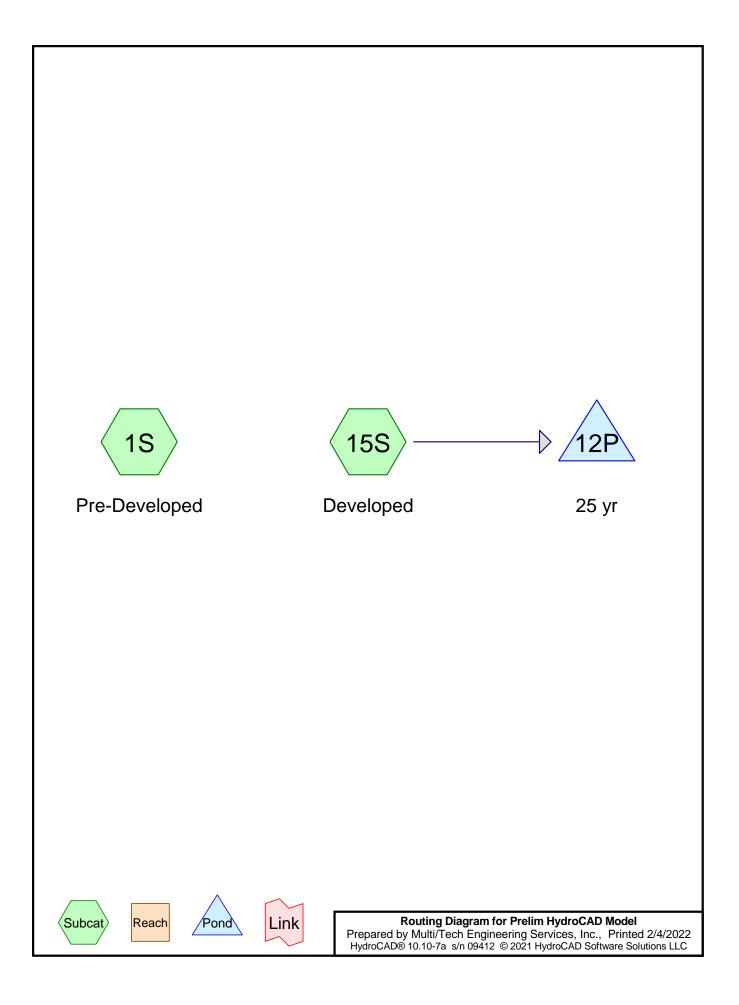
Primary OutFlow Max=2.26 cfs @ 14.70 hrs HW=218.59' (Free Discharge)

-1=Culvert (Passes 2.26 cfs of 15.15 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 2.26 cfs @ 7.89 fps)

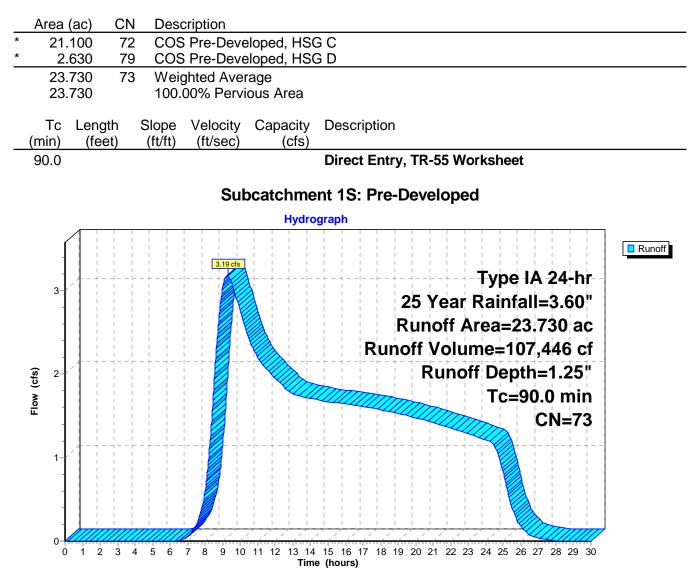
Pond 13P: 10 yr





Runoff = 3.19 cfs @ 9.29 hrs, Volume= 107,446 cf, Depth= 1.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr 25 Year Rainfall=3.60"



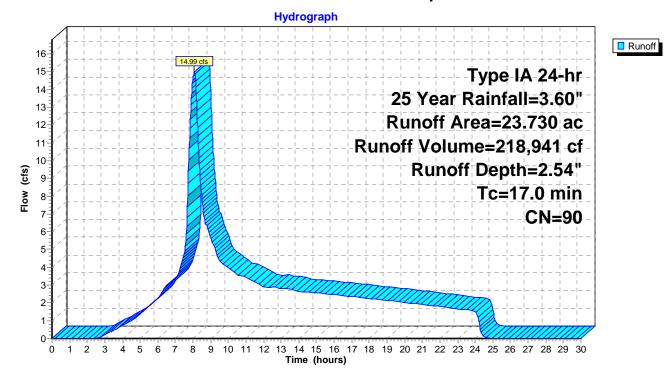
Impervious and total area from AutoCAD

Runoff	=	14.99 cfs @	8.06 hrs, Volume=	218,941 cf, Depth= 2.54"
Routed	d to Po	nd 12P : 25 yr		

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr 25 Year Rainfall=3.60"

 Area	(ac)	CN	Desc	ription		
15.	130	98	Pave	ed parking	HSG D	
0.	860	80	>75%	6 Grass co	over, Good,	HSG D
 7.	740	74	>75%	6 Grass co	over, Good,	HSG C
23.	23.730 90 Weighted Average					
8.	600		36.24	4% Pervio	us Area	
15.	130		63.7	6% Imperv	vious Area	
Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
 17.0						Direct Entry, Direct Entry

Subcatchment 15S: Developed



Summary for Pond 12P: 25 yr

[44] Hint: Outlet device #2 is below defined storage

Inflow Are	a =	1,033,679 sf, 63.76% Impervious, Inflow Depth = 2.54" for 25 Year event
Inflow	=	14.99 cfs @ 8.06 hrs, Volume= 218,941 cf
Outflow	=	3.12 cfs @ 11.61 hrs, Volume= 209,491 cf, Atten= 79%, Lag= 212.7 min
Primary	=	3.12 cfs @ 11.61 hrs, Volume= 209,491 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Peak Elev= 218.65' @ 11.61 hrs Surf.Area= 22,140 sf Storage= 66,810 cf

Plug-Flow detention time= 298.6 min calculated for 209,351 cf (96% of inflow) Center-of-Mass det. time= 269.0 min (1,018.1 - 749.1)

Volume	Inve	rt Avail.Sto	rage	Storage	Description	
#1 #2	215.68 215.66	,	39 cf	18.000"	Stage Data (Pri Round Pipe Sto)' S= 0.0035 '/'	ismatic) Listed below (Recalc) orage
		96,7	08 cf	Total Av	ailable Storage	
Elevatio		Surf.Area (sq-ft)	Inc.s (cubic)	Store -feet)	Cum.Store (cubic-feet)	
215.6		21,855		0	0	
216.0		21,887		7,655	7,655	
217.0		21,970		1,929	29,583	
218.0		22,053		2,012	51,595	
219.0		22,137		2,095	73,690	
220.0	00	22,220	22	2,179	95,868	
Device	Routing	Invert	Outle	t Device	s	
#1	Primary	215.60'	18.00	0" Roui	nd Culvert	
	-		L= 12	2.0' RCF	P, rounded edge	headwall, Ke= 0.100
						215.58' S= 0.0017 '/' Cc= 0.900
				,	w Area= 1.77 sf	
#2	Device 1	215.60'			Drifice/Grate C	
					r flow at low hea	
#3	Device 1	218.75'		-		d-Crested Rectangular Weir
				· · ·	.20 0.40 0.60	
			Coef.	(English	n) 2.80 2.92 3.0	08 3.30 3.32
			_			

Primary OutFlow Max=3.12 cfs @ 11.61 hrs HW=218.65' (Free Discharge)

-1=Culvert (Passes 3.12 cfs of 15.47 cfs potential flow)

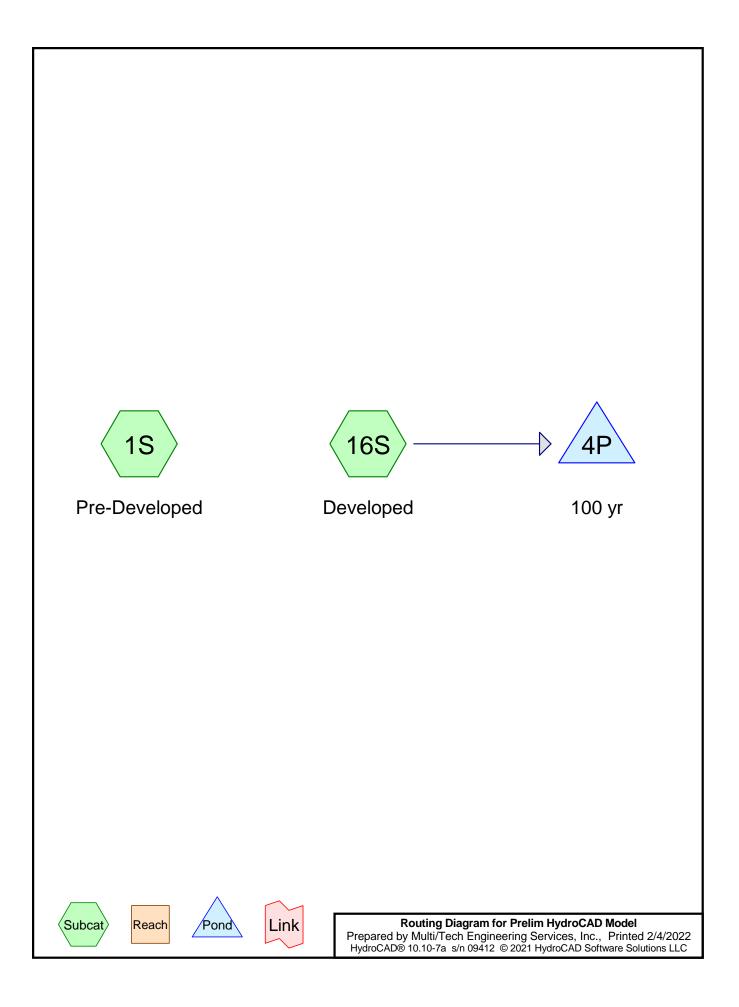
-2=Orifice/Grate (Orifice Controls 3.12 cfs @ 7.91 fps)

-3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

2[.] 1.

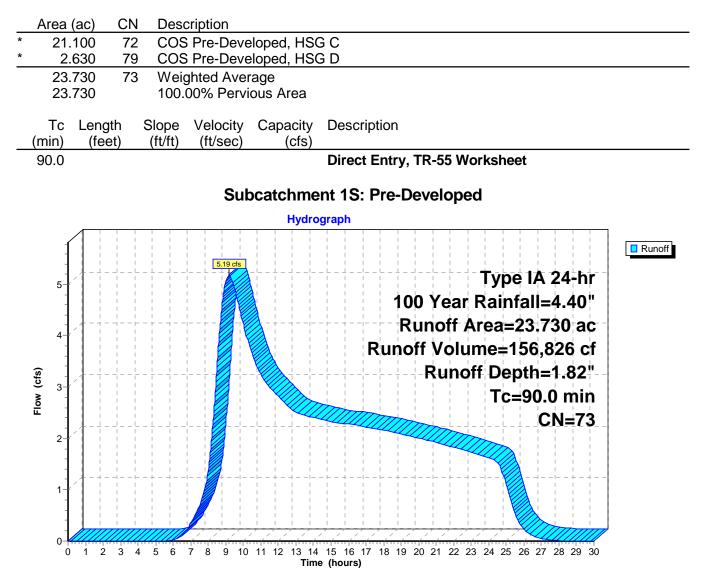
Hydrograph Inflow
 Primary 14.99 cfs 16 Inflow Area=1,033,679 sf 15 Peak Elev=218.65' 14 13-Storage=66,810 cf 12 11 10-Flow (cfs) 9 8 7-6 5 4 3.12 cfs 3-

Pond 12P: 25 yr



Runoff = 5.19 cfs @ 9.19 hrs, Volume= 156,826 cf, Depth= 1.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr 100 Year Rainfall=4.40"



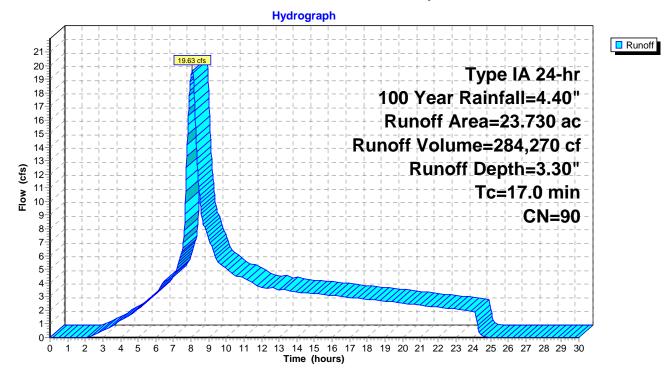
Impervious and total area from AutoCAD

Runoff	=	19.63 cfs @	8.06 hrs,	Volume=	284,270 cf, Depth= 3.30"
Routed	d to Po	nd 4P : 100 yr			

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr 100 Year Rainfall=4.40"

Area	(ac)	CN	Desc	cription		
15.	130	98	Pave	ed parking,	HSG D	
0.	860	80	>75%	6 Grass co	over, Good,	, HSG D
7.	740	74	>75%	6 Grass co	over, Good,	, HSG C
23.730 90 Weighted Average						
8.	600		36.24	4% Pervio	us Area	
15.	130		63.7	6% Imperv	vious Area	
Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
17.0	(100	-/	()	(12,000)	(010)	Direct Entry, Direct Entry

Subcatchment 16S: Developed



Summary for Pond 4P: 100 yr

[44] Hint: Outlet device #2 is below defined storage

Inflow Area	=	1,033,679 sf,	63.76% Impervious,	Inflow Depth =	3.30"	for 100 Year event
Inflow =	=	19.63 cfs @	8.06 hrs, Volume=	284,270 c	f	
Outflow =	=	5.16 cfs @	9.90 hrs, Volume=	279,587 c	f, Atter	n= 74%, Lag= 110.5 min
Primary =	=	5.16 cfs @	9.90 hrs, Volume=	279,587 c	f	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Peak Elev= 218.92' @ 9.90 hrs Surf.Area= 22,130 sf Storage= 72,661 cf

Plug-Flow detention time= 195.6 min calculated for 279,587 cf (98% of inflow) Center-of-Mass det. time= 183.9 min (919.7 - 735.8)

Volume	Invert	Avail.Sto	rage Storag	e Description	
#1 #2	215.65' 215.66'	,	39 cf 18.000	m Stage Data (Pr)" Round Pipe St 5.0' S= 0.0035 '/'	ismatic) Listed below (Recalc) orage
		96,70	08 cf Total /	Available Storage	
Elevatio (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
215.6		21,855	0	0	
216.0		21,887	7,655	7,655	
217.0		21,970	21,929	29,583	
218.0		22,053	22,012	51,595	
219.0		22,137	22,095	73,690	
220.0	00	22,220	22,179	95,868	
Device	Routing	Invert	Outlet Devi	ces	
#1	Primary	215.60'	18.000" Ro	ound Culvert	
			L= 12.0' R	CP, rounded edge	e headwall, Ke= 0.100
			Inlet / Outle	t Invert= 215.60' /	215.58' S= 0.0017 '/' Cc= 0.900
			n= 0.013, F	Flow Area= 1.77 sf	
#2	Device 1	215.60'		t. Orifice/Grate	
			Limited to w	eir flow at low hea	ads
#3	Device 1	218.90'	4.0' long x	0.5' breadth Broa	nd-Crested Rectangular Weir
			Head (feet)	0.20 0.40 0.60	0.80 1.00
			Coef. (Engli	ish) 2.80 2.92 3.	08 3.30 3.32
					_

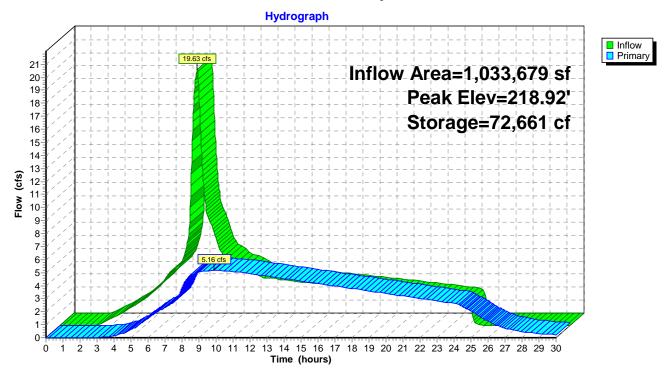
Primary OutFlow Max=5.16 cfs @ 9.90 hrs HW=218.92' (Free Discharge)

-1=Culvert (Passes 5.16 cfs of 16.73 cfs potential flow)

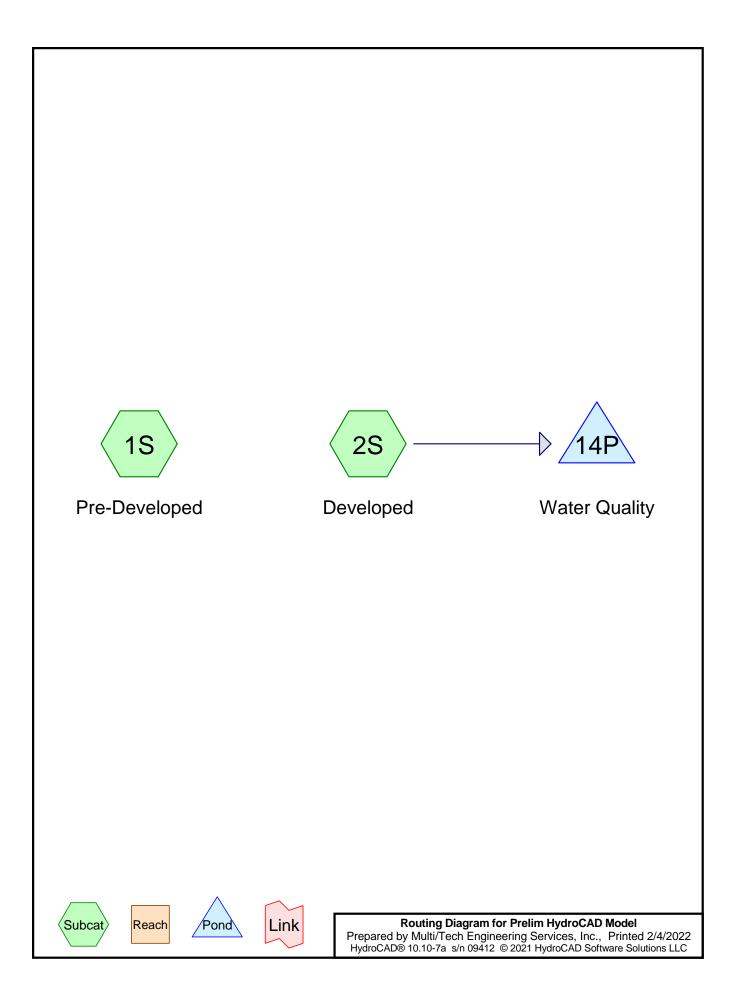
-2=Orifice/Grate (Orifice Controls 5.14 cfs @ 8.15 fps)

-3=Broad-Crested Rectangular Weir (Weir Controls 0.02 cfs @ 0.35 fps)

Pond 4P: 100 yr



Appendix E

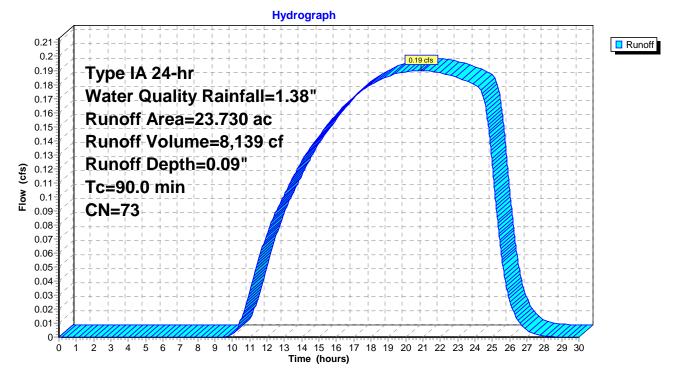


Runoff = 0.19 cfs @ 20.90 hrs, Volume= 8,139 cf, Depth= 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr Water Quality Rainfall=1.38"

_	Area	(ac)	CN	Desc	cription		
*	21.	100	72	COS	S Pre-Deve	loped, HSC	€C
*	2.	630	79	COS	S Pre-Deve	loped, HSC	G D
	23.	730	73	Weig	ghted Aver	age	
	23.	730		100.	00% Pervi	ous Area	
	Тс	Leng		Slope	Velocity	Capacity	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	90.0						Direct Entry, TR-55 Worksheet

Subcatchment 1S: Pre-Developed



Impervious and total area from AutoCAD

Runoff	=	2.92 cfs @	8.10 hrs,	Volume=	50,891 cf,	Depth= 0.59"
Routed	d to Pond	d 14P : Water	Quality			-

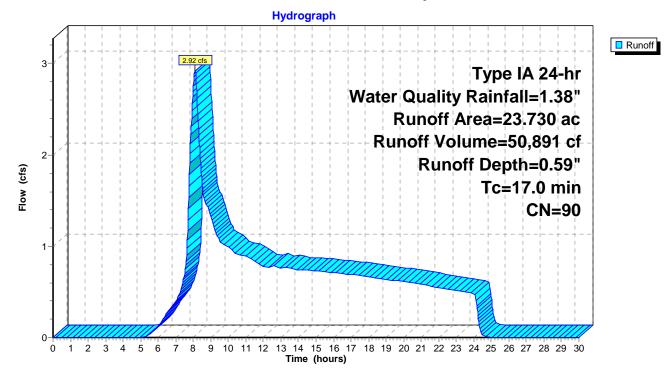
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Type IA 24-hr Water Quality Rainfall=1.38"

Area	(ac)	CN	Desc	cription			
15.	130	98	Pave	ed parking	, HSG D		
0.	860	80	>75%	% Grass co	over, Good,	, HSG D	
7.	740	74	>75%	% Grass co	over, Good,	, HSG C	
23.	730	90	Weig	phted Aver	age		
8.	600		36.2	4% Pervio	us Area		
15.	130		63.7	6% Imperv	vious Area		
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
(min)	(iee	:U	(11/11)	(INSEC)	(015)		

17.0

Direct Entry, Direct Entry

Subcatchment 2S: Developed



Summary for Pond 14P: Water Quality

[44] Hint: Outlet device #2 is below defined storage

Inflow Area =	1,033,679 sf, 63.76% Impervious,	Inflow Depth = 0.59" for Water Quality event
Inflow =	2.92 cfs @ 8.10 hrs, Volume=	50,891 cf
Outflow =	0.63 cfs @ 19.43 hrs, Volume=	21,765 cf, Atten= 79%, Lag= 680.1 min
Primary =	0.63 cfs @ 19.43 hrs, Volume=	21,765 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.02 hrs Peak Elev= 217.13' @ 19.43 hrs Surf.Area= 22,484 sf Storage= 32,818 cf

Plug-Flow detention time= 677.6 min calculated for 21,765 cf (43% of inflow) Center-of-Mass det. time= 385.7 min (1,220.3 - 834.7)

Volume	Inver	t Avail.Sto	rage Storage	Description	
#1 #2	215.65 215.66	,		Custom Stage Data (Prismatic) Listed below (Recalc)	
	210100			0' S= 0.0035 '/'	
		96,70	08 cf Total Av	ailable Storage	
Elevatio		Surf.Area	Inc.Store	Cum.Store	
(fee	1	(sq-ft)	(cubic-feet)	(cubic-feet)	
215.6		21,855	0	0	
216.0		21,887	7,655	7,655	
217.0		21,970	21,929	29,583	
218.0		22,053	22,012	51,595	
219.0		22,137	22,095	73,690	
220.0	0	22,220	22,179	95,868	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	215.60'	18.000" Rou	Ind Culvert	
	-		L= 12.0' RC	P, rounded edge	headwall, Ke= 0.100
			Inlet / Outlet	Invert= 215.60' / 2	215.58' S= 0.0017 '/' Cc= 0.900
			,	ow Area= 1.77 sf	
#2	Device 1	215.60'		Orifice/Grate C	
				ir flow at low hea	
#3	Device 1	217.00'			d-Crested Rectangular Weir
			· · ·	0.20 0.40 0.60 0	
Coef. (English) 2.80 2.92 3.08 3.30 3.32					
Drimory	OutFlow	Max-0.63 cfc (⑦ 10 /3 hrs ⊔	\//_217 13' (Free	o Dischargo)

Primary OutFlow Max=0.63 cfs @ 19.43 hrs HW=217.13' (Free Discharge)

-1=Culvert (Passes 0.63 cfs of 6.56 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.10 cfs @ 5.81 fps)

-3=Broad-Crested Rectangular Weir (Weir Controls 0.53 cfs @ 1.01 fps)

Prelim HydroCAD Model

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Pond 14P: Water Quality

